5.2.2.2. <u>199 Street NW</u>, south of 23 Avenue NW (N2-011 to N2-055)

The noise levels for receptor locations backing onto 199 Street NW south of 23 Avenue NW are projected to be below 65 dBA and range from 59.9 - 62.7 dBA. The relative difference in noise levels from the Future case *with* and *without* mitigation ranges from -3.5 to -4.5 dBA.

5.2.2.3. 215 Street NW, north of Quadrant Avenue (N2-056 to N2-083)

All $L_{eq}24$ noise levels for residential receptors backing on 215 Street north of Quadrant Avenue are projected to be below 65 dBA and range from 56.3 – 58.7 dBA. The relative difference in noise levels from the Future case *with* and *without* mitigation ranges from -6.8 to -10.7 dBA which is a significant decrease in noise level.

5.2.2.4. Riverview Way, between 215 Street NW and 199 Street NW (N2-084 to N2-116)

Noise mitigation was not required for residential receptors in this area. However, certain receptor locations will benefit from the noise mitigation implemented for other areas. For example, N2-084 will benefit from the noise mitigation implemented for receptors adjacent to 215 Street NW.



5.2.3. Neighbourhood 3 Residential Development

The results of the Future Case modeling *with* mitigation for NBHD 3 indicate noise levels ranging from 54.6 - 63.7 dBA $L_{eq}24$ as presented in Table 2d & Table 2e. Since all residential receptor $L_{eq}24$ noise levels are below 65 dBA, no further mitigation will be required to meet the requirements of the City of Edmonton UTNP C506A.

Receptor	L _{eq} 24 (dBA)	Difference Relative to Future Case Leq24 (dBA)	L _{eq} Day (dBA)	L _{eq} Night (dBA)		Receptor	Difference Relative to Future Case Leq24 (dBA)	L _{eq} 24 (dBA)	L _{eq} Day (dBA)	L _{eq} Night (dBA)
N3-001	62.9	-3.6	64.5	57.0		N3-034	63.5	-1.1	65.1	57.5
N3-002	62.0	-6.1	63.6	56.1		N3-035	63.7	-1.2	65.3	57.8
N3-003	62.0	-6.9	63.6	56.0		N3-036	60.1	0.0	61.6	54.4
N3-004	61.2	-7.3	62.9	55.2		N3-037	58.2	0.0	59.8	52.8
N3-005	61.2	-7.3	62.8	55.1		N3-038	57.1	0.0	58.6	51.9
N3-006	61.0	-7.5	62.6	54.9		N3-039	56.5	0.0	58.0	51.5
N3-007	60.9	-7.6	62.5	54.8		N3-040	56.2	0.0	57.6	51.2
N3-008	60.7	-7.9	62.3	54.6		N3-041	55.9	0.0	57.4	51.1
N3-009	60.6	-8.4	62.3	54.5		N3-042	55.8	0.0	57.3	51.1
N3-010	60.9	-7.4	62.6	54.8		N3-043	55.7	0.0	57.1	51.0
N3-011	60.8	-8.1	62.4	54.7		N3-044	55.6	0.0	57.0	51.0
N3-012	60.7	-8.1	62.3	54.6		N3-045	55.6	0.0	57.1	51.1
N3-013	61.0	-7.9	62.6	54.9		N3-046	55.7	0.0	57.2	51.2
N3-014	61.1	-7.6	62.7	55.0		N3-047	55.9	0.0	57.3	51.4
N3-015	60.9	-8.4	62.5	54.8		N3-048	56.2	0.0	57.6	51.7
N3-016	60.9	-8.4	62.6	54.9		N3-049	56.6	0.0	58.0	52.2
N3-017	61.6	-7.5	63.2	55.5		N3-050	57.7	0.0	59.1	53.3
N3-018	61.2	-7.5	62.8	55.2		N3-051	58.5	0.0	59.9	54.1
N3-019	61.3	-7.7	62.9	55.2		N3-052	57.3	0.0	58.7	52.9
N3-020	61.3	-7.6	62.9	55.2		N3-053	55.3	0.0	56.7	50.9
N3-021	61.6	-7.3	63.2	55.5		N3-054	54.6	0.0	56.0	50.2
N3-022	61.3	-6.7	62.9	55.3		N3-055	61.7	-3.2	63.3	55.9
N3-023	62.3	-7.5	63.9	56.2		N3-056	60.6	-3.5	62.2	54.8
N3-024	62.8	-6.9	64.4	56.7		N3-057	60.8	-3.1	62.4	55.0
N3-025	62.5	-7.0	64.1	56.4		N3-058	60.3	-3.7	61.9	54.5
N3-026	62.5	-6.5	64.1	56.5	ļ	N3-059	60.0	-3.3	61.5	54.2
N3-027	61.9	-6.6	63.5	55.9		N3-060	60.3	-3.5	61.8	54.5
N3-028	62.0	-7.2	63.6	55.9	ļ	N3-061	60.3	-3.2	61.9	54.5
N3-029	62.6	-6.7	64.2	56.5	ļ	N3-062	60.2	-3.9	61.8	54.5
N3-030	62.6	-6.8	64.2	56.5	ļ	N3-063	61.7	-3.2	63.3	56.0
N3-031	62.5	-7.1	64.1	56.4	ļ	N3-064	59.9	-4.0	61.5	54.2
N3-032	62.2	-0.9	63.8	56.2		N3-065	59.8	-3.9	61.4	54.1
N3-033	62.7	-1.2	64.3	56.7		N3-066	59.8	-3.5	61.4	54.1

Table 2d. Future Case With Mitigation Noise Modeling Results (Neighbourhood 3)



Receptor	L _{eq} 24 (dBA)	Difference Relative to Future Case Leq24 (dBA)	L _{eq} Day (dBA)	L _{eq} Night (dBA)	Receptor	Difference Relative to Future Case Leq24 (dBA)	L _{eq} 24 (dBA)	L _{eq} Day (dBA)	L _{eq} Night (dBA)
N3-067	59.6	-3.9	61.1	53.8	N3-099	58.9	-4.1	60.5	53.1
N3-068	59.4	-3.6	61.0	53.7	N3-100	59.1	-3.7	60.6	53.3
N3-069	59.5	-4.0	61.0	53.7	N3-101	58.9	-4.2	60.5	53.2
N3-070	59.4	-3.7	61.0	53.7	N3-102	58.9	-4.2	60.5	53.2
N3-071	59.4	-4.0	60.9	53.6	N3-103	59.1	-3.7	60.6	53.3
N3-072	59.4	-3.7	61.0	53.7	N3-104	58.9	-4.2	60.5	53.2
N3-073	59.4	-4.1	60.9	53.6	N3-105	58.9	-4.0	60.5	53.2
N3-074	59.4	-3.6	61.0	53.6	N3-106	58.9	-3.9	60.5	53.2
N3-075	59.4	-4.1	61.0	53.7	N3-107	58.9	-4.2	60.5	53.1
N3-076	59.5	-3.6	61.1	53.7	N3-108	58.9	-4.0	60.5	53.1
N3-077	60.1	-4.5	61.6	54.3	N3-109	59.0	-4.2	60.6	53.2
N3-078	61.1	-3.4	62.7	55.4	N3-110	59.2	-4.0	60.7	53.4
N3-079	61.4	-3.3	63.0	55.6	N3-111	60.1	-5.1	61.7	54.4
N3-080	60.7	-3.6	62.3	55.0	N3-112	59.5	0.0	61.1	53.8
N3-081	59.8	-3.7	61.4	54.1	N3-113	59.4	0.0	61.0	53.7
N3-082	59.5	-3.8	61.1	53.7	N3-114	61.1	0.0	62.7	55.4
N3-083	59.6	-3.7	61.2	53.8	N3-115	61.2	-0.1	62.8	55.5
N3-084	59.5	-3.7	61.0	53.7	N3-116	61.5	0.0	63.0	55.7
N3-085	59.3	-3.7	60.8	53.5	N3-117	62.0	-0.4	63.6	56.3
N3-086	59.3	-3.9	60.9	53.6	N3-118	62.2	-3.9	63.8	56.5
N3-087	59.3	-4.3	60.9	53.6	N3-119	61.5	-3.8	63.1	55.8
N3-088	59.3	-3.9	60.9	53.6	N3-120	61.1	-4.1	62.7	55.4
N3-089	59.3	-4.1	60.9	53.5	N3-121	61.3	-4.1	62.9	55.5
N3-090	59.4	-3.7	61.0	53.6	N3-122	61.1	-4.1	62.7	55.3
N3-091	60.1	-4.8	61.7	54.3	N3-123	61.0	-4.1	62.5	55.2
N3-092	59.6	-3.7	61.2	53.8	N3-124	60.9	-4.0	62.5	55.2
N3-093	58.9	-3.9	60.5	53.2	N3-125	61.1	-4.2	62.6	55.3
N3-094	58.6	-3.9	60.2	52.9	N3-126	61.2	-3.8	62.7	55.4
N3-095	59.2	-4.0	60.8	53.5	N3-127	61.3	-3.6	62.8	55.5
N3-096	59.2	-3.9	60.8	53.5	N3-128	61.5	-3.9	63.1	55.7
N3-097	59.2	-4.0	60.8	53.4	N3-129	61.3	-3.8	62.9	55.6
N3-098	59.2	-3.8	60.7	53.4	N3-130	61.7	-4.4	63.2	55.9

Table 2e. Future Case With Mitigation Noise Modeling Results (Neighbourhood 3 cont.)



5.2.3.1. 23 Avenue NW, between 199 Street NW and AHD (N3-001 to N3-035)

The noise levels for receptor locations backing onto 23 Avenue NW between 199 Street NW and AHD are projected to be below 65 dBA and range from 60.6 - 63.7 dBA. The relative difference in noise levels from the Future case *with* and *without* mitigation ranges from -0.9 to -8.4 dBA.

5.2.3.2. Anthony Henday Drive, (N3-036 to N3-054)

Noise mitigation was not required for residential receptors in this area.

5.2.3.3. Riverview Way, between 23 Avenue NW and 199 Street NW (N3-055 to N3-117)

The noise levels for receptor locations backing onto Riverview Way between 23 Avenue NW and 199 Street NW are projected to be below 65 dBA and range from 58.6 - 62.0 dBA. The relative difference in noise levels from the Future case *with* and *without* mitigation ranges from 0.0 to -5.1 dBA.

5.2.3.4. <u>199 Street NW, north of 23 Avenue NW (N2-118 to N2-130)</u>

As indicated in Table 2e, the noise levels for receptor locations backing onto 199 Street between 23 Avenue NW and Riverview Way are projected to be below 65 dBA and range from 60.9 - 62.2 dBA. The relative difference in noise levels from the Future case *with* and *without* mitigation ranges from -3.6 to -4.4 dBA.



5.3. Noise Barrier Description

To achieve the noise levels shown in Tables 2a - 2e and Figures 3a - 3g the following barriers were included in the model. To simplify the description of the barrier configuration, the study area has been again divided into separate sections within each neighbourhood. A breakdown of each section can be found in Figures 4a - 4f. Note that all barrier heights are relative to the **modeled existing grade** at the residential area boundary line (the location of the modeled barriers). It is also important to note that the barriers are modeled as continuous and must meet any adjacent segment with no holes or gaps. The barriers can either start/finish abruptly or slowly taper up/down after the required barrier lengths/heights are implemented. Lastly, in areas in which the barrier terminates at an adjacent road the barrier must tie-in to the rear of the residential structure (i.e. house) as shown in the figures.

5.3.1. <u>Neighbourhood 1 Residential Development</u>

5.3.1.1. 215 Street NW, north of 23 Avenue NW (N1-001 to N1-006)

As stipulated by the City of Edmonton's Transportation Planning a minimum of a 1.0 m berm + 1.83 m noise fence is required adjacent to designated truck routes. Therefore a 1.0 m berm + 1.83 m noise barrier is required along the property line (side or rear) adjacent to 215 Street NW. For Receptor N1-001 the barrier must wrap around approximately 10 m to the east. For Receptor N1-005, the berm/barrier must continue until it reaches the southwest corner before reducing in height to 1.83 m. It must then continue east for approximately 30 m at a height of 1.83 m.

5.3.1.2. 23 Avenue NW, between 215 Street NW and 199 Street NW (N1-006 to N1-023)

A 1.83 m barrier is required for residential receptors N1-010 to N1-021¹. A 1.83 m barrier will also be required for the MDR lands west 203 Street NW only if there are private backyards adjacent to 23 Avenue NW or 203 Street NW. The noise model indicated that the barrier in this location must extend approximately 20 m to the west and 30 m north of the southeast corner.

5.3.1.3. <u>199 Street NW, north of 23 Avenue NW (N1-024 to N1-054)</u>

A 1.83 m barrier is required for all residential receptor locations adjacent to 199 Street NW north of 23 Avenue NW.

¹ It should be noted that a barrier is technically not required for Receptors N1-019 to N1-021. The barrier was implemented in order to remain consistent with the other adjacent residential lots to the west.



5.3.1.4. 23 Avenue NW, between 199 Street NW and AHD (N1-055 to N1-063)

A 2.44 m barrier is required for all residential receptor locations adjacent to 23 Avenue NW. For Receptor N1-055, the barrier must extend approximately 10 m to the north. A 2.44 m barrier will also be required for the MDR lands east 203 Street NW only if there are private backyards adjacent to 23 Avenue NW or the adjacent collector road. The noise model indicated that the barrier in this location must extend approximately 25 m north of the southwest corner and 10 m north of the southeast corner.

5.3.2. Neighbourhood 2 Residential Development

5.3.2.1. 23 Avenue NW, between 215 Street NW and 199 Street NW (N2-001 to N2-010)

A 1.83 m barrier is required for residential receptors N2-004 to N2-010. A 1.83 m barrier will also be required for the MDR lands east 203 Street NW if there are private backyards adjacent to 23 Avenue NW or 203 Street NW. The noise model indicated that the barrier for the MDR lands would have to extend to the detached single family residential properties to the west (Receptor N2-009) and would have to wrap around to the south by approximately 70 m.

5.3.2.2. <u>199 Street NW, south of 23 Avenue NW (N2-011 to N2-055)</u>

A 1.83 m barrier is required for all residential receptor locations adjacent to 199 Street NW south of 23 Avenue NW. In areas in which the barrier does not meet an adjacent segment of fence or tie-in to a residential structure the barrier must extend approximately 10 m in the opposite direction of 199 Street NW.

5.3.2.3. 215 Street NW, north of Quadrant Avenue (N2-056 to N2-083)

A 1.0 m berm + 1.83 m noise barrier is required along the property line (side or rear) adjacent to 215 Street NW. The barrier must extend approximately 10 m east in areas in which the barrier does not meet an adjacent segment of fence or tie-in to a residential structure.

5.3.2.4. <u>Riverview Way, between 215 Street NW and 199 Street NW (N2-084 to N2-116)</u> Noise mitigation was not required for residential receptors in this area.



5.3.3. Neighbourhood 3 Residential Development

5.3.3.1. 23 Avenue NW, between 199 Street NW and AHD (N3-001 to N3-035)

Noise mitigation will be required for the MDR lands directly adjacent to 199 Street NW only if there are private backyards adjacent to 23 Avenue NW or 199 Street NW. The noise model indicated that the required barrier height adjacent to 199 Street is 1.83 m. The barrier must extend approximately 10 m east of the southwest corner. The required barrier height increases to 2.44 m in the northwest corner of the MDR lands and continues east until reaching the detached single family residential properties (Receptor N3-007). Continuing to the east, a 2.44 m barrier is required for all residential receptor locations directly adjacent to 23 Avenue NW. (N3-007 to N3-031). Receptors adjacent to, but further away from 23 Avenue (N3-032 to N3-035) require a 1.83 m barrier.

5.3.3.2. Anthony Henday Drive, (N3-036 to N3-054)

Noise mitigation was not required for residential receptors in this area.

5.3.3.3. Riverview Way, between 23 Avenue NW and 199 Street NW (N3-055 to N3-117)

With exception of Receptors N3-112 to N3-117, a 1.83 m barrier is required for all residential receptor locations adjacent to Riverview Way south of 23 Avenue NW. In areas in which the barrier does not meet an adjacent segment of fence or tie-in to a residential structure the barrier must extend approximately 10 m in the opposite direction of Riverview Way.

5.3.3.4. <u>199 Street NW, north of 23 Avenue NW (N3-118 to N3-130)</u>

A 1.83 m barrier is required for all residential receptor locations adjacent to 199 Street NW, south of 23 Avenue NW. In areas in which the barrier does not meet an adjacent segment of fence or tie-in to a residential structure the barrier must extend approximately 10 m in the opposite direction of 199 Street NW / Quadrant Avenue.



5.4. Barrier Construction

Barrier construction can be either solid screen wood fences or masonry noise walls. If using wood materials, the fences should be, at a minimum, double boarded with no visible gaps through the fence or at the bottom and have a surface density of at least 20 kg/m². A sample schematic of fence construction is provided in <u>Figure 5</u>. For masonry noise walls, there should also be no visible gaps and the surface density must also be at least 20 kg/m².

If there are to be any walkways or roadways penetrating through the proposed barrier locations, then the barrier should either: a) wrap around on both sides of the opening on the inside for at least the distance from the rear property line to the structure or, b) wrap around past the opening for at least 3 equivalent opening dimensions. Both options are shown in Figure 6.

With regards to noise control, for all barriers it is possible to exchange berm height for fence height and vice-versa, as long as the centerline of the barrier does not change (i.e. it remains at the current proposed property line). The key is that the total height has to be that listed above.



6.0 Conclusion

The results of the Future Case modeling for Neighbourhood 1 indicated noise levels ranging from 61.7 - 70.8 dBA $L_{eq}24$. Neighbourhood 2 indicated noise levels ranging from 57.6 – 67.8 dBA $L_{eq}24$ while Neighbourhood 3 indicated noise levels ranging from 54.6 – 69.8 dBA $L_{eq}24$. As a result, noise mitigation measures were investigated for residential receptor locations above 65 dBA $L_{eq}24$ to lower the noise levels to below the requirements the UTNP C506A criteria.

The results of the Future Case noise modeling *with* mitigation for all 3 neighbourhoods (for residential backyard spaces that initially exceeded 65 dBA) indicated noise levels below the UTNP C506A criteria of 65 dBA $L_{eq}24$. A variety of barrier heights were implemented within the model to achieve the projected noise levels.



7.0 <u>References</u>

- City of Edmonton Urban Traffic Noise Policy (C506A), 2013
- City of Edmonton Community Standards Bylaw 14600, 2008
- Riverview Neighbourhoods 1, 2 &3 Neighbourhood Structure Plans Transportation Impact Assessment, prepared for Qualico Development West, Walton Development and Management LP, Sunwapta Holdings Corp., Melcor Developments Ltd. & S.P. Singh by Bunt & Associates (May 30, 2014).
- Environmental Noise Study for Southwest Anthony Henday Drive in Edmonton, AB, Prepared for AECOM, by aci Acoustical Consultants Inc., December 2013.
- International Organization for Standardization (ISO), Standard 1996-1, Acoustics Description, measurement and assessment of environmental noise – Part 1: Basic quantities and assessment procedures, 2003, Geneva Switzerland.
- International Organization for Standardization (ISO), Standard 9613-1, Acoustics Attenuation of sound during propagation outdoors Part 1: Calculation of absorption of sound by the atmosphere, 1993, Geneva Switzerland.
- International Organization for Standardization (ISO), Standard 9613-2, Acoustics Attenuation of sound during propagation outdoors – Part 2: General method of calculation, 1996, Geneva Switzerland.



To be inserted once available

Figure 1. Study Area



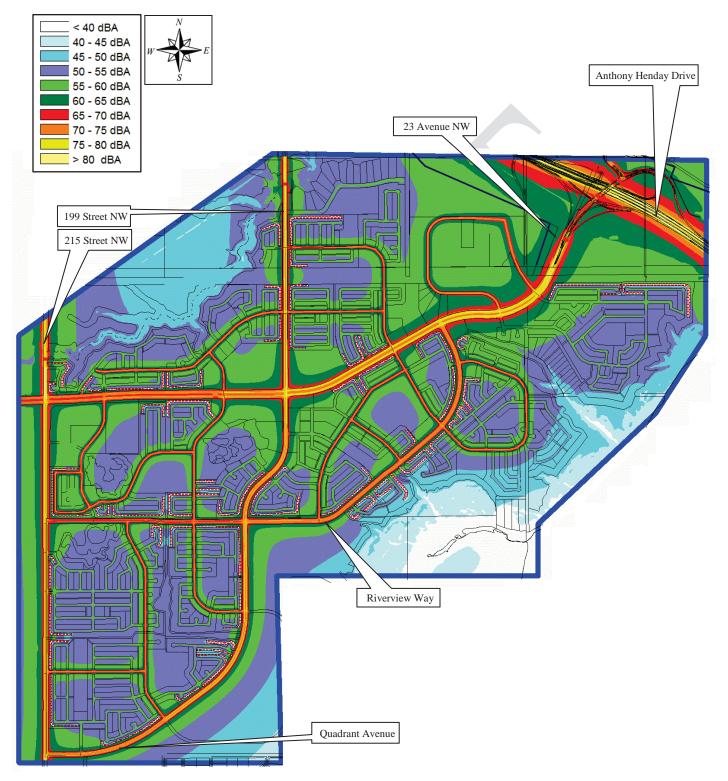
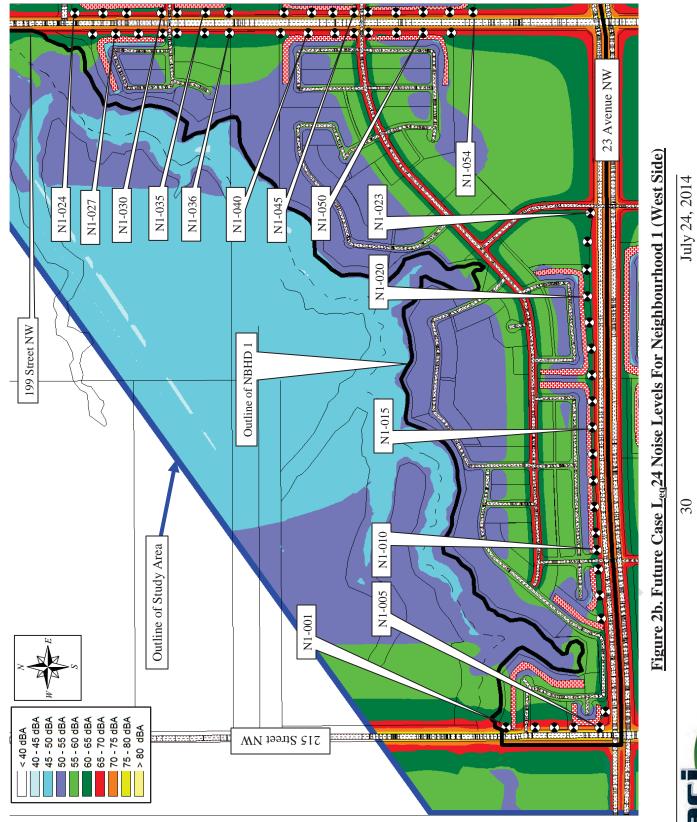


Figure 2a. Future Case Leg24 Noise Levels For Entire Study Area



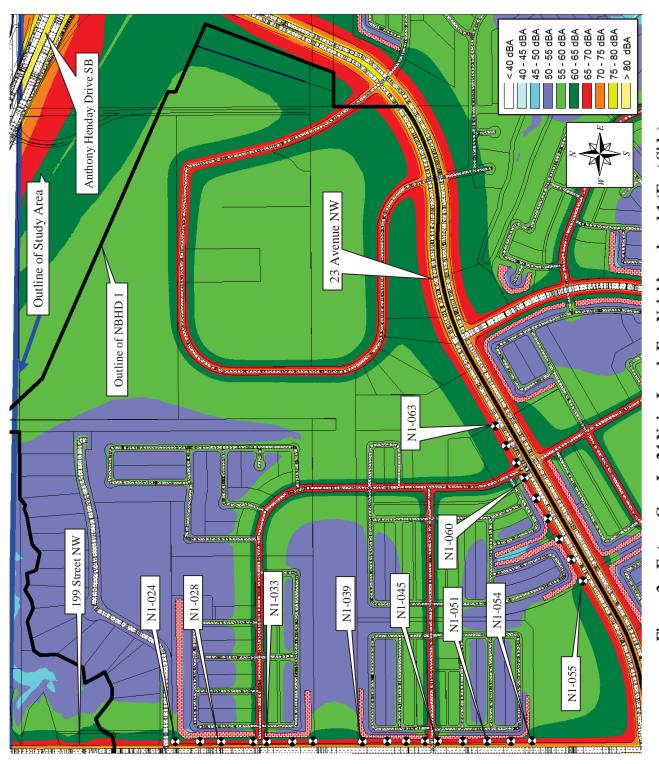


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Figure 2c. Future Case Levels Levels For Neighbourhood 1 (East Side) July 24, 2014 31



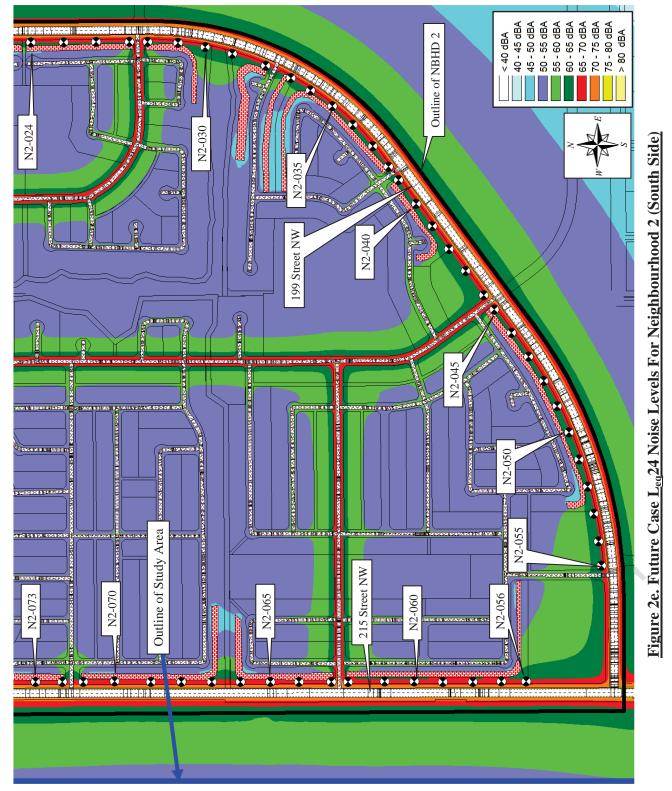


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July 24, 2014



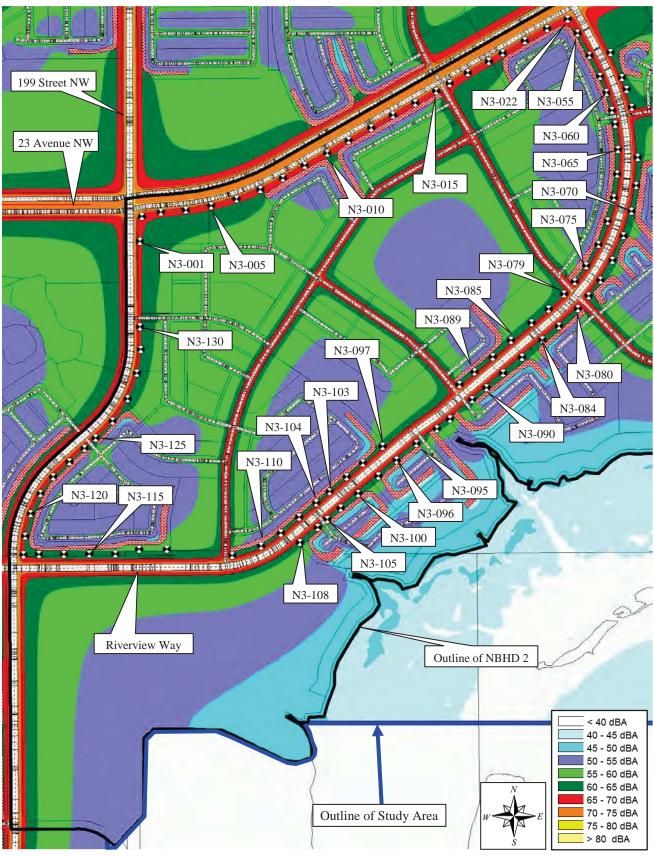


Figure 2f. Future Case Leg24 Noise Levels For Neighbourhood 3 (West Side)



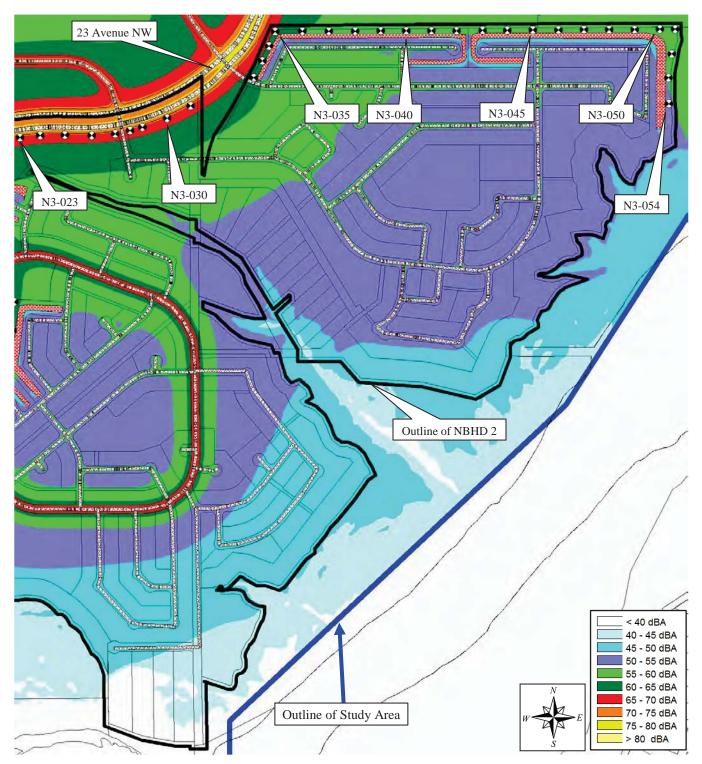


Figure 2g. Future Case L_{eq}24 Noise Levels For Neighbourhood 3 (East Side)



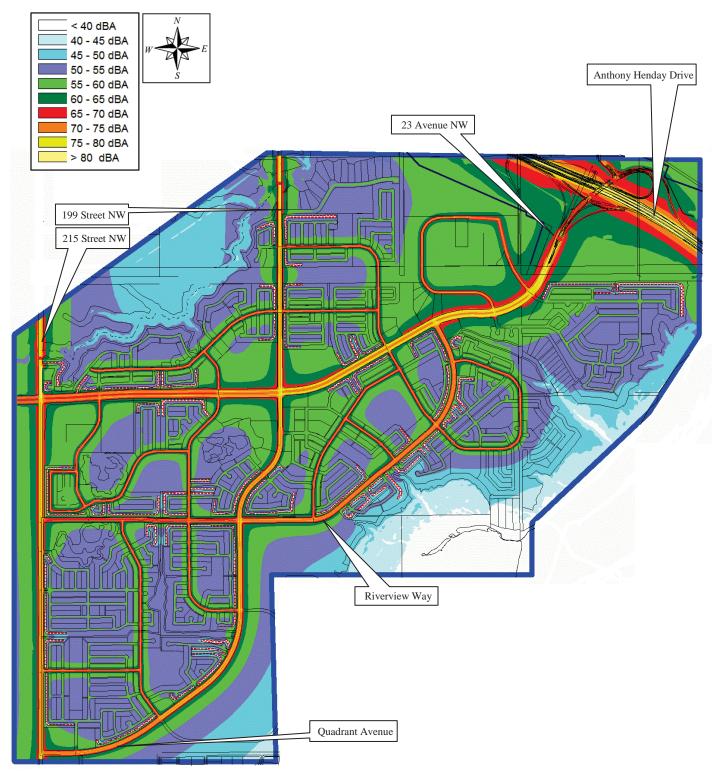
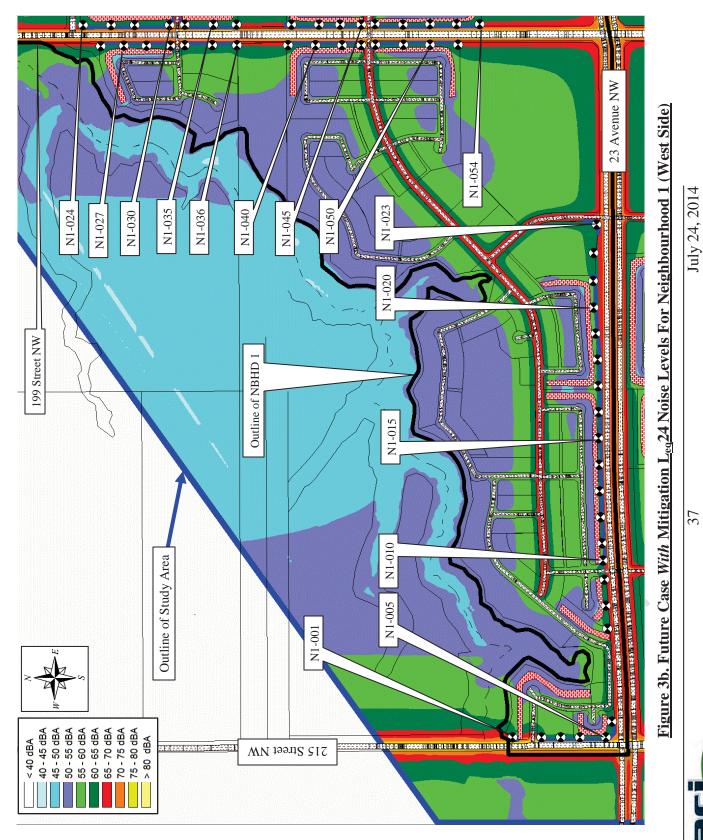


Figure 3a. Future Case With Mitigation Levels For Entire Study Area





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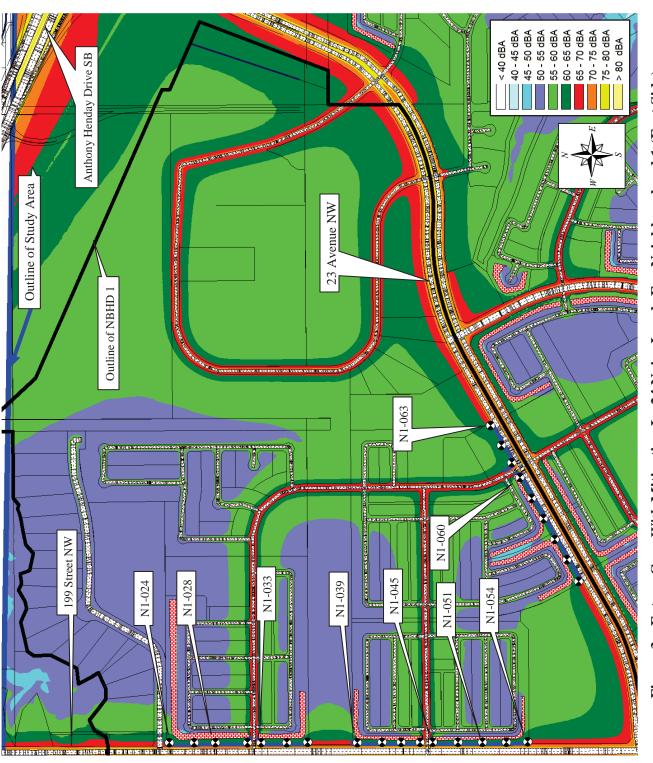


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Figure 3c. Future Case With Mitigation Leaded Noise Levels For Neighbourhood 1 (East Side) July 24, 2014





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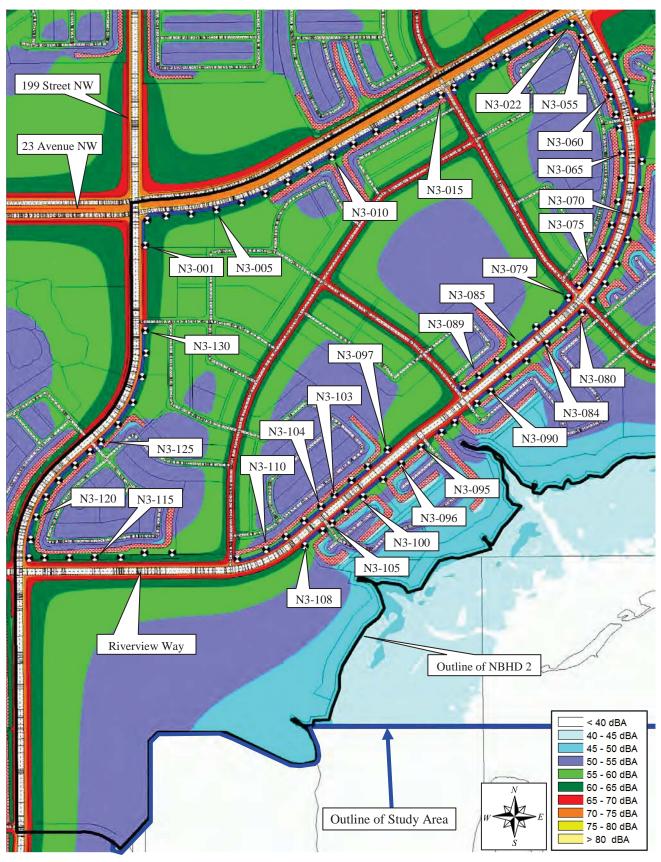


Figure 3f. Future Case With Mitigation Leg24 Noise Levels For Neighbourhood 3 (West Side)



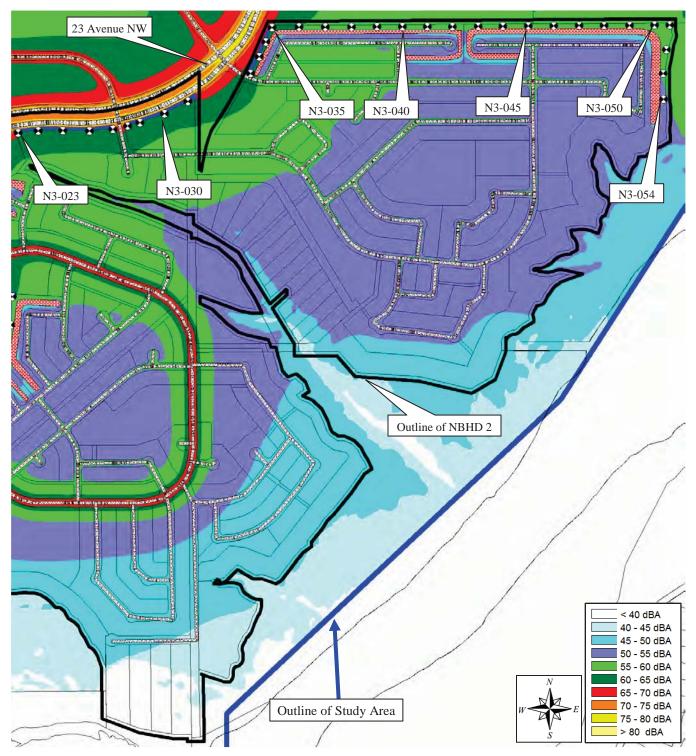
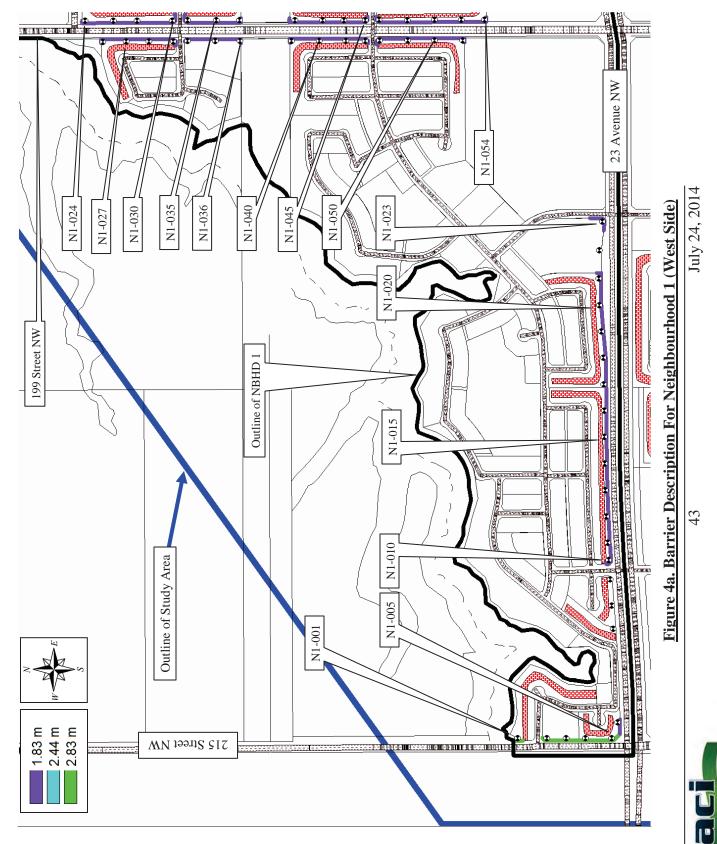
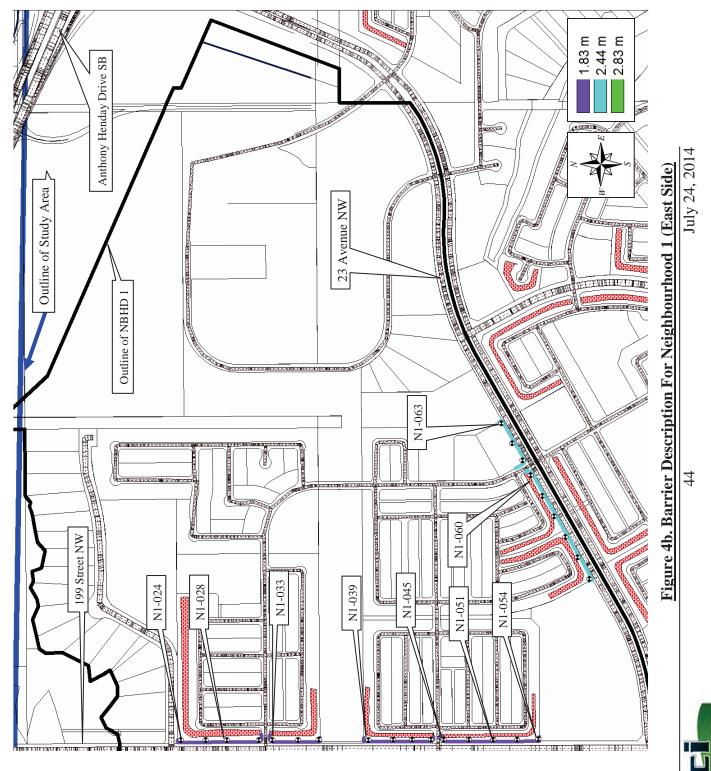


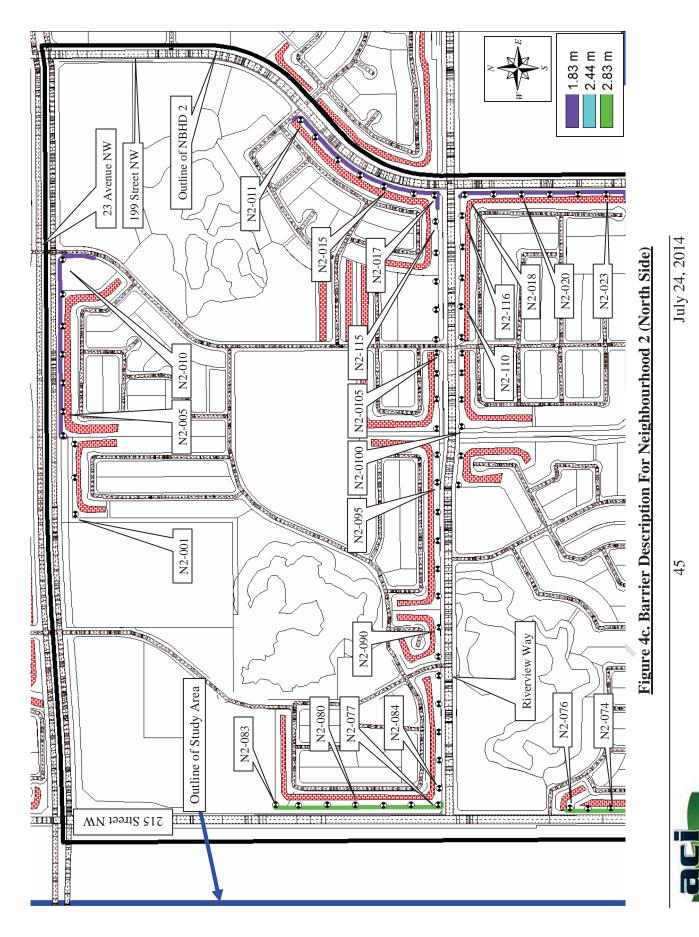
Figure 3g. Future Case With Mitigation Leg24 Noise Levels For Neighbourhood 3 (East Side)

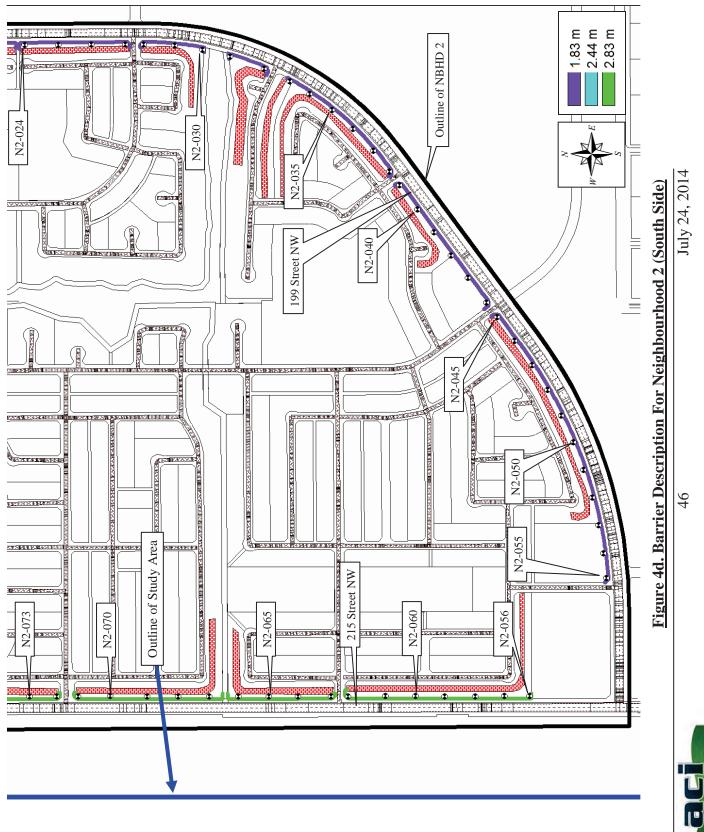






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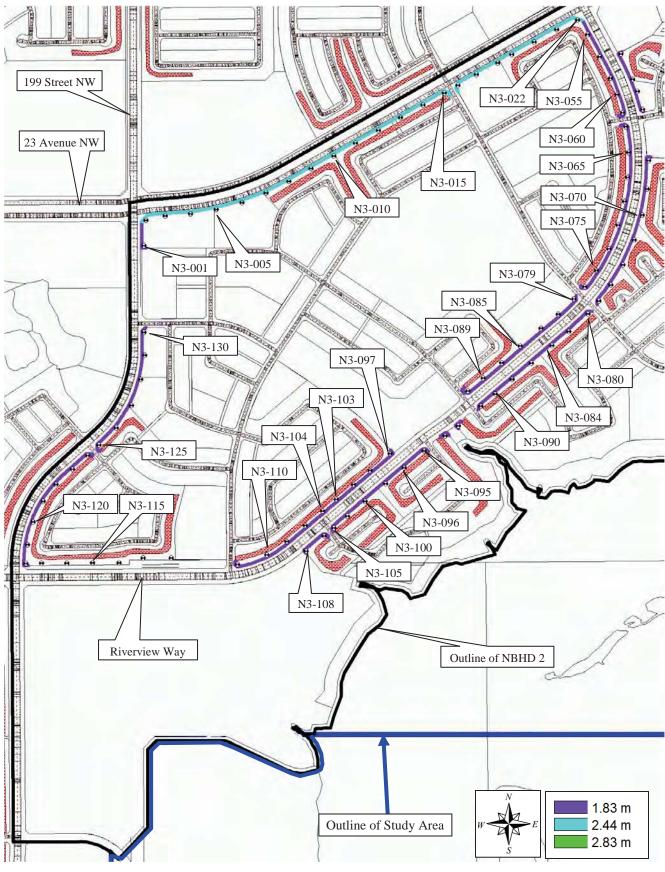


Figure 4e. Barrier Description For Neighbourhood 3 (West Side)



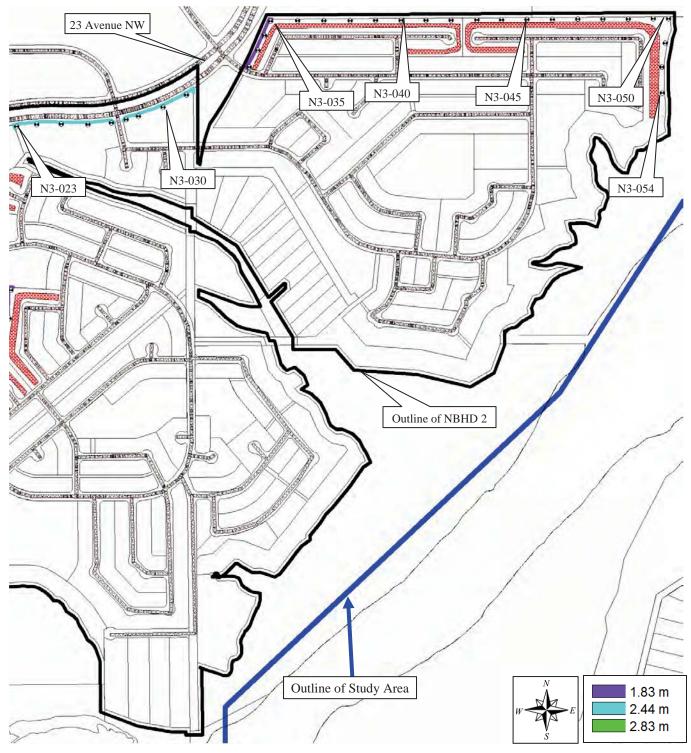


Figure 4f. Barrier Description For Neighbourhood 3 (East Side)



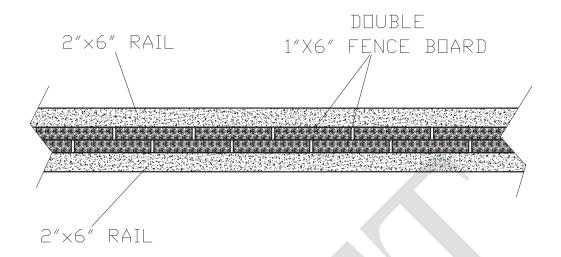


Figure 5. Minimum Recommended Wooden Fence Construction Sectional View

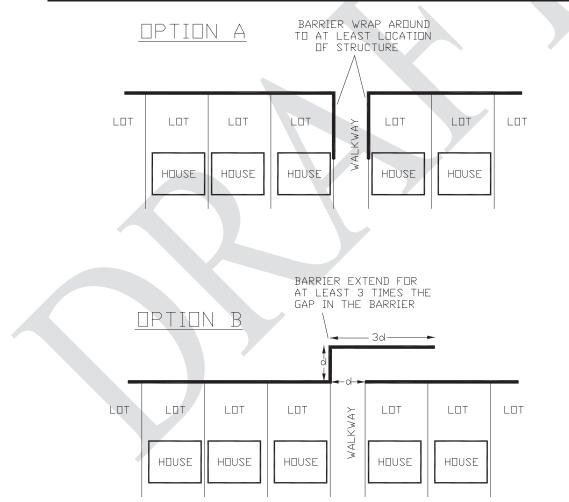


Figure 6. Minimum Recommended Walkway/Roadway Penetration Barrier Construction



Appendix I NOISE MODELING PARAMETERS

(Wendlos) Per Hour) Vehicles Per Hour) Vehicles (Wmnr) 23 Avenue - West of AHD - EB 34878 2093 5 388 4 70 23 Avenue - West of 148 Street - WB 33388 2003 5 371 4 70 23 Avenue - West of 184 Street - WB 233388 2003 5 371 4 70 23 Avenue - West of 187 Street - WB 29828 1790 5 331 4 70 23 Avenue - West of 187 Street - EB 19883 1199 5 222 4 70 23 Avenue - West of Newniew Way - EB 19983 1199 5 222 4 70 23 Avenue - West of 195 Street - EB 18448 1107 5 205 4 70 23 Avenue - West of 199 Street - EB 13498 810 5 150 4 70 23 Avenue - West of 199 Street - BB 10183 611 5 113 4 70 23 Avenue - West of 212 Street - BB 7338 446	Deed	Total Volume	Day	Day	Night	Night	Speed
23 Avenue - West of AHD - EB 34878 2003 5 388 4 70 23 Avenue - West of 184 Street - EB 33388 2003 5 371 4 70 23 Avenue - West of 184 Street - EB 33388 2003 5 331 4 70 23 Avenue - West of 187 Street - EB 29828 1790 5 331 4 70 23 Avenue - West of 187 Street - EB 29828 1790 5 331 4 70 23 Avenue - West of 195 Street - EB 19893 1199 5 222 4 70 23 Avenue - West of 195 Street - WB 194983 1107 5 205 4 70 23 Avenue - West of 198 Street - EB 18448 1107 5 205 4 70 23 Avenue - West of 198 Street - WB 10183 611 5 113 4 70 23 Avenue - West of 212 Street - WB 7438 446 5 83 4 70 23 Avenue - West of 212 Street - WB 7438 <t< th=""><th>Road</th><th>•</th><th>(Vehicles Per Hour)</th><th>% Heavy Vehicles</th><th>(Vehicles Per Hour)</th><th>% Heavy Vehicles</th><th></th></t<>	Road	•	(Vehicles Per Hour)	% Heavy Vehicles	(Vehicles Per Hour)	% Heavy Vehicles	
23 Avenue - West of 184 Street - EB 33388 2003 5 371 4 70 23 Avenue - West of 187 Street - EB 33388 2003 5 331 4 70 23 Avenue - West of 187 Street - EB 29828 1790 5 331 4 70 23 Avenue - West of 187 Street - EB 29828 1790 5 231 4 70 23 Avenue - West of 187 Street - WB 19983 1199 5 222 4 70 23 Avenue - West of 195 Street - WB 18448 1107 5 205 4 70 23 Avenue - West of 195 Street - EB 18448 1107 5 205 4 70 23 Avenue - West of 203 Street - EB 18448 1107 5 150 4 70 23 Avenue - West of 203 Street - EB 10183 611 5 113 4 70 23 Avenue - West of 203 Street - EB 1738 446 5 83 4 70 23 Avenue - West of 212 Street - EB 7438	23 Avenue - West of AHD - WB	34878	2093	5	388	4	70
23 Avenue - West of 184 Street - EB 33388 2003 5 371 4 70 23 Avenue - West of 187 Street - EB 29828 1790 5 331 4 70 23 Avenue - West of 187 Street - EB 29828 1790 5 331 4 70 23 Avenue - West of 187 Street - EB 19983 1199 5 222 4 70 23 Avenue - West of 195 Street - EB 19983 1199 5 222 4 70 23 Avenue - West of 195 Street - EB 199848 1107 5 205 4 70 23 Avenue - West of 199 Street - EB 18448 1107 5 205 4 70 23 Avenue - West of 199 Street - EB 13498 810 5 150 4 70 23 Avenue - West of 203 Street - EB 10183 611 5 113 4 70 23 Avenue - West of 212 Street - WB 7438 446 5 83 4 70 23 Avenue - West of 212 Street - WB 7438	23 Avenue - West of AHD - EB	34878	2093	5	388	4	70
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	Highway 627 - East of 215 Street - WB Highway 627 - East of 215 Street - EB	8280	497 497	4	92 92	4	70



Road	Total Volume (vehicles per day)	Day (Vehicles Per Hour)	Day % Heavy Vehicles	Night (Vehicles Per Hour)	Night % Heavy Vehicles	Speed (km/hr)
AHD South of 62 Avenue NB	45540	2620	12.3	693	12.3	100
AHD South of 62 Avenue SB	48176	2772	12.3	733	12.3	100
AHD South of Lessard Road NB	47331	2723	11.5	720	11.5	100
AHD South of Lessard Road SB	48935	2815	11.5	745	11.5	100
AHD East of Cameron Heights Drive NB	48728	2804	11.0	742	11.0	100
AHD East of Cameron Heights Drive SB	50250	2891	11.0	765	11.0	100
AHD South of Terwillegar Drive NB	45841	2637	10.6	698	10.6	100
AHD South of Terwillegar Drive SB	47065	2708	10.6	716	10.6	100
AHD East of Rabbit Hill Road WB	47283	2720	10.0	720	10.0	100
AHD East of Rabbit Hill Road EB	49998	2877	10.0	761	10.0	100
Lessard Road East of AHD EB	7200	414	4.2	110	4.2	60
Lessard Road East of AHD WB	7950	457	4.2	121	4.2	60
Lessard Road West of AHD EB	10150	584	4.8	154	4.8	60
Lessard Road West of AHD WB	8450	486	4.8	129	4.8	60
AHD NB to Lessard Road EB Ramp	3050	175	4.0	46	4.0	70
AHD NB to Lessard Road WB Ramp	3150	181	7.0	48	7.0	70
Lessard Road WB to AHD NB Ramp	3300	190	4.1	50	4.1	70
Lessard Road WB to AHD SB Ramp	3000	173	5.2	46	5.2	60
AHD SB to Lessard Road WB Ramp	3650	210	5.5	56	5.5	70
AHD SB to Lessard Road EB Ramp	1750	101	5.9	27	5.9	70
Lessard Road EB to AHD SB Ramp	3900	224	5.7	59	5.7	70
Lessard Road EB to AHD NB Ramp	3850	222	4.1	59	4.1	60
Cameron Heights Drive South of AHD NB	3450	198	2.0	53	2.0	70
Cameron Heights Drive South of AHD SB	3300	190	2.0	50	2.0	70
Cameron Heights Drive North of AHD NB	3000	173	9.5	46	9.5	60
Cameron Heights Drive North of AHD SB	3500	201	9.5	53	9.5	60
AHD WB to Cameron Heights Drive NB Ramp	1100	63	6.0	17	6.0	60
AHD WB to Cameron Heights Drive SB Ramp	2400	138	2.0	37	2.0	60
Cameron Heights Drive SB to AHD WB Ramp	1950	112	9.9	30	9.9	60
Cameron Heights Drive SB to AHD EB Ramp	1200	69	8.6	18	8.6	60
AHD EB to Cameron Heights Drive SB Ramp	550	32	2.0	8	2.0	60
AHD EB to Cameron Heights Drive NB Ramp	1700	98	12.9	26	12.9	60
Cameron Heights Drive NB to AHD EB Ramp	2750	158	2.0	42	2.0	60
Cameron Heights Drive NB to AHD WB Ramp	500	29	2.0	8	2.0	60
170 Street South of AHD NB	18700	1076	7.4	285	7.4	70
170 Street South of AHD NB	16950	975	7.4	258	7.4	70
Terwillegar Drive North of AHD NB	17800	1024	4.2	230	4.2	70
Terwillegar Drive North of AHD SB	15750	906	4.2	240	4.2	70
AHD NB to Terwillegar Drive NB Ramp	4750	273	8.0	72	8.0	70
AHD NB to 170 Street SB Ramp	4150	273	11.4	63	0.0 11.4	70
				72		
Terwillegar Drive SB to AHD NB Ramp	4700	270	4.8		4.8	70
Terwillegar Drive SB to AHD SB Ramp	4400	253	8.8	67	8.8	70
AHD SB to 170 Street SB Ramp	6150	354	4.2	94	4.2	70
AHD SB to Terwillegar Drive NB Ramp	4900	282	4.3	75	4.3	70
170 Street NB to AHD SB Ramp	4550	262	13.2	69	13.2	70
170 Street NB to AHD NB Ramp	6000	345	5.2	91	5.2	70
156 Street South of AHD NB	16200	932	10.0	247	10.0	60
156 Street South of AHD SB	12400	713	10.0	189	10.0	60
Ellerslie Road East of Gateway Boulevard EB	23340	1343	4	355.3	4	60.0
Ellerslie Road East of Gateway Boulevard WB	23340	1343	4	355.3	4	60.0
Collector Roads	8000	480	3	89	3	60
Residential Streets	200	12	2	2	2	50



Appendix II THE ASSESSMENT OF ENVIRONMENTAL NOISE (GENERAL)

Sound Pressure Level

Sound pressure is initially measured in Pascal's (Pa). Humans can hear several orders of magnitude in sound pressure levels, so a more convenient scale is used. This scale is known as the decibel (dB) scale, named after Alexander Graham Bell (telephone guy). It is a base 10 logarithmic scale. When we measure pressure we typically measure the RMS sound pressure.

$$SPL = 10\log_{10}\left[\frac{P_{RMS}^{2}}{P_{ref}^{2}}\right] = 20\log_{10}\left[\frac{P_{RMS}}{P_{ref}}\right]$$

Where:

SPL = Sound Pressure Level in dB

 P_{RMS} = Root Mean Square measured pressure (Pa)

 P_{ref} = Reference sound pressure level ($P_{ref} = 2 \times 10^{-5} \text{ Pa} = 20 \text{ }\mu\text{Pa}$)

This reference sound pressure level is an internationally agreed upon value. It represents the threshold of human hearing for "typical" people based on numerous testing. It is possible to have a threshold which is lower than 20 μ Pa which will result in negative dB levels. As such, zero dB does not mean there is no sound!

In general, a difference of $1 - 2 \, dB$ is the threshold for humans to notice that there has been a change in sound level. A difference of 3 dB (factor of 2 in acoustical energy) is perceptible and a change of 5 dB is strongly perceptible. A change of 10 dB is typically considered a factor of 2. This is quite remarkable when considering that 10 dB is 10-times the acoustical energy!



A.	Sound pressure in decibels (dB)	Sound pres in pound per squa inch (PS	ls re
	-		Common Sounds
M.C.S.	160 -	3 X10 -1	Medium jet engine
RF {	140-	3x10 ⁻²	Large propeller aircraft Air raid siren Rıveting and chipping
	120-	3x10 ⁻³	Discotheque
		-	Punch press
	100-	3X10 ⁻⁴	Canning plant Heavy city traffic; subway
en [80-	3x10 ⁻⁵	Busy office
E Co B	60-	3x10 ⁻⁶	Normal speech
	-		Private office
IT A Y	40-	3X10-7	Quiet residential neighborhood
	-	1010	
	20-	3 x10 -8	Whisper
	1 204		
	0-	3 X10 -9	Threshold of hearing



Frequency

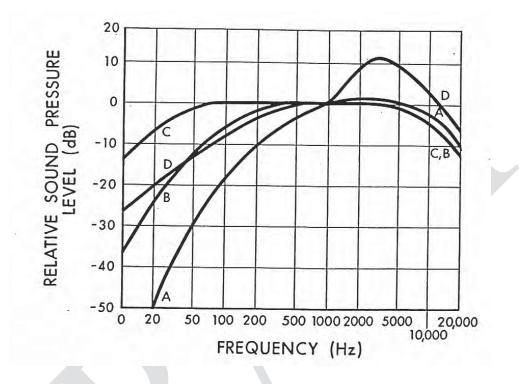
The range of frequencies audible to the human ear ranges from approximately 20 Hz to 20 kHz. Within this range, the human ear does not hear equally at all frequencies. It is not very sensitive to low frequency sounds, is very sensitive to mid frequency sounds and is slightly less sensitive to high frequency sounds. Due to the large frequency range of human hearing, the entire spectrum is often divided into 31 bands, each known as a 1/3 octave band.

The internationally agreed upon center frequencies and upper and lower band limits for the 1/1 (whole octave) and 1/3 octave bands are as follows:

	Whole Octave			1/3 Octave	
Lower Band	Center	Upper Band	Lower Ba		Upper Band
Limit	Frequency	Limit	Limit	Frequency	Limit
11	16	22	14.1	16	17.8
			17.8	20	22.4
			22.4	25	28.2
22	31.5	44	28.2	31.5	35.5
			35.5	40	44.7
			44.7	50	56.2
44	63	88	56.2	63	70.8
			70.8	80	89.1
			89.1	100	112
88	125	177	112	125	141
00			141	160	178
			178	200	224
177	250	355	224	250	282
			282	315	355
			355	400	447
355	500	710	447	500	562
			562	630	708
			708	800	891
710	1000	1420	891	1000	1122
			1122	1250	1413
			1413	1600	1778
1420	2000	2840	1778	2000	2239
			2239	2500	2818
			2818	3150	3548
2840	4000	5680	3548	4000	4467
			4467	5000	5623
			5623	6300	7079
5680	8000	11360	7079	8000	8913
			8913	10000	11220
			11220	12500	14130
11360	16000	22720	14130	16000	17780
			17780	20000	22390



Human hearing is most sensitive at approximately 3500 Hz which corresponds to the ¹/₄ wavelength of the ear canal (approximately 2.5 cm). Because of this range of sensitivity to various frequencies, we typically apply various weighting networks to the broadband measured sound to more appropriately account for the way humans hear. By default, the most common weighting network used is the so-called "A-weighting". It can be seen in the figure that the low frequency sounds are reduced significantly with the A-weighting.



Combination of Sounds

When combining multiple sound sources the general equation is:

$$\Sigma SPL_n = 10\log_{10} \left[\sum_{i=1}^n 10^{\frac{SPL_i}{10}} \right]$$

Examples:

- Two sources of 50 dB each add together to result in 53 dB.
- Three sources of 50 dB each add together to result in 55 dB.
- Ten sources of 50 dB each add together to result in 60 dB.
- One source of 50 dB added to another source of 40 dB results in 50.4 dB

It can be seen that, if multiple similar sources exist, removing or reducing only one source will have little effect.



Sound Level Measurements

Over the years a number of methods for measuring and describing environmental noise have been developed. The most widely used and accepted is the concept of the Energy Equivalent Sound Level (L_{eq}) which was developed in the US (1970's) to characterize noise levels near US Air-force bases. This is the level of a steady state sound which, for a given period of time, would contain the same energy as the time varying sound. The concept is that the same amount of annoyance occurs from a sound having a high level for a short period of time as from a sound at a lower level for a longer period of time. The L_{eq} is defined as:

$$L_{eq} = 10\log_{10}\left[\frac{1}{T}\int_{0}^{T}10^{\frac{dB}{10}}dT\right] = 10\log_{10}\left[\frac{1}{T}\int_{0}^{T}\frac{P^{2}}{P_{ref}^{2}}dT\right]$$

We must specify the time period over which to measure the sound. i.e. 1-second, 10-seconds, 15-seconds, 1-minute, 1-day, etc. An L_{eq} is meaningless if there is no time period associated.

In general there a few very common L_{eq} sample durations which are used in describing environmental noise measurements. These include:

- L_{eq}24 Measured over a 24-hour period
 - L_{eq} Night Measured over the night-time (typically 22:00 07:00)
 - L_{eq} Day Measured over the day-time (typically 07:00 22:00)
- L_{DN}
- Same as $L_{eq}24$ with a 10 dB penalty added to the night-time



Statistical Descriptor

Another method of conveying long term noise levels utilizes statistical descriptors. These are calculated from a cumulative distribution of the sound levels over the entire measurement duration and then determining the sound level at xx % of the time.

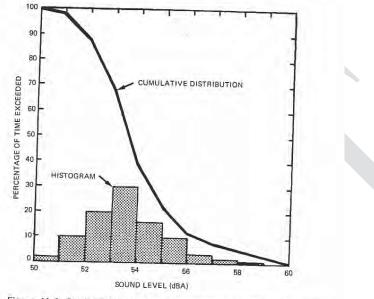


Figure 16.6 Statistically processed community noise showing histogram and cumulative distribution of A weighted sound levels.

Industrial Noise Control, Lewis Bell, Marcel Dekker, Inc. 1994

The most common statistical descriptors are:

L_{min}	- minimum sound level measured
L ₀₁	- sound level that was exceeded only 1% of the time
L ₁₀	- sound level that was exceeded only 10% of the time.
	- Good measure of intermittent or intrusive noise
	- Good measure of Traffic Noise
L ₅₀	- sound level that was exceeded 50% of the time (arithmetic average)
	- Good to compare to Leq to determine steadiness of noise
L ₉₀	- sound level that was exceeded 90% of the time
	- Good indicator of typical "ambient" noise levels
L99	- sound level that was exceeded 99% of the time
L _{max}	- maximum sound level measured

These descriptors can be used to provide a more detailed analysis of the varying noise climate:

- If there is a large difference between the L_{eq} and the L_{50} (L_{eq} can never be any lower than the L_{50}) then it can be surmised that one or more short duration, high level sound(s) occurred during the time period.
- If the gap between the L_{10} and L_{90} is relatively small (less than 15 20 dBA) then it can be surmised that the noise climate was relatively steady.



Sound Propagation

In order to understand sound propagation, the nature of the source must first be discussed. In general, there are three types of sources. These are known as 'point', 'line', and 'area'. This discussion will concentrate on point and line sources since area sources are much more complex and can usually be approximated by point sources at large distances.

Point Source

As sound radiates from a point source, it dissipates through geometric spreading. The basic relationship between the sound levels at two distances from a point source is:

$$\therefore SPL_1 - SPL_2 = 20\log_{10}\left(\frac{r_2}{r_1}\right)$$

Where:

: SPL₁ = sound pressure level at location 1, SPL₂ = sound pressure level at location 2 r_1 = distance from source to location 1, r_2 = distance from source to location 2

Thus, the reduction in sound pressure level for a point source radiating in a free field is **6 dB per doubling of distance**. This relationship is independent of reflectivity factors provided they are always present. Note that this only considers geometric spreading and does not take into account atmospheric effects. Point sources still have some physical dimension associated with them, and typically do not radiate sound equally in all directions in all frequencies. The directionality of a source is also highly dependent on frequency. As frequency increases, directionality increases.

Examples (note no atmospheric absorption):

- A point source measuring 50 dB at 100m will be 44 dB at 200m.
- A point source measuring 50 dB at 100m will be 40.5 dB at 300m.
- A point source measuring 50 dB at 100m will be 38 dB at 400m.
- A point source measuring 50 dB at 100m will be 30 dB at 1000m.

Line Source

A line source is similar to a point source in that it dissipates through geometric spreading. The difference is that a line source is equivalent to a long line of many point sources. The basic relationship between the sound levels at two distances from a line source is:

$$SPL_1 - SPL_2 = 10 \log_{10} \left(\frac{r_2}{r_1} \right)$$

The difference from the point source is that the '20' term in front of the 'log' is now only 10. Thus, the reduction in sound pressure level for a line source radiating in a free field is **3 dB per doubling of distance**.

Examples (note no atmospheric absorption):

- A line source measuring 50 dB at 100m will be 47 dB at 200m.
- A line source measuring 50 dB at 100m will be 45 dB at 300m.
- A line source measuring 50 dB at 100m will be 44 dB at 400m.
- A line source measuring 50 dB at 100m will be 40 dB at 1000m.



Atmospheric Absorption

As sound transmits through a medium, there is an attenuation (or dissipation of acoustic energy) which can be attributed to three mechanisms:

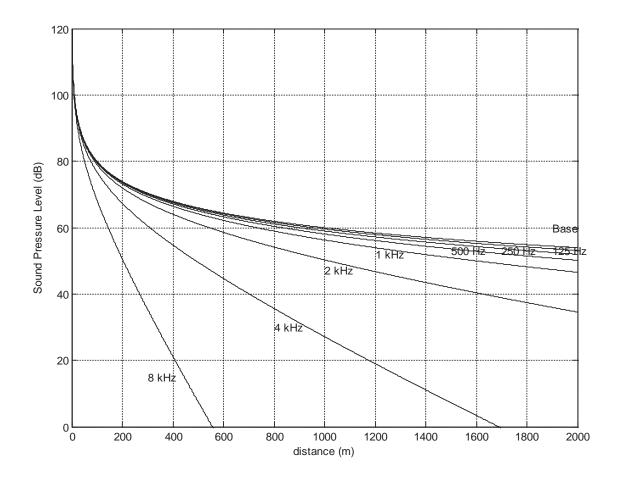
- 1) **Viscous Effects** Dissipation of acoustic energy due to fluid friction which results in thermodynamically irreversible propagation of sound.
- 2) **Heat Conduction Effects** Heat transfer between high and low temperature regions in the wave which result in non-adiabatic propagation of the sound.
- 3) **Inter Molecular Energy Interchanges** Molecular energy relaxation effects which result in a time lag between changes in translational kinetic energy and the energy associated with rotation and vibration of the molecules.

The following table illustrates the attenuation coefficient of sound at standard pressure (101.325 kPa) in units of dB/100m.

Temperature	Relative Humidity	Frequency (Hz)					
°C	(%)	125	250	500	1000	2000	4000
	20	0.06	0.18	0.37	0.64	1.40	4.40
30	50	0.03	0.10	0.33	0.75	1.30	2.50
	90	0.02	0.06	0.24	0.70	1.50	2.60
	20	0.07	0.15	0.27	0.62	1.90	6.70
20	50	0.04	0.12	0.28	0.50	1.00	2.80
	90	0.02	0.08	0.26	0.56	0.99	2.10
	20	0.06	0.11	0.29	0.94	3.20	9.00
10	50	0.04	0.11	0.20	0.41	1.20	4.20
	90	0.03	0.10	0.21	0.38	0.81	2.50
	20	0.05	0.15	0.50	1.60	3.70	5.70
0	50	0.04	0.08	0.19	0.60	2.10	6.70
	90	0.03	0.08	0.15	0.36	1.10	4.10

- As frequency increases, absorption tends to increase
- As Relative Humidity increases, absorption tends to decrease
- There is no direct relationship between absorption and temperature
- The net result of atmospheric absorption is to modify the sound propagation of a point source from 6 dB/doubling-of-distance to approximately 7 8 dB/doubling-of-distance (based on anecdotal experience)





Atmospheric Absorption at 10°C and 70% RH



Meteorological Effects

There are many meteorological factors which can affect how sound propagates over large distances. These various phenomena must be considered when trying to determine the relative impact of a noise source either after installation or during the design stage.

Wind

- Can greatly alter the noise climate away from a source depending on direction
- Sound levels downwind from a source can be increased due to refraction of sound back down towards the surface. This is due to the generally higher velocities as altitude increases.
- Sound levels upwind from a source can be decreased due to a "bending" of the sound away from the earth's surface.
- Sound level differences of ± 10 dB are possible depending on severity of wind and distance from source.
- Sound levels crosswind are generally not disturbed by an appreciable amount
- Wind tends to generate its own noise, however, and can provide a high degree of masking relative to a noise source of particular interest.

Temperature

- Temperature effects can be similar to wind effects
- Typically, the temperature is warmer at ground level than it is at higher elevations.
- If there is a very large difference between the ground temperature (very warm) and the air aloft (only a few hundred meters) then the transmitted sound refracts upward due to the changing speed of sound.
- If the air aloft is warmer than the ground temperature (known as an *inversion*) the resulting higher speed of sound aloft tends to refract the transmitted sound back down towards the ground. This essentially works on Snell's law of reflection and refraction.
- Temperature inversions typically happen early in the morning and are most common over large bodies of water or across river valleys.
- Sound level differences of ±10dB are possible depending on gradient of temperature and distance from source.

Rain

- Rain does not affect sound propagation by an appreciable amount unless it is very heavy
- The larger concern is the noise generated by the rain itself. A heavy rain striking the ground can cause a significant amount of highly broadband noise. The amount of noise generated is difficult to predict.
- Rain can also affect the output of various noise sources such as vehicle traffic.

<u>Summary</u>

- In general, these wind and temperature effects are difficult to predict
- Empirical models (based on measured data) have been generated to attempt to account for these effects.
- Environmental noise measurements must be conducted with these effects in mind. Sometimes it is desired to have completely calm conditions, other times a "worst case" of downwind noise levels are desired.



Topographical Effects

Similar to the various atmospheric effects outlined in the previous section, the effect of various geographical and vegetative factors must also be considered when examining the propagation of noise over large distances.

Topography

- One of the most important factors in sound propagation.
- Can provide a natural barrier between source and receiver (i.e. if berm or hill in between).
- Can provide a natural amplifier between source and receiver (i.e. large valley in between or hard reflective surface in between).
- Must look at location of topographical features relative to source and receiver to determine importance (i.e. small berm 1km away from source and 1km away from receiver will make negligible impact).

Grass

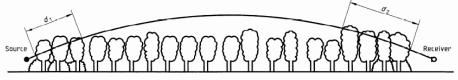
- Can be an effective absorber due to large area covered
- Only effective at low height above ground. Does not affect sound transmitted direct from source to receiver if there is line of sight.
- Typically less absorption than atmospheric absorption when there is line of sight.
- Approximate rule of thumb based on empirical data is:

$$A_g = 18\log_{10}(f) - 31$$
 (*dB*/100*m*)

Where: A_g is the absorption amount

Trees

- Provide absorption due to foliage
- Deciduous trees are essentially ineffective in the winter
- Absorption depends heavily on density and height of trees
- No data found on absorption of various kinds of trees
- Large spans of trees are required to obtain even minor amounts of sound reduction
- In many cases, trees can provide an effective visual barrier, even if the noise attenuation is negligible.



NOTE — $d_f = d_1 + d_2$

For calculating d_1 and d_2 , the curved path radius may be assumed to be 5 km.

Figure A.1 — Attenuation due to propagation through foliage increases linearly with propagation distance $d_{\rm f}$ through the foliage

Table A.1 — Attenuation of an octave band of noise due to propagation a distance $d_{\rm f}$ through dense foliage

Propagation distance d _f	Nominal midband frequency							
		Hz						
m	63	125	250	500	1 000	2 000	4 000	8 000
	Attenuati	on, dB:						
$10 \le d_{\rm f} \le 20$	0	0	1	1	1	1	2	3
	Attenuati	on, dB/m:						
$20 \le d_{\rm f} \le 200$	0,02	0,03	0,04	0,05	0,06	0,08	0,09	0,12

Tree/Foliage attenuation from ISO 9613-2:1996



Bodies of Water

- Large bodies of water can provide the opposite effect to grass and trees.
- Reflections caused by small incidence angles (grazing) can result in larger sound levels at great distances (increased reflectivity, Q).
- Typically air temperatures are warmer high aloft since air temperatures near water surface tend to be more constant. Result is a high probability of temperature inversion.
- Sound levels can "carry" much further.

Snow

- Covers the ground for approximately 1/2 of the year in northern climates.
- Can act as an absorber or reflector (and varying degrees in between).
- Freshly fallen snow can be quite absorptive.
- Snow which has been sitting for a while and hard packed due to wind can be quite reflective.
- Falling snow can be more absorptive than rain, but does not tend to produce its own noise.
- Snow can cover grass which might have provided some means of absorption.
- Typically sound propagates with less impedance in winter due to hard snow on ground and no foliage on trees/shrubs.



Appendix III SOUND LEVELS OF FAMILIAR NOISE SOURCES

Used with Permission Obtained from ERCB Guide 38: Noise Control Directive User Guide (February 2007)

Source¹

Sound Level (dBA)

Bedroom of a country home	30
Soft whisper at 1.5 m	30
Quiet office or living room	40
Moderate rainfall	50
Inside average urban home	50
Quiet street	50
Normal conversation at 1 m	60
Noisy office	60
Noisy restaurant	70
Highway traffic at 15 m	75
Loud singing at 1 m	75
Tractor at 15 m	78-95
Busy traffic intersection	80
Electric typewriter	80
Bus or heavy truck at 15 m	88-94
Jackhammer	88-98
Loud shout	90
Freight train at 15 m	95
Modified motorcycle	95
Jet taking off at 600 m	100
Amplified rock music	110
Jet taking off at 60 m	120
Air-raid siren	130

¹ Cottrell, Tom, 1980, *Noise in Alberta*, Table 1, p.8, ECA80 - 16/1B4 (Edmonton: Environment Council of Alberta).



SOUND LEVELS GENERATED BY COMMON APPLIANCES

Used with Permission Obtained from ERCB Guide 38: Noise Control Directive User Guide (February 2007)

Source ¹	Sound level at 3 feet (dBA)	
Freezer	. 38-45	
Refrigerator	34-53	
Electric heater	47	
Hair clipper	50	
Electric toothbrush	. 48-57	
Humidifier	41-54	
Clothes dryer	51-65	
Air conditioner	. 50-67	
Electric shaver	47-68	
Water faucet	62	
Hair dryer	. 58-64	
Clothes washer	. 48-73	
Dishwasher	. 59-71	
Electric can opener	. 60-70	
Food mixer	. 59-75	
Electric knife	65-75	
Electric knife sharpener	72	
Sewing machine	. 70-74	
Vacuum cleaner	65-80	
Food blender	65-85	
Coffee mill	. 75-79	
Food waste disposer	. 69-90	
Edger and trimmer	81	
Home shop tools	64-95	
Hedge clippers	85	
Electric lawn mower	. 80-90	

¹ Reif, Z. F., and Vermeulen, P. J., 1979, "Noise from domestic appliances, construction, and industry," Table 1, p.166, in Jones, H. W., ed., Noise in the Human Environment, vol. 2, ECA79-SP/1 (Edmonton: Environment Council of Alberta).





Conceptual Bridge Planning Report &

Additional Communications



Conceptual Bridge Planning Report

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Conceptual Bridge Planning Report

Wedgewood Creek Crossing on 199 Street NW in the City of Edmonton

May 9, 2014

Prepared for:





Terrace Engineering Ltd.

Introduction

The overall project involves roadway planning for an upgrade to 199 Street NW in the City of Edmonton in support of a proposed subdivision development by Walton Development and Management, Qualico Communities and Melcor in the area to the south of Wedgewood Creek. For this project Terrace Engineering Ltd. (Terrace) has been retained by CIMA+ to explore conceptual planning for replacement of the existing bridge culvert carrying Wedgewood Creek under 199 Street NW. Terrace has not yet visited the crossing site. Much of the existing site information is derived in part from a report by Golder Associates entitled "Erosion Study of Wedgewood Creek at Edmonton", dated December 2012.

Existing Bridge Culvert

Based on Alberta Transportation infrastructure records, the existing main culvert structure is a 1.8 metre diameter structural plate culvert with a 62.8 metre length built in 1952 and modified in 1968. Based on survey information provided to us by CIMA+, the roadway has an 8 metre clear roadway located about 10 metres above the stream. According to the Golder report referenced in the Introduction, there is also a 1.05 metre diameter overflow culvert located 6 metres above the streambed. The report further identifies that the main culvert has been caged with light mesh to try and address drift and beaver activity concerns. Based on photos and text in the Golder report, the cage is heavily damaged at the culvert inlet and there is a large debris field surrounding the cage. The photos of the outlet show an unsupported hanging culvert outlet bevel, with the bottom of the culvert about a foot above the downstream water level. Based on the age of the culvert, it is expected that the culvert would be replaced at the time of roadway improvements.

Golder Report Information and Recommendations Applicable to 199 Street Crossing

The Golder report carried out an extensive review of Wedgewood Creek within the City of Edmonton. The executive summary and main body of the Golder report identified a number of issues that are relevant to the crossing at 199 Street and many of these are described herein.

Wedgewood Creek is a typical North Saskatchewan River tributary that has its headwaters in the tablelands and then transitions to a deeply incised ravine as it flows towards the river. The Golder report identifies a gross drainage area of 170 km² for Wedgewood Creek. There are crossings of Wedgewood Creek on 215 Street, 199 Street, Anthony Henday Drive (AHD) and 184 Street (pedestrian) within the City. With the exception of the 3 span bridges at AHD, these crossings consist of smaller diameter culverts, with 1.8 metre diameter culverts at 215 and 199 Streets and twin 2 metre diameter culverts at 184 Street. Preliminary hydrotechnical investigations by Golder suggest that these existing culvert crossings are undersized for a design flood event, although it is indicated that additional work is required to determine a more accurate

design flood discharge before this can be established with certainty. A brief exploration of the hydrotechnical design criteria noted in the Golder report was carried out by Terrace. An examination of the stream characteristics, such as bank height and channel width, as well as a consideration of the stream and culvert conditions at the crossings would suggest that the design flood values stated in the Golder report may be excessively conservative. For purposes of this report, it is assumed that a slightly larger culvert diameter than exists today would likely meet the hydrotechnical needs of the stream. This will need to be verified during detailed design.

However, in contrast to the above, the Golder report recommends that the culvert sizes remain unchanged to continue to provide a benefit to the ecosystem of the valley by providing flow attenuation and sediment retention. To address flow capacity issues, Golder is recommending the use of high elevation bypass culvert(s) to avoid overtopping of the roadway. This concept needs to be given further consideration before implementation as flow hydraulic issues and the culvert fill erosion that would likely occur with high level overflow culvert openings may not be desirable for 1:100 year design flow conditions. A more robust examination of design flow requirements and the resulting design flow value is required to fully assess the overflow culvert concept.

When Golder explored the Wedgewood Creek valley they encountered very high beaver activity levels and strongly recommended support for continued beaver activity. This is somewhat in conflict with the ability of a culvert to function as a conduit for both normal flows and extreme flows of Wedgewood Creek under the roadway. The current culvert inlet is screened to try and keep beaver dams and drift accumulation from blocking the entrance to the culvert, but the existing system is damaged. A more robust drift block cage should be considered if any work is carried out at this crossing so as to preserve the flow capacity of the culvert. We would also recommend that strong consideration be given to removing drift and beaver dam structures at the culvert inlet as a regular maintenance activity to allow the culvert to adequately pass flows under the roadway.

Wildlife Passage

It has been identified by others that wildlife passage opportunities under 199 Street will be a necessary component of any upgrading of 199 Street across the Wedgewood Creek valley. Based on a brief discussion with Bill Harper, Senior Wildlife Biologist with Stantec, it is our understanding that the focal wildlife species is white-tailed deer. He has provided some comments to Terrace and these are as follows:

- The City of Edmonton (2010) includes white-tailed deer as part of the "large terrestrial design group" in their wildlife passage engineering design guidelines. Recommendations for minimum wildlife crossing structure dimensions for large terrestrials is 6 m x 2.4 m, (w x h) or 3.1 m x 3.1 m, with openness index of 1.5 or higher. The openness ratio is

calculated by Structure Openness Ratio = (Opening Height x Width)/Length.

- Install wildlife fencing (2.4 m high) to reduce wildlife-vehicle collisions and encourage wildlife use of the structure
- Maximize natural light, but avoid artificial lighting near structure entrances
- Human use reduces animal use, so avoid human trails through crossing structure or separate human trails from wildlife pathways.
- Reduce traffic noise inside structure and at structure entrances

Obviously an open bridge type structure can be easily designed to accommodate wildlife passage in addition to stream flows. However, this is more challenging when a very long culvert structure is required for the stream flows. Based on a brief review by Terrace, it appears that a reasonable and cost effective option to handle wildlife passage for the culvert option is to consider utilizing a separate structure for wildlife located just below the roadway surface so as to reduce overall structure length and maximize the openness.

Geotechnical Considerations

The 199 Street crossing is located across a deeper incised valley carrying Wedgewood Creek. These types of valley crossings often have geotechnical issues and considerations that affect the size and length of bridge and culvert structures, and may affect the type of structure recommended for the crossing. During our review of the site, there appears to be a possibility that a surface slide affected the sideslope of the existing culvert embankment at some point in its life. It is recommended that a geotechnical engineering study be undertaken to identify and quantify the geotechnical issues that may affect the crossing alternatives. This study should identify areas of geotechnical concern and provide reasonable assumptions for embankment slopes that can be considered for different crossing alternatives at the preliminary stage. This study should also identify future work that would be required to confirm and refine the geotechnical input that may be required for replacement and/or modifications to the crossing. In the absence of such a study, fill slopes of 3H:1V will be used to assess conceptual options with the understanding that geotechnical advise and direction will be utilized by the project proponent at a later date.

Roadway Improvement Options

The roadway improvements being developed by CIMA+ will bring the existing two lane rural roadway to a four lane divided urban arterial standard. In addition, a multi-use trail is proposed for the west side of the roadway, with a standard sidewalk on the east side. Improvements to the vertical curvature of the roadway are being considered that would raise the roadway one to two metres higher and improve the sag curve through the valley.

Wedgewood Creek Crossing Options

Several options for the crossing were considered and these options needed to address both Wedgewood Creek flows as well as wildlife passage. In general there are three types of solutions that have been identified:

- Bridge structure with or without large abutment walls
- Oversized culvert structure suitable for wildlife passage in addition to stream flows
- Culvert sized only for stream flows and a separate wildlife passage structure

The bridge structure concept has a number of issues which affect the practicality of this structure type. The high fill height results in a very long bridge, and the very large skew between the roadway alignment and the creek valley alignment makes the bridge even longer. The geotechnical stability of the valley may affect the design of the headslope and/or retaining walls and affect the size of the bridge. In addition, the Golder report recommended a culvert type structure to provide flow attenuation and sediment retention, which is not achieved with a bridge. One of the largest concerns affecting the practicality is the cost of implementing this type of solution, with <u>additional costs</u> in the order of \$18 million compared to other feasible options.

For a bridge option, using large abutment walls or a normal headslope configuration is something that will need to be determined during more detailed design. For costing purposes at this conceptual stage a unit cost multiplied by the out to out of fills and the overall width of the bridge structure will give a representative cost. Details are as follows:

- $$5500/m^2$ unit cost for high bridge
- 3:1 headslopes, a 5 m bedwidth, a 6 m wildlife passageway, an average deck height of 13.5 m and a skew of 40 degrees results in an out to out of fills of 120 m
- bridge width comprises of 20.9 of roadway width, a 1.5 m sidewalk, a 4.2 m multi-use trail width (incorporating 0.6 m shy to barriers) and 4 barriers with a width of 0.5 m each resulting in an overall width of 28.6 m
- allocation of \$0.2 million for removal of the existing culvert structure
- cost allowance for contingencies and engineering set at 30% additional

Thus the conceptual bridge cost is estimated to be in the order of **\$25 million**.

An oversized culvert option will also have a large cost component due to its size and length. A typical culvert with the roadway fills sloping down to the bottom of the valley is not really practical for wildlife passage due to the length of culvert through which the wildlife will need to travel. A 150 m long culvert would require an opening of 45 m wide by 5 m high to achieve the required openness ration, which is not practical. Building retaining walls to shorten the culvert sufficiently for wildlife passage is likely not feasible due to geotechnical stability and cost issues. This option is not considered further within this report.

The conceptual option which shows the most promise is the use of a culvert that is sized for stream flows, with a separate wildlife passage structure higher up on the slope. The stream culvert would be built to the skew of the valley and the wildlife passageway would be built square to the roadway so as to minimize the length of structure through which wildlife must pass. The wildlife passage structure could be either a bridge type structure or a box culvert type structure. This option is explored in more detail following and is shown conceptually on Figures 1 and 2.

In order to develop this concept a number of assumptions needed to be made. Firstly it was assumed that 3:1 sideslopes are geotechnically feasible for the culvert. It was also assumed that a 2.4 m diameter culvert is sufficiently large to ensure flow capacity. Thirdly it was assumed that the use of some sort of debris catcher at the culvert inlet, combined with regular drift and beaver dam removal at the inlet, would be provided so as to maintain flow capacity. Fourthly it was assumed that a separate underpass structure located higher up on the slope would meet the needs for wildlife passage and that it would need to be quite large to meet the openness ratio requirements.

For costing purposes at this conceptual stage, the wildlife passage bridge cost can be determined using a unit cost multiplied by the out to out of fills and the overall width of the bridge structure. The stream culvert can be determined using a unit cost multiplied by the circumference and length to develop a representative cost. Details are as follows:

- \$4500/m² unit cost for simple passageway bridge
- bridge width comprises of 20.9 of roadway width, a 1.5 m sidewalk, a 4.2 m multi-use trail width (incorporating 0.6 m shy to barriers) and 4 barriers with a width of 0.5 m each resulting in an overall width of 28.6 m
- 2:1 headslopes, an average deck height of 5 m (3.5m opening height), a 6 m bottom width (average 13 m wide opening at mid-height) results in an out to out of fills of 26 m and an opening ratio of 1.6
- wildlife bridge cost without contingency is \$3.35 million
- $\$800/m^2$ unit cost for culvert under high fill, excluding fill cost
- 2.4 m diameter SPCSP culvert (7.5 m circumference)
- 150 m culvert length along 45 degree skew
- stream culvert cost without contingency \$0.9 million
- allocation of \$0.2 million for removal of the existing culvert structure
- allocation of \$0.3 million for fill and road work above culvert
- allocation of \$0.2 million for additional environmental mitigation
- allocation of \$0.1 million for drift catcher and riprap
- cost allowance for contingencies and engineering set at 30% additional

Thus the option with a culvert and separate wildlife passageway structure is estimated to cost in the order of **\$7 million**.

These order of magnitude cost estimates are highly dependent upon site specific bridge/culvert geotechnical input, which has not yet been carried out. Obtaining such input will greatly assist in refining the configuration and cost.

Next Steps

This conceptual Bridge Planning Report is intended to assist in the development of an acceptable solution for crossing Wedgewood Creek and the valley. It is preliminary in nature and is subject to change and refinement as the design work progresses. Upon acceptance or refinement of the conceptual design, additional engineering work should be undertaken to design the crossing including geotechnical and hydrotechnical studies.

Closure

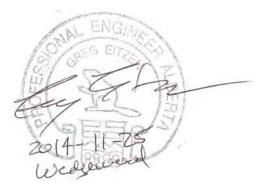
This study has been prepared exclusively for CIMA+ for the Conceptual Bridge Planning associated with the Wedgewood Creek Crossing on 199 Street NW in the City of Edmonton. The information and data contained herein represent our professional judgement in light of the knowledge and information available to us at the time of preparation. The information in this report is conceptual and preliminary in nature. It is therefore subject to change and refinement as the design work progresses and should not be relied upon without additional engineering design.

Except as required by law, this study and the information and data contained herein are to be treated as confidential and may be used and relied upon only by the client, who is restricted to using this information only for the purpose for which it was intended. We deny any liability whatsoever to other parties who may obtain access to this study for any injury, loss or damage suffered by such parties arising from their use of, or reliance upon, this study or any of its contents. Any use of this study by third parties, or any reliance or decisions based on it, are the responsibility of such third parties.

Respectfully submitted,

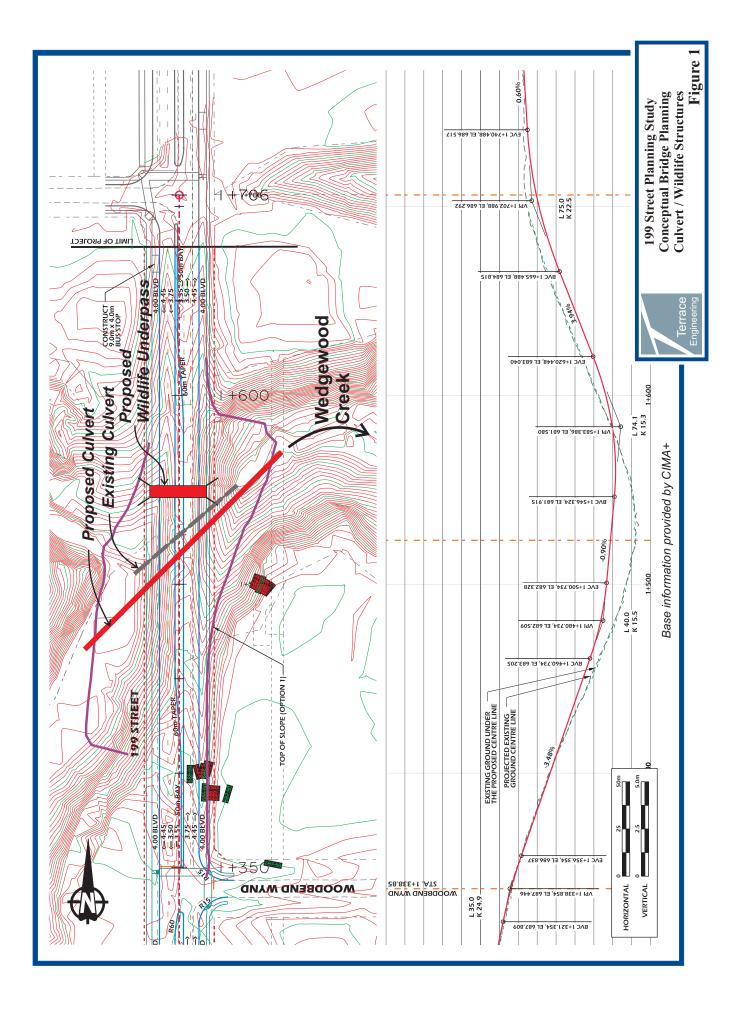
Terrace Engineering Ltd.

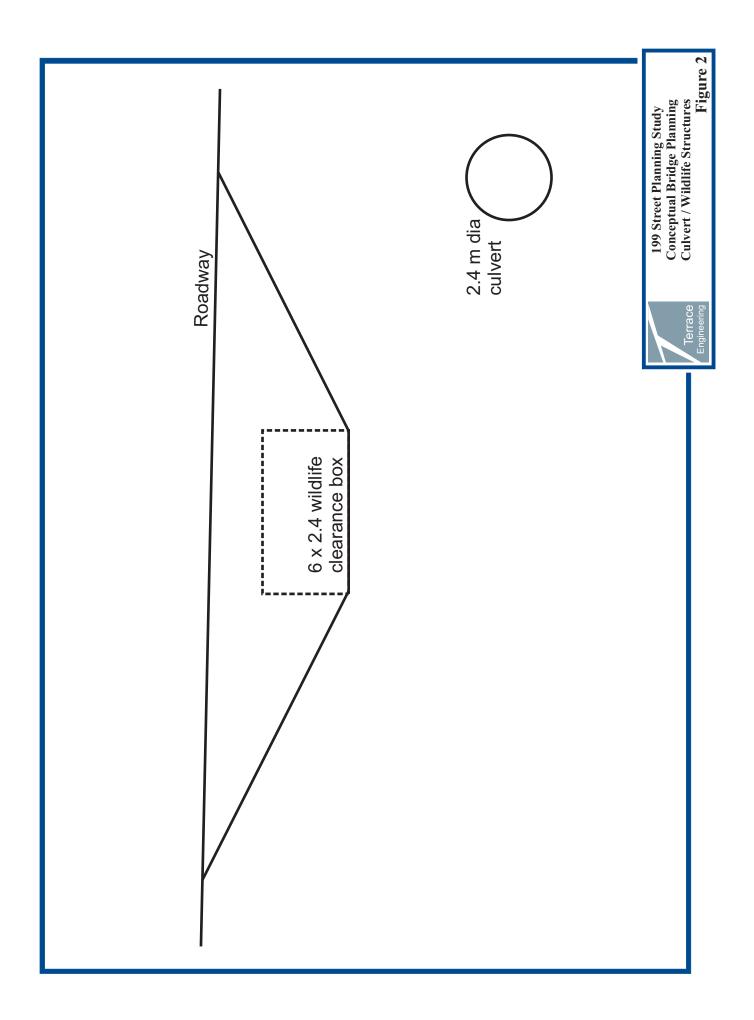
Permit to Practice Number: P 6715



Submitted in draft form: May 9, 2014 Finalized without modification: November 25, 2014

Conceptual Bridge Planning Report - Wedgewood Creek Crossing on 199 Street NW Terrace Engineering Ltd., May 9, 2014 **FIGURES**





Additional Communications

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Wildlife Passage Design Recommendations— 199 Street Widening Project Within the Riverview Neighborhood



Prepared for: Riverview Owners Group (Qualico Communities, Walton Development and Management LP, Melcor Developments Ltd, and Sunwapta Holdings Corporation)

Prepared by: William L. Harper, R.P.Bio.

May 20, 2014

Table of Contents

1.0	BACKGROUND	1
2.0	PROPOSED LOCATION OF THE 199 STREET WILDLIFE CROSSING STRUCTURES	1
3.0	OBJECTIVES	2
4.0	METHODS	2
5.0	WILDLIFE SPECIES PRESENT AND ECOLOGICAL DESIGN GROUPS	
5.1	FISH AND WILDLIFE PRESENT IN THE PROJECT AREA	2
5.2	ECOLOGICAL DESIGN GROUPS	3
6.0	WILDLIFE PASSAGE DESIGN RECOMMENDATIONS	4
6.1	LARGE AND MEDIUM TERRESTRIAL WILDLIFE BELOW-GRADE CROSSING	
	STRUCTURE: TYPE, SIZE AND LOCATION	4
6.2	SMALL TERRESTRIAL AND AQUATIC WILDLIFE BELOW-GRADE CROSSING	
	STRUCTURE: TYPE, SIZE AND LOCATION DESIGN	5
6.3	DETAILED DESIGN	6
7.0	RECOMMENDATIONS FOR REDUCING BIRD AND BAT VEHICLE COLLISION	
	RISK	7
8.0	CLOSURE	8
9.0	REFERENCES	9

LIST OF FIGURES

Figure 1	Proposed Location for the Wildlife Crossing Structures	2
Figure 2	Conceptual Design of Wildlife Crossing Structure at Wedgewood Creek	5

LIST OF APPENDICES

Appendix A Fish and Wildlife Species Summary Report (AESRD 2014)



Background May 20, 2014

1.0 BACKGROUND

Stantec Consulting Ltd. (Stantec) was retained by Riverview Owners Group (the Client) to provide environmental consulting services and recommendations for wildlife passage as part of the 199 Street Widening within the Riverview Neighbourhood 2 (the project). In an effort to minimize the impacts on wildlife movement from transportation infrastructure, the City of Edmonton commissioned the development of the Wildlife Passage Engineering Design Guidelines (WPEDG) (City of Edmonton 2010). The objective of these guidelines is to reduce human-wildlife conflict through improved awareness, safety, and collision reduction while also aiding in the maintenance of habitat connectivity and reduced genetic isolation.

The 199 Street Concept Planning Report determined that 22% of all vehicle collisions and 30% of collisions at midblocks (between intersections) were animal-vehicle collisions (CIMA 2014). These were attributed to the presence of white-tailed deer in the project area and the lack of wildlife passage across 199 Street at the Wedgewood Ravine (CIMA 2014).

As part of the Riverview Neighbourhood 2 development, 199 Street will be widened. The widened road, along with projected increases in traffic volume and vehicle speed, will increase the barrier effect of the road on wildlife. For these reasons, and to reduce animal-vehicle collisions, provisions for a wildlife crossing structure were considered.

2.0 PROPOSED LOCATION OF THE 199 STREET WILDLIFE CROSSING STRUCTURES

To support the development of residential neighbourhoods, 199 Street will be widened. Wildlife passage will be required as part of the road design to maintain permeability for wildlife movements.

Within the project area, 199 Street NW bisects Wedgewood Ravine approximately 150 m south of 35 Avenue (Figure 1). Wedgewood Ravine is a major ecological feature that provides both key habitat for many wildlife species and important corridors and linkages to adjacent agricultural areas, wetlands, Natural Areas, and Environmentally Sensitive Area (Ecoventure 2013).

The proposed location for the wildlife crossing structures (Figure 1) was identified as a potential location for a wildlife crossing in the Ecological Network Report (Ecoventure 2013). This ravine was also identified as a suitable location for wildlife crossing structures based on preliminary engineering considerations (Greg Eitzen, Terrace Engineering, pers. comm., 5 February 2014).



Objectives May 20, 2014

3.0 **OBJECTIVES**

Stantec understands that the City of Edmonton has requested specific details pertaining to wildlife passage associated with the Project at the concept stage to allow for early planning and incorporation of the ecological features into the ultimate design. In that context, the objectives of this report are:

- To identify wildlife that are present or likely to occur in the area
- To categorize wildlife in the area according to the Ecological Design Groups (EDGs) outlined in the WPEDG
- To identify target EDGs for wildlife passage mitigation
- To provide recommendations to mitigate the potential adverse effects to wildlife passage resulting from the Project

4.0 METHODS

Identification of wildlife present or likely to occur in the project area was based the Riverview Ecological Network Report (Ecoventure 2013), a search of the Fisheries and Wildlife Management Information System (FWMIS) database, and a wildlife snow-tracking survey (Stantec 2014). The wildlife species known or likely to occur in the area were then assigned to EDGs. Consistent with the WPEDG, the EDGs identified for the project area were then assessed to identify appropriate measures to mitigate adverse effects of widening 199 Street in the project area.

5.0 WILDLIFE SPECIES PRESENT AND ECOLOGICAL DESIGN GROUPS

5.1 FISH AND WILDLIFE PRESENT IN THE PROJECT AREA

A search of the FWMIS database (AESRD 2014) was performed on May 19, 2014, to identify previously recorded species occurrences in the vicinity of the project area. The search was conducted using a maximum 2 km radius from the proposed wildlife crossing. The results of an electrofishing survey of Wedgewood Creek are available for a location approximately 1800 m northeast of the project area (AESRD 2014). Two fish species, brook stickleback (*Culaea inconstans*) and fathead minnow (*Pimephales promelas*) were confirmed in Wedgewood Creek downstream of the project area in 2009 (Appendix A). No wildlife inventory records were identified within 2 km of the proposed wildlife crossing.





Wildlife Species Present and Ecological Design Groups May 20, 2014

A wildlife snow-tracking survey conducted four kilometres south of Wedgewood Creek in March 2014 (Stantec 2014) identified six species of wintering mammals in the Project area: white-tailed deer (*Odocoileus virginianus*), coyote (*Canis latrans*), red fox (*Vulpes vulpes*), least weasel (*Mustela nivalis*), snowshoe hare (*Lepus americanus*), and red squirrel (*Tamiasciurus hudsonicus*). Sets of deer tracks were the most abundant (n = 78), followed by snowshoe hare (n = 73), coyote (n = 41), red squirrel (n = 8), red fox (n = 3), unspecified microtine (voles, shrews and mice, n = 3), and least weasel (n = 3) (Stantec 2014).

5.2 ECOLOGICAL DESIGN GROUPS

EDGs are groupings of species that share characteristics that should be taken into account in wildlife passage planning and design. There are 11 EDGs: Large Terrestrial, Medium Terrestrial, Small Terrestrial, Amphibians, Aerial Mammals, Aquatic Species, Scavenger Birds, Birds of Prey, Water Birds, Ground Dwelling Birds, and Other Birds (City of Edmonton 2010).

The Ecological Network Report (Ecoventure 2013) identified a number of wildlife species likely to occur in association with the aspen and willow communities present in the project area (e.g., red-tailed hawk (*Buteo jamaicensis*), least flycatcher (*Empidonax minimus*), Baltimore oriole (*Icterus galbula*), red-eyed vireo(*Vireo olivaceus*), yellow warbler(*Dendroica petechia*), white-tailed deer, snowshoe hare, northern pocket gopher (*Thomomys talpoides*), and North American porcupine (*Erethizon dorsatum*). Based on this information, the FWMIS search, and the wildlife snow-tracking survey, one or more species within all 11 EDGs are predicted to occur in the project area.

Passage requirements for the Large Terrestrial, Medium Terrestrial, and Small Terrestrial EDGs are addressed in a below-grade dry culvert (Section 6.1). Passage requirements for the Medium Terrestrial, Small Terrestrial, Amphibian, and Aquatic Species EDGs are addressed in a modified drainage culvert (Section 6.2). Passage requirements for the Aerial Mammals, Scavenger Birds, Birds of Prey, Ground Dwelling Birds, Water Birds and Other Birds EDGs are addressed abovegrade in the Recommendations for Reducing Bird and Bat Vehicle Collision Risk (Section 7.0).



Wildlife Passage Design Recommendations May 20, 2014

6.0 WILDLIFE PASSAGE DESIGN RECOMMENDATIONS

Based on the WPEDG and the EDGs, it was identified that two below-grade crossing structures would be required for this area to accommodate terrestrial EDGs. A relatively large openbottom arch culvert is proposed to accommodate the Large and Medium Terrestrial EDGs and a modified drainage culvert is proposed to accommodate the other terrestrial and aquatic EDGs. The smaller culvert would also accommodate water drainage from the Wedgewood Creek under 199 Street.

6.1 LARGE AND MEDIUM TERRESTRIAL WILDLIFE BELOW-GRADE CROSSING STRUCTURE: TYPE, SIZE AND LOCATION

Based on the WPEDG and the EDGs identified for the project area, a below-grade crossing will be required to accommodate Large Terrestrials EDG species (particularly white-tailed deer). A wildlife crossing structure designed for Large Terrestrial species will also accommodate species in the Medium Terrestrial and Small Terrestrial EDGs.

For the Large Terrestrials EDG, open bottom culverts are preferred over closed bottom culverts because species in this EDG prefer large open structures (City of Edmonton 2010). Open bottom culverts also maintain the existing soil surface. For this project, an open bottom arch dry culvert separate from the drainage culvert (see Section 6.2) is recommended since it can provide a large open structure with reduced length as it can be located higher on the fill slope to better accommodate white-tailed deer that are common in the project area.

An analysis of the effectiveness of wildlife crossing structures in Utah suggests they should be designed to be as short as possible. Schwender (2013) found that within a multivariate regression model, culvert length outperformed all other parameters, and culvert width and length together were the best predictors of successful mule deer passage. Cramer (2012) felt that when considering the metrics of wildlife crossing design, length was the most important factor, followed by width, and height was the least important consideration. Based on this analysis, Cramer (2012) recommended keeping wildlife underpasses under 37 m long.

Although measures of a structure's width, height and length are important considerations in designing wildlife structures, Clevenger and Huijser (2011) do not recommend the use of an openness index during planning and design. They believe that underpass dimensions should be used in conjunction with other structural and environmental factors when designing appropriate wildlife crossing structures.

The 199 Street Concept Planning Report recommend designing a "structure for wildlife located just below the roadway surface so as to reduce overall structure length and maximize the openness" (Appendix G in CIMA 2014). The current conceptual design proposes an open bottom culvert 6 m x 4 m x 65 m (width x height x length) (Figure 2; CIMA 2014). As proposed this



Wildlife Passage Design Recommendations May 20, 2014

design is likely too long to allow effective passage of Large Terrestrials EDGs (e.g., white-tailed deer).

The length of the crossing structure should be shortened to facilitate its use by Large Terrestrial wildlife species. The length of the structure could be addressed in a number of ways, including:

- adjusting the position of the structures so it crosses the roadway at right angles
- divide the roadway and construct two shorter crossing structures
- increasing the use of wing-walls

Culvert length has been shown to be the strongest predictor for deer use of underpasses (Schwender 2013; Clevenger and Waltho 2005). Although wildlife crossing structures with smaller openings (6 m wide x 3.4 m high) have been found to be effective for mule deer (*Odocoileus hemionus*) in Wyoming, these structures were only 18 m long (Sawyer and LeBeau 2011).

Clevenger and Huijser's (2011) general guidelines recommend a width of >12 m and height of >4.5 m for large mammal underpasses. Preliminary design of this crossing structure should consider increasing the opening dimensions to these recommended dimensions to better address the long length of this structure.

To facilitate deer passage, approaches to both entrances should not exceed a 1:3 slope.

6.2 SMALL TERRESTRIAL AND AQUATIC WILDLIFE BELOW-GRADE CROSSING STRUCTURE: TYPE, SIZE AND LOCATION DESIGN

Based on the WPEDG and the EDGs identified for the project area, an additional below-grade crossing in conjunction with the drainage culvert will be required to accommodate Small Terrestrial, Amphibian, and Aquatic Species in the project area.

The 199 Street Concept Planning Report assumes "a slightly larger culvert diameter than exists today would likely meet the hydrotechnical needs of the stream" (CIMA 2014). Preliminary and detailed designs also need to address the passage needs for fish, amphibian and small terrestrial mammal using Wedgewood Creek.





Wildlife Passage Design Recommendations May 20, 2014

Installation of an appropriately-sized concrete box or round culvert is recommended in order to be consistent with other similar crossings completed within the City of Edmonton. This structure will conform to Kintsch and Cramer's (2011) "Class 1 Small Underpass", which includes drainage culverts. According to their system, this type of culvert has the potential to provide passage for the species movement guilds that include the target EDGs at this site, Small Terrestrial, Amphibians and Aquatic Species. This type of structure is considered to be adequate to allow passage of small-sized animals (City of Edmonton 2010; Clevenger and Huijser 2011; Phillips et al. 2012).

Aquatic Species EDGs are particularly sensitive to poorly designed crossing structures (City of Edmonton 2010). Issues of increased water velocity and poorly embedded structures can create a barrier to upstream movement of aquatic species. The concrete box structure should be sized and positioned appropriately to minimize flow velocities, avoid confining the channel, and be sufficiently embedded in the stream channel to provide a natural substrate at the bottom of the culvert.

The concrete box structure has an advantage over round culverts since it can be more easily modified with the addition of raised platforms to allow "dry passage" of wildlife when water is flowing in the culvert. There are also options for installation of shelves in round culverts that will allow "dry passage" of small mammals.

6.3 DETAILED DESIGN

The recommended wildlife passage design for 199 Street at Wedgewood Creek includes construction of two new below-grade crossing structures for terrestrial EDGs. As this project is just at the concept design stage, specific recommendations pertaining to wildlife passage measures and other general mitigation measures are provided below but will likely need to be refined at the detailed design stage.

- The large below-grade crossing should be designed for the largest of the Large Terrestrials EDG, in this case white-tailed deer. By designing for this group, the majority of the other EDGs should be able to use the crossing.
- The small below-grade crossing should address the fish passage needs by 1) minimizing flow velocities, 2) avoiding channel confinement, and 3) being sufficiently embedded in the stream channel to provide a natural substrate and prevent culvert perching.
- The small below-grade crossing should be modified with the addition of raised platforms to allow for dry passage of small-sized animals when water is flowing through the culvert.
- Natural substrate and native vegetation should be present at the approaches to both wildlife crossing structures. These will create a more natural appearance around the structure and, for smaller EDGs, provide security cover from predators. Rip-rap used at the entrances of the drainage culvert should be the smallest possible to prevent erosion. Debris grates should not be installed.



Recommendations for Reducing Bird and Bat Vehicle Collision Risk May 20, 2014

- Wildlife exclusion fencing should be considered in the area of the ravine, both to encourage wildlife use of the crossing structures, and to mitigate wildlife-vehicle collisions should this become an issue.
- Wildlife-friendly lighting with reduced spill and glare should be incorporated in the final design of the road. Street lighting design should avoid illuminating the entrances of the wildlife crossing structures and nearby natural features.

7.0 RECOMMENDATIONS FOR REDUCING BIRD AND BAT VEHICLE COLLISION RISK

For the avian and Aerial Mammals (i.e., bat) EDGs, it is recommended that diversionary methods be incorporated to direct the flight of the birds and bats up and over the road as these species rarely use below grade crossing structures. The following above-grade mitigation measure is recommended to reduce the risk of collisions between vehicles and the Aerial Mammals, Scavenger Birds, Birds of Prey, Water Birds and Other Birds EDGs as they fly over 199 Street:

• Use natural vegetation and tree plantings to direct the flight paths of birds and bats higher over the road, above the traffic (Tremblay 2006). This measure will also minimize the reduction in habitat created by the road right-of-way, and maintain the aesthetics of the area. To accomplish this measure, clearing of trees and vegetation should be minimized along 199 Street and tree plantings should be designed to grow taller than the highest vehicles using the road.



Closure May 20, 2014

8.0 CLOSURE

This document entitled *Wildlife Passage Design Recommendations—199 Street Widening Project within Riverview Neighbourhood 2* was prepared by Stantec Consulting Ltd. for the account of Riverview Owners Group. The material in it reflects Stantec's best judgment in light of the information available to it at the time of preparation. Any use which a third party makes of this report, or any reliance on or decisions made based on it, are the responsibilities of such third parties. Stantec Consulting Ltd. accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report

Stantec has endeavored to incorporate the principles of the WPEDG into the 199 Street wildlife passage design and the constraints associated with the physical site characteristics and available materials. We trust that this information is sufficient to support the submission of the initial concept and understand further refinement will be required as design progresses.

Respectfully submitted,

STANTEC CONSULTING LTD.

Hane

Bill Harper, R.P.Bio. Senior Wildlife Biologist

Reviewed by:

Colleen Bryden, R.P.Bio. Principal, Environmental Services



References May 20, 2014

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Appendix A Fish and Wildlife Species Summary Report (AESRD 2014)



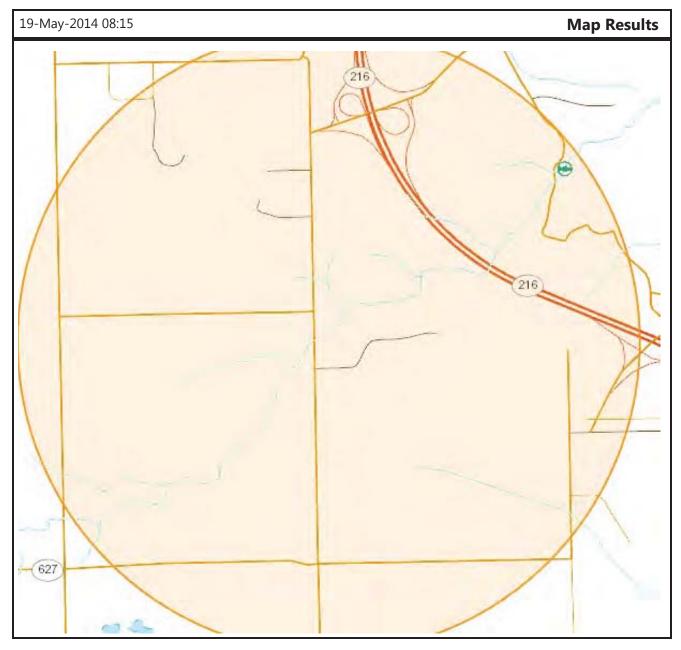
Fish and Wildlife Internet Mapping Tool (FWIMT)

(source database: Fish and Wildlife Management Information System (FWMIS))

Species Summary Report

Report Created: 19-May-2014 08:15

Species present within the current extent :				
Fish Inventory BROOK STICKLEBACK FATHEAD MINNOW		Wildlife Inventory No records found.		
Buffer Extent				
Centroid (X,Y): 588723, 5922668	Projection 10-TM AEP Forest	Centroid: (Qtr Sec Twp Rng Mer) NW 5 52 25 4	Buffer Radius: 2 kilometers	
Wildlife Contact Information				
Primary Contact Name: Curtis Stambaugh Alternative	Phone: 780-778-7116	Email: Curtis.Stambaugh@gov.ab.ca	Town:	
Name:	Phone:	Email:	Town:	
Fisheries Contact Information				
Primary Contact Name: Owen Watkins	Phone: 780-960-8189	Email: Owen.Watkins@gov.ab.ca	Town: Spruce Grove	
Alternative Name: Don Hildebrandt	Phone: 780-723-8523	Email: Don.Hildebrandt@gov.ab.ca	Town: Spruce Grove	



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12TH FLOOR, CENTURY PLACE 9803 - 102A AVENUE EDMONTON, ALBERTA T5J 3A3 780-496-1795 FAX: 780-496-4287

August 6, 2014

File: 199 Street (23 Avenue to 35 Avenue)

CIMA+ 10235 – 101 Street Edmonton, AB T5J 3G1

Attention: Glen Campbell, P.Eng.

Subject:199 Street (23 Avenue to 35 Avenue)
Review of Stantec Wildlife Crossing Report by Facility and Capital
Planning (FCP) and Office of Biodiversity (OBD)

Dear Mr. Campbell,

Thank you for submitting the report entitled "Wildlife Passage Design Recommendations -199 Street Widening Project Within the River Neighborhood," completed by Stantec and dated May 20, 2014. The City's Facility and Capital Planning (FCP) and Office of Biodiversity (OBD) sections have completed a review of the report; this letter provides a summary of the City's outstanding concerns and requests additional information to be provided by CIMA+ regarding the proposed two-culvert crossing treatment. Additional information is being requested in order to provide the City with the necessary background required to make an informed decision regarding the crossing treatment.

It is understood that the purpose of Stantec's study was to review and evaluate, from a wildlife passage perspective, Wedgewood Creek crossing options outlined in Terrace Engineering's (Terrrace) draft report entitled "Conceptual Bridge Planning Report, Wedgewood Creek Crossing on 199 Street NW in the City of Edmonton," dated May 9, 2014.

Stantec's report outlines support for a two-culvert wildlife passage at Wedgewood Creek; Terrace's report also considered this option to be the most desirable out of a number of potential options. However, it is the opinion of both FCP and OBD that the information provided in Stantec's report is not sufficient to clearly support that a two-culvert treatment will accommodate passage of all of the Ecological Design Groups (EDGs) that are anticipated to use the Wedgewood Creek ravine. The proposed alternative design (twoculverts) for wildlife passage should be accompanied by supporting study that shows that the passage will accommodate all of the EDGs identified. At this time, a bridge structure is the only option that is known to support all of the EDGs.

FCP and OBD are pleased with the level of effort that was taken by Stantec to identify the EDGs for this area and are in support of ensuring that the measures implemented at this location provide accommodation for all of the EDGs identified. FCP and OBD are also pleased with the recognition outlined in Stantec's report that diversionary measures are required for some EDGs (i.e. birds and bats) and that a 65 m culvert would be too long for medium to small sized mammals.

Before the City can make a final determination as to whether the two-culvert design will accommodate the EDGs identified and whether this alternative is an acceptable solution for this crossing, further information is required. We ask that the following items be addressed with, or in advance of, the next submission of the concept plan:

- Review of the impacts that wing-walls would have on the use of the crossing structures by wildlife. It is felt that overly tall and/or unnatural walls may be a perceived barrier to wildlife. Further, excess fill should be avoided (Ruediger and DiGiorgio 2006).
- The elevations of the medium and large wildlife passage culvert has not be identified in any documentation that has been provided to the City (i.e. location on the slope). Terrace's report suggests that it should be placed somewhere near the elevation of the roadway so as to minimize the passage length. OBD has expressed concern that a culvert placed near the top of the roadway may not be used by wildlife, and further their concern is drawn from the fact that there are no twoculvert crossings of similar design in place in the City.
 - The City is requesting additional evaluation of the effectiveness of a culvert placed near the roadway out of the typical travel path for the EDGs identified for this crossing. OBD suggests that the optimum culvert elevation is at the level of the natural travel corridor, which may be at the base of the ravine. It was noted that road cuts, drop offs and cliffs dissuade large mammals from using the crossings (Ruediger and DiGiorgio, 2006); these items should also be considered.
- Review of the effectiveness of comparable wildlife passages already constructed. As there are presently no two-culvert wildlife passages that have been constructed in the City; OBD would like some evidence that a two-culvert treatment would effectively accommodate the design EDGs. Furthermore, it is requested that for any case studies presented a clear comparison be provided of the crossing location along the slope with respect to the natural travel corridor.
- A review of general constructability and integration of the crossing treatment into the surrounding creek.

If you have any other questions or concerns, please do not hesitate to contact me at 780-442-4529 (Natalie.Lazurko@edmonton.ca) or Christopher Wintle at 780-496-1792. (Christopher.Wintle@edmonton.ca).

Yours truly,

1 Bayur Ko

Natalie Lazurko, P. Eng. Senior Engineer - Facility and Capital Planning Transportation Planning Branch

NL/ccw



September 19, 2014

Mr. Christopher Wintle Project Engineer Facility and Capital Planning City of Edmonton Transportation Services

Subject: 199 Street (23 Avenue to 35 Avenue) Comments to Your Correspondence dated August 6, 2014

Dear Mr. Wintle,

Thank you for your comments on the Stantec Wildlife Crossing Report. We have reviewed all of your comments and have assembled a new conceptual design for the wildlife animal underpass taking into consideration your comments. The new concept utilizes a standard bridge cross section with an opening that is 14 m wide and 4.5 m deep under the structure. The openness factor for this crossing is calculated to be 2.20. There is also a sky light in the median between the traffic lanes to assist with light entering the underpass. For additional information on this concept refer to the 199 Street Wedgewood Ravine wildlife crossing concept plan attached to this letter.

Also to assist you with your review of this concept, below is a summary of your comments/ questions with answers or clarification.

City Comment:

It is understood that the purpose of Stantec's study was to review and evaluate, from a wildlife passage perspective, Wedgewood Creek crossing options outlined in Terrace Engineering's (Terrrace) draft report entitled "Conceptual Bridge Planning Report, Wedgewood Creek Crossing on 199 Street NW in the City of Edmonton," dated May 9, 2014.

CIMA+: Yes, this is correct

City Comment:

The proposed alternative design (two culverts) for wildlife passage should be accompanied by supporting study that shows that the passage will accommodate all of the EDGs identified. At this time, a bridge structure is the only option that is known to support all of the EDGs.

CIMA+: The new proposed wildlife underpass is now a standard bridge structure. The current concept design is considered adequate to accommodate passage of all of the EDGs identified in the area (see Appendix A).



10235 - 101 Street, 4th Floor Edmonton (Alberta) T5J 3G1 CANADA

City Comment:

Before the City can make a final determination as to whether the two-culvert design will accommodate the EDGs identified and whether this alternative is an acceptable solution for this crossing, further information is required. We ask that the following items be addressed with, or in advance of, the next submission of the concept plan:

• Review of the impacts that wing-walls would have on the use of the crossing structures by wildlife. It is felt that overly tall and/or unnatural walls may be a perceived barrier to wildlife. Further, excess fill should be avoided (Ruediger and DiGiorgio 2006).

CIMA+: The wing walls in the current proposed option will follow the side slopes of the roadway embankment at 3:1 side slopes. At the entrance to the underpass the wing walls will be a similar height to the sides of the underpass. Animal fencing will direct the wildlife into the underpass. The wing walls are also angled away from the underpass to open each end up of the underpass. Natural shrubs and undergrowth will over time help to disguise the wing walls. The grade into the wildlife underpass is all set at 3:1, the underpass has been located towards the center of the ravine to minimise the amount of fill/cut that is needed. The wing wall design is considered more than adequate to facilitate movement of the EDGs that this structure is designed for (see Appendix A).

City Comment

• The elevations of the medium and large wildlife passage culvert has not been identified in any documentation that has been provided to the City (i.e. location on the slope). Terrace's report suggests that it should be placed somewhere near the elevation of the roadway so as to minimize the passage length. OBD has expressed concern that a culvert placed near the top of the roadway may not be used by wildlife, and further their concern is drawn from the fact that there are no two culvert crossings of similar design in place in the City.

CIMA+: Road stations have been shown on the plan view of the above noted plan that are the same stations as shown on the overall 199 Street Concept Plans; this shows the approximate location of the underpass relative to the ravine. Due to the angle of 199 Street crossing the ravine, one side of the underpass is in cut and the other side is in fill. The bridge structure will be located at the road surface with the wildlife underpass opening directly below the structure. The new vertical alignment of the proposed arterial roadway follows very closely to the previous alignment, with improved vertical curves. Knowing this, with an animal underpass 4.5 m below the road surface, any wildlife that has crossed the existing roadway will now be able to cross at a lower elevation.

An evaluation of wildlife travel corridors in the vicinity of 199 Street and Wedgewood Ravine indicate most game trails (presumably deer) were along ridges at the top of the ravine (see Appendix A). The location of the open-span crossing structure is near the typical travel path of deer in the area.



City Comment

• The City is requesting additional evaluation of the effectiveness of a culvert placed near the roadway out of the typical travel path for the EDGs identified for this crossing. OBD suggests that the optimum culvert elevation is at the level of the natural travel corridor, which may be at the base of the ravine. It was noted that road cuts, drop offs and cliffs dissuade large mammals from using the crossings (Ruediger and DiGiorgio, 2006); these items should also be considered.

CIMA+: An evaluation of wildlife travel corridors in the vicinity of 199 Street and Wedgewood Ravine indicate most game trails were along ridges at the top of the ravine (see Appendix A). Beaver movement was observed both at the base of the ravine and at the top of the ravine. The location of the open-span crossing structure is near the typical travel path of deer in the area.

City Comment

• Review of the effectiveness of comparable wildlife passages already constructed. As there are presently no two-culvert wildlife passages that have been constructed in the City; OBD would like some evidence that a two-culvert treatment would effectively accommodate the design EDGs. Furthermore, it is requested that for any case studies presented a clear comparison be provided of the crossing location along the slope with respect to the natural travel corridor.

CIMA+: A comparable structure to the large open-span bridge being proposed for Wedgewood Ravine has been installed near Lake Louise, AB. This structure has been monitored since 2007, and considered a highly effective structure for facilitating passage of a wide range wildlife species in Banff National Park (see Appendix A). Clevenger et al (2001) recommend a mixed size classes of wildlife crossing structures to accommodate the greatest variety of species possible. The proposed two-culvert system is not unlike the design being employed at Ellerslie Road in Edmonton, where large terrestrial wildlife are accommodated at Whitemud Creek, 400 m from a smaller crossing structure designed for small- and medium-sized EDGs.

City Comment

• A review of general constructability and integration of the crossing treatment into the surrounding creek.

CIMA+: Cost estimates for the culvert and standard bridge option as shown in the attached plan are estimated at \$8M. A bridge structure spanning the entire Wedgewood creek ravine is estimate at \$25M. There is approximately a magnitude of 3.1 times greater in the costs of the culvert and standard bridge option to the complete bridge option. If 199 Street is staged and only two lanes are built in the initial stage, the ultimate earth works, foundations, abutments and wing walls for the animal underpass and culvert could all be constructed in the initial stage leaving only the bridge top to be constructed at a later date. The bridge girders for the final two lanes can be placed at a later time with little or no impact on the Wedgewood creek/ravine.



Please review the attached wildlife concept plan and the above comments and confirm if this crossing structure is adequate. If the City wishes to discuss this concept in more detail CIMA+ would be glad to attend a meeting for further discussions.

Yours sincerely,

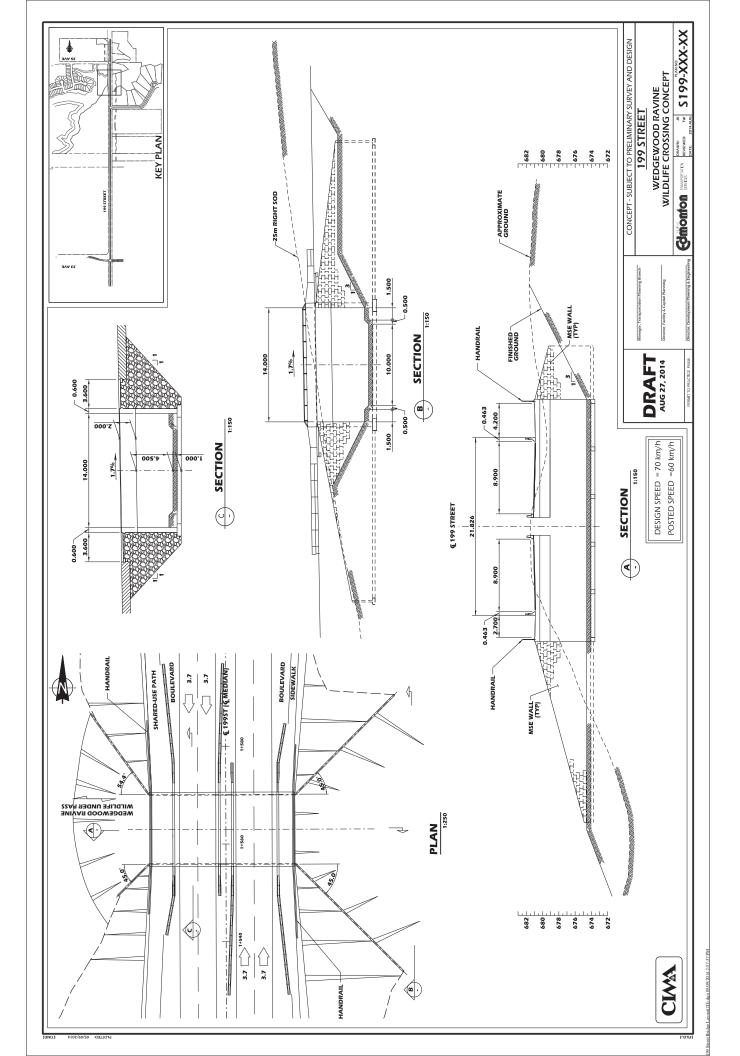
CIMA+

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Glen Campbell, P.Eng. Project Manager, Highway Engineering

Encl.





Wildlife Passage Design —199 Street Widening Project Within Riverview Neighbourhood 1



Prepared for: Riverview Owners Group (Qualico Communities, Walton Development and Management LP, Melcor Developments Ltd, and Sunwapta Holdings Corporation)

Prepared by: William L. Harper, R.P.Bio.

1102-18864

September 19, 2014

Table of Contents

1.0	BACKGROUND 1		
2.0	OBJECTIVES 1		
3.0	EVALUATION OF THE CONCEPTUAL DESIGN OF THE LARGE BELOW-GRADE WILDLIFE CROSSING STRUCTURE		
4.0	FIELD SURVEY OF WILDLIFE MOVEMENT PATTERNS 4		
5.0	CONCLUSION		
6.0	CLOSURE		
7.0	REFERENCES		
LIST OF	FIGURES		
Figure	1 Proposed Location of the Open-Span Wildlife Crossing Structure at Wedgewood Creek		
Figure	2 Observations of Wildlife Game Trails at Wedgewood Creek – Sept 2014 		



September 19, 2014

1.0 BACKGROUND

Stantec Consulting Ltd. (Stantec) was retained by Riverview Owners Group (the Client) to provide environmental consulting services and recommendations for wildlife passage as part of the 199 Street Widening within the Riverview Neighbourhood 1 (the Project).

As part of the Riverview Neighbourhood 1 development, 199 Street will be widened (CIMA+ 2014). The widened road, along with projected increases in traffic volume and vehicle speed, will increase the barrier effect of the road on wildlife. For these reasons, and to reduce animal-vehicle collisions, provisions for a wildlife crossing structure where 199 Street crosses the Wedgewood Ravine were considered.

2.0 OBJECTIVES

The City of Edmonton has requested additional information pertaining to wildlife passage associated with the Project (City of Edmonton 2014). The objective of this report is to evaluate the potential for the proposed wildlife crossing structures to maintain landscape permeability for the Ecological Design Groups (EDGs) predicted to occur in the area.

This report should be considered as follow-up to an earlier report on wildlife passage design dated May 20, 2014 (Stantec Consulting Ltd. 2014).

3.0 EVALUATION OF THE CONCEPTUAL DESIGN OF THE LARGE BELOW-GRADE WILDLIFE CROSSING STRUCTURE

The new concept utilises a standard bridge cross section with an opening that is 14 m wide and 4.5 m deep under the structure. The total length of the structure is estimated at 28.6 m. There is also a sky light in the median between the traffic lanes to increase natural light inside the structure.

Open-span bridge structures such as the one proposed for Wedgewood Ravine have been shown to be effective for both large wildlife (e.g., deer, bears), and a variety of smaller species (Ruediger and DiGiorgio 2007).

In Utah, analyses of the effectiveness of wildlife crossing structures confirm they should be designed to be as short as possible. Schwender (2013) found that culvert length outperformed all other parameters, and culvert width and length together were the best predictors of successful mule deer passage. As well, Cramer (2012) felt that when considering the metrics of wildlife crossing design, length was the most important factor, followed by width, and height was the least important consideration. Based on this analysis, Cramer (2012) recommended keeping wildlife



September 19, 2014

underpasses under 37 m long. The estimated length of the large below-grade crossing structure at Wedgewood Ravine is 28.6 m, well within Cramer's (2012) recommendation.

Clevenger and Huijser's (2011) general guidelines recommend a width of >12 m and height of >4 m for large mammal underpasses. The dimensions of the new open-span crossing structure are 14 m wide and 4.5 high, which is above Clevenger and Huijser's (2011) recommendation.

Although measures of a structure's width, height and length are important considerations in designing wildlife structures, Clevenger and Huijser (2011) do not recommend the use of an openness index during planning and design. However, the Wildlife Passage Engineering Design Guidelines (WPEDG; City of Edmonton 2010) indicate that an "optimal passage openness" ratio of 1.5 is preferred for Large Terrestrial EDG. The openness ratio for the large below-grade crossing structure is 2.20, which is above the City of Edmonton (2010) recommendation.

A similar structure to the open-span bridge proposed for Wedgewood Ravine has recently been installed near Lake Louise in Banff National Park. Referred to as the "Island" crossing structure, it has been monitored for wildlife use since 2007 (Clevenger et al. 2009). Between April 2012 and March 2013 this structure was successfully used by 7 grizzly bears, 3 black bears, 3 wolves, 4 coyotes, 23 moose, 41 elk, and 148 deer (Clevenger et al. 2013). Total monitored use to date is 22 grizzly bears, 5 black bears, 27 wolves, 24 coyotes, 77 moose, 100 elk, and 471 deer (Clevenger et al. 2013). This is considered a high quality wildlife crossing structure within the national parks system.

In response to the comment (City of Edmonton 2014) that "It is felt that overly tall and/or unnatural walls may be a perceived barrier to wildlife", we were unable to find any literature that indicated negative effects of wing-walls on the effectiveness of wildlife crossing structures. To the contrary, the wildlife crossing structure handbook (Clevenger and Huijser 2011) only refer to wing-walls as encouraging and guiding animals to the entrance of wildlife crossing structures. Since wing-walls have potential to greatly reduce the overall length of a crossing structure, their presence in the proposed concept design is considered to have a positive effect on promoting wildlife use of the structure. The maximum height of the wing-walls (4.5 m) is not considered excessive.



September 19, 2014

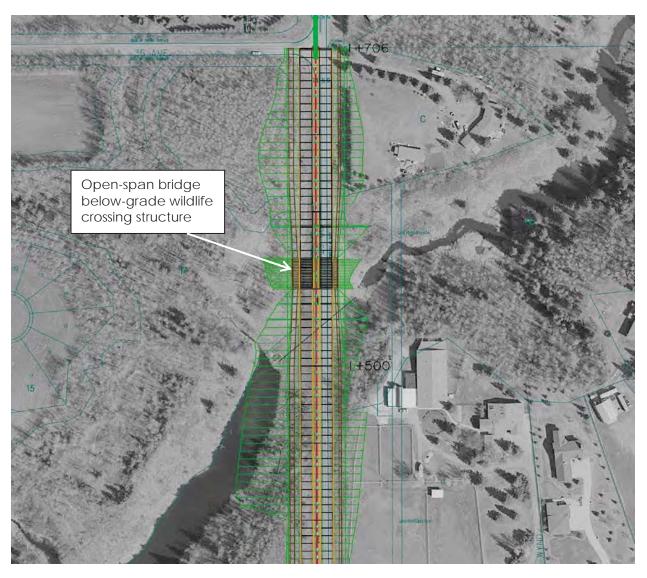


Figure 1 Proposed Location of the Open-Span Wildlife Crossing Structure at Wedgewood Creek



September 19, 2014

4.0 FIELD SURVEY OF WILDLIFE MOVEMENT PATTERNS

A field survey was undertaken on September 12, 2014 between 10:30 – 14:00 hr in order to determine movement patterns of wildlife in the vicinity of the proposed wildlife crossing structure.

West of 199 Street, South of the Beaver Pond

Faint game trails (consistent with use by deer), were located along the slope above the water south of the beaver pond on the west side of 199 Street (Figure 2). These trails meandered in the forested area along the slope to an open area approximately where the proposed open-span crossing structure will be located. A single patch of deer scat was observed along this trail. There were also multiple faint trails running parallel to the 199 Street in a young aspen patch. These trails run roughly parallel to the roadway (Figure 2).

Numerous beaver trails were found running up from the water into the forested area on both sides of the beaver pond. Single sets of coyote and deer tracks were observed at the north-east end of the water body in a mud/gravel area.

West of 199 Street, North of the Beaver Pond

The slope immediately northwest of the pond is extremely steep (Figure 2). The only tracks/trails observed were those of beavers travelling up from the pond to the forested area above. The top of the slope is a crest/ridge with slopes NW and SE. A faint game trail was observed along the top of this ridge and a more active trail was observed parallel to the ridge on the northwest side. Both of these trails eventually faded out near the residential areas currently under construction. The treed area north of the pond was also searched and faint game trails associated with trampling of vegetation were observed, along with signs of human activity.

East of 199 Street, North of Wedgewood Creek

The slope along the north edge of the stream is very steep (Figure 1). No tracks/trails were observed besides beaver trails, which were very common in the area. A very faint game (presumably deer), trail was observed along the top edge of the ridge along residential fencing.

East of 199 Street, South of Wedgewood Creek

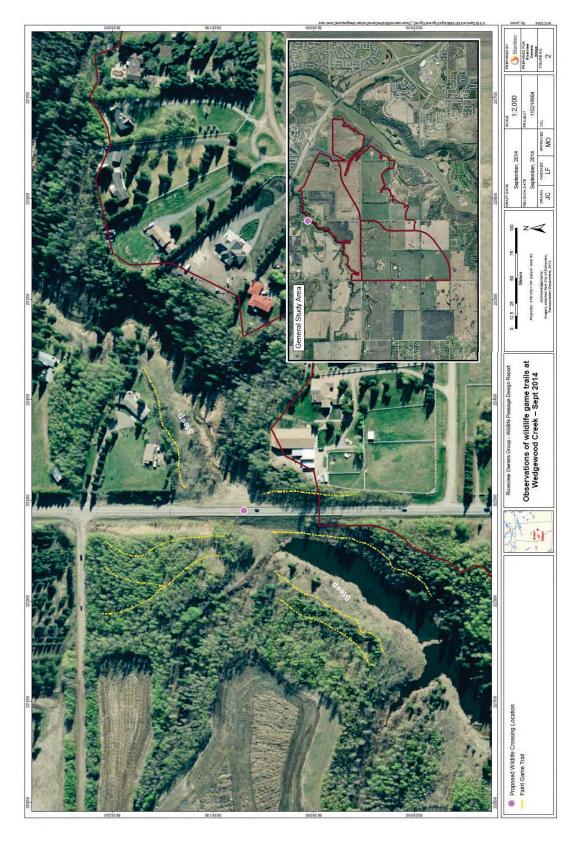
The south edge of the stream consisted of a narrow, relatively level area (less than 10 m wide), with grades sufficiently low that it is walkable. Further away from the water it became steeper with dense shrub cover and large mature trees. The only tracks/trails observed in the area were beaver trails that were abundant and well-used.

199 Street

Both edges of 199 Street were surveyed for tracks/trails crossing the roadway. The substrate was not ideal for detecting wildlife use as the roadway is paved and the sides of the road are fine gravel. No wildlife tracks or trails were observed along the roadway.



September 19, 2014



Observations of Wildlife Game Trails at Wedgewood Creek - Sept 2014 Figure 2



September 19, 2014

Summary of Wildlife Field Survey

Few established game trails were observed in the area, possibly from nearby active construction in the area. Most of the faint deer trails and scat observed were not in the bottom of the ravine but were higher up on the edges. This suggests that deer wouldn't be "climbing out of the ravine to go through the underpass" but rather moving along their existing routes or even descending slightly to travel under 199 Street.

5.0 CONCLUSION

The City of Edmonton (2010) has identified 11 Ecological Design Groups (EDGs) to be addressed when planning and designing wildlife passage: Large Terrestrial, Medium Terrestrial, Small Terrestrial, Amphibians, Aerial Mammals, Aquatic Species, Scavenger Birds, Birds of Prey, Water Birds, Ground Dwelling Birds, and Other Birds. It is expected that one or more species within all 11 EDGs are predicted to occur in the vicinity of Wedgewood Creek (Stantec 2014).

The current concept design is adequate to accommodate the passage requirements for all of the EDGs identified in the Stantec (2014) report. Passage requirements for the Large Terrestrial, Medium Terrestrial, and Small Terrestrial EDGs are adequately addressed in concept design for the large open-span wildlife crossing structure (Figure 1). The proposed location approximately 5 m below the roadway is near the natural travel area of deer at the top of Wedgewood Ravine.

Passage requirements for the Small Terrestrial, Amphibian, and Aquatic Species EDGs are adequately addressed in the proposed modified drainage culvert associated with Wedgewood Creek. Passage requirements for the Aerial Mammals, Scavenger Birds, Birds of Prey, Ground Dwelling Birds, Water Birds and Other Birds EDGs will be adequately addressed above-grade in the Recommendations for Reducing Bird and Bat Vehicle Collision Risk (see Stantec 2014).

6.0 CLOSURE

This document entitled *Wildlife Passage Design Recommendations—199 Street Widening Project within Riverview Neighbourhood 1* was prepared by Stantec Consulting Ltd. for the account of Riverview Owners Group. The material in it reflects Stantec's best judgment in light of the information available to it at the time of preparation. Any use which a third party makes of this report, or any reliance on or decisions made based on it, are the responsibilities of such third parties. Stantec Consulting Ltd. accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report

Stantec has endeavored to incorporate the principles of the WPEDG into the 199 Street wildlife passage design and the constraints associated with the physical site characteristics and available materials. We trust that this information is sufficient to support the submission of the initial concept.



September 19, 2014

Respectfully submitted,

STANTEC CONSULTING LTD.

Fill Hayper

William Harper, R.P. Bio Senior Wildlife Biologist Phone (250) 655-5394 bill.harper@stantec.com

Stephanie Grossman, M.Sc., P.Biol. Wildlife Biologist Phone: (780) 917-7429 stephanie.grossman@stantec.com



September 19, 2014

7.0 REFERENCES

- CIMA+. 2014. 199 Street concept planning report: 23 Avenue to 35 Avenue draft submission. Draft concept plan prepared by G. Campbell, P.Eng. for the Riverview Ownership Group, April 2014.
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September 19, 2014

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October 15, 2014

TO:	Natalie Lazurko, P.Eng. Transportation Planning
FROM:	Catherine Shier Ecology Unit, Parks + Biodiversity
CC:	Francis Wambugu, P.Eng., MBA Development Planning and Engineering
SUBJECT:	Comments for document titled "199 street (23 Avenue to 35 Avenue). Comments to your correspondence date August 6, 2014)"

The Ecology Unit (Parks + Biodiversity) has reviewed CIMA's September 19, 2014 report titled "199 street (23 Avenue to 35 Avenue). Comments to your correspondence date August 6, 2014" that our office received on September 23, 2014. Thank you for the opportunity to review. We would like to offer the following comments for your consideration as design of the wildlife passage at Wedgewood Creek and 199th street proceeds:

Large Terrestrial wildlife below-grade crossing structure:

We are encouraged to see that a bridge structure is being proposed at this location. However, we have a few questions/concerns with the proposed design:

- a) How does the wildlife crossing interact with the newly installed outfall west of 199th street on the north bank of the creek?
- b) It is currently unclear how wildlife is intended to move west of this passage. Most notably, after going over (or around) the rip rap of the outfall (which, for access reasons, is likely to remain devoid of significant vegetation), they would need to cross over a small tributary (which is often flooded by beaver dams making passage difficult) and then up a steep slope to continue to move west.
- c) Line of sight: the structure should be located at near equal contour sites on either side of the road and be angled to fit the line of the creek bottom. This would provide for a more appropriate line of sight.

There is reference in this report that the proposed structure is comparable to a large open-span bridge that was installed near Lake Louise, AB. Please note that a few important differences between the two include:

I. There is no outfall or small tributary/flooded area to design around or that impacts the functionality of the passage.

II. The line of site of the island structure is unobstructed. See Figure 1 as an example of a similar site. (Figure 1: http://www.pc.gc.ca/eng/pnnp/ab/banff/plan/transport/tch-rtc/passagescrossings/passagesstructures.aspx?a=1&photo=%7B1235FE0E-46C7-464D-BA57-27876ACA7CA0%7D)



III. The Island crossing is close to perpendicular to the valley (Figure 2a) as compared to the crossing at Wedgewood where we see a crossing of about 45% (Figure 2b)



Figure 2a

Figure 2b

- IV. The width of the bridge span across the Lake Louise crossing is approximately 50% or more of the valley. In the case of Wedgewood Creek it appears the width of the bridge span is 1/5th of the ravine (Note: these estimates are based on measurement estimates taken from Google Earth and are not exact).
- V. I could not find details that speak to the elevation change wildlife need to traverse to use the Island crossing. However, it seems from the image above that it is not that great as one can see the creek flow through the passage as well. Also, note that the open meridian is greater than the width of each road sections. Both of these are different from what is being proposed at the Wedgewood crossing.

Small terrestrial and aquatic wildlife below-grade crossing structure

Appendix A of the report speaks to the passage requirements of small terrestrial, amphibian and aquatic EDGs being adequately addressed in the proposed modified drainage culvert. Has this culvert been modified from what was presented formerly? Please outline the difference. As outlined in the *Wildlife Passage Engineering Design Guidelines* the minimum openness ratio that the design should be aiming for is 0.4 with open bottom culverts being preferred over closed bottom structures as they incorporate natural substrate.

Given the concerns outlined above for both large and small wildlife use of the proposed passages, our office strongly encourages the installation of a wider bridge at this location which would improve the line of sight and overall functionality of the passage. We feel this request is reasonable given that:

- Three designs have been reviewed to date and none adequately address the needs of all of the targeted Ecological Design Groups;
- The unique site challenges of this location (e.g. culvert, small flooded tributary, road crossing angle, steep slope on west side of road) could be overcome by the installation of a wider bridge;
- The 199 Street arterial roadway crossing of Wedgewood Ravine is identified in the current ARA Bylaw as a bridge structure;
- The requirement for a bridge (as suggested in the ARA) is referenced in the recently approved Riverview ASP;
- The proponent has been aware of this requirement since October 2012, where a verbal agreement was made with the Office of Biodiversity that a bridge would be constructed
- Wedgewood creek is a significant natural corridor in SW Edmonton that provides connectivity into surrounding communities;
- The request above falls in line with current City objectives on maintaining (or restoring degraded) ecological linkages, most notably the following objectives as outlined in The Way We Grow; and
- This project falls within the North Saskatchewan River Valley Bylaw Area Redevelopment Plan (Bylaw 7188). This Bylaw provides the following direction when upgrading approved transportation corridors: "To support a transportation system which serves the needs of the City and the Plan area, yet is compatible with the parkland development and the environmental protection of the River Valley and Ravine System."

Thank you for the opportunity to comment. Please contact Catherine Shier at 780-442-4531 with any questions or concerns.

Catherine Shier Senior Ecological Planner, Ecology unit Parks + Biodiversity Sustainable Development Ph: 780-442-4531 Catherine.shier@edmonton.ca



November 18, 2014

Mr. Christopher Wintle Project Engineer Facility and Capital Planning City of Edmonton Transportation Services

Subject: 199 Street (23 Avenue to 35 Avenue) Comments to Your Correspondence dated October 15, 2014

Dear Mr. Wintle,

Further to the memo dated October 15, 2014 from Catherine Shier and the site visit held on October 30, 2014. We have reviewed all of your comments and have assembled a new conceptual design for the wildlife animal underpass taking into consideration your comments. The new concept continues to utilize a standard bridge cross section with an opening that is 14 m wide and 4.5 m deep under the structure and a separate culvert for the stream crossing. The structure is now skewed at 25 degrees to the roadway to assist with the line of sight for the wildlife and the stream crossing culvert has been adjusted so the overall length is now shorter. The Skew on the bridge structure has lengthened the overall structure by 2.0m given a new openness ratio of 2.0 (see appendix A for additional comments). There will still be a "sky light" in the bridge structure in the median between the traffic lanes to assist with light entering the underpass. For additional information on this concept refer to the 199 Street Wedgewood Ravine wildlife crossing concept plan attached to this letter.

Also to assist you with your review of this concept, below is a summary of your comments/ questions with answers or clarification.

City Comment:

How does the wildlife crossing interact with the newly installed outfall west of 199th street on the north bank of the creek?

CIMA+: The manhole and outfall were in the vicinity of where the wildlife underpass crossed under 199 St. in our previous submission, the underpass crossing perpendicular to 199 Street on the west side pointing directly at the manhole. As discussed on site the alignment of the underpass has now been moved to the south and skewed such that the west side entrance/exit is approximately centered between the manhole and the outfall. The pipeline associated with the outfall is approximately 3.5 meters below grade and won't be impacted by the cut/fill slope from the underpass.



10235 - 101 Street, 4th Floor Edmonton (Alberta) T5J 3G1 CANADA

City Comment:

It is currently unclear how wildlife is intended to move west of this passage. Most notably, after going over (or around) the rip rap of the outfall (which, for access reasons, is likely to remain devoid of significant vegetation), they would need to cross over a small tributary (which is often flooded by beaver dams making passage difficult) and then up a steep slope to continue to move west.

CIMA+: With the proposed skew angle and also some flat benching provided in the side slopes of the 199 Street embankment, the wildlife will have adequate options to continue on either side of the ravine banks to the west. Refer to appendix A for additional comments.

City Comment:

Line of sight: the structure should be located at near equal contour sites on either side of the road and be angled to fit the line of the creek bottom. This would provide for a more appropriate line of sight.

CIMA+: The underpass structure has been skewed to align closer with the angle of the ravine and to improve the line of site for the wildlife. The structure has also been moved further to the south.

City Comment:

There is reference in this report that the proposed structure is comparable to a large open-span bridge that was installed near Lake Louise, AB. (5 differences were notes, refer to the memorandum from Catherine Shier, October 15, 2014 in Appendix A)

CIMA+: Duly noted, the Lake Louise bridge structure itself is very similar in terms of engineering design to the structure shown in the concept for 199 Street. Each and every wildlife crossing structure is unique to the topographical constraints in an area and target species the structure is being designed for. In particular we have improved the "line of sight".

City Comment

Appendix A of the report speaks to the passage requirements of small terrestrial, amphibian and aquatic EDGs being adequately addressed in the proposed modified drainage culvert. Has this culvert been modified from what was presented formerly? Please outline the difference.

CIMA+: The culvert length has been shortened from what was shown on the previous submission, the culvert length is now 112.5m long. The original conceptual bridge report suggested that this culvert be a 2.4 m diameter SPCSP culvert. In Stantec's report Wildlife Passage Design Recommendations as a response to the above noted report, for the small terrestrial wildlife, commented that raised platforms could be installed within the culvert to accommodate this wildlife group. For additional information on this please refer to Appendix A.

City Comment



The unique site challenges of this location (e.g. culvert, small flooded tributary, road crossing angle, steep slope on west side of road) could be overcome by the installation of a wider bridge;

CIMA+: The side slopes along the Wedgewood creek ravine are all of a slope such that they could be traversable by wildlife. The current opening under the wildlife passage provides adequate openness as required in the City's guidelines. With the assistance of fencing and landscaping the underpass will function adequately. The underpass has been located such that it limits interference of the foundations under the abutments at each end of the bridge structure and the stream culvert that is directly south of the wildlife underpass and at a lower level.

The south bank of the ravine was examined as a possible location for the wildlife underpass, however the land in the south east quadrant at the raving crossing is a private landowner and the property lines follow the existing road right of way providing little or no access into a possible underpass, so this option is not a valid option.

Currently the underpass is set at 14 meters wide to allow for the structure to be constructed as a standard bridge. The revised alignment of the underpass has improved sightlines and reduced the magnitude of elevation change at each end for animal entrance/egress. For additional information on this please refer to Appendix A.

City Comment

The 199 Street arterial roadway crossing of Wedgewood Ravine is identified in the current ARA Bylaw as a bridge structure;

The requirement for a bridge (as suggested in the ARA) is referenced in the recently approved Riverview ASP ;

The proponent has been aware of this requirement since October 2012, where a verbal agreement was made with the Office of Biodiversity that a bridge would be constructed

CIMA+: A bridge structure is now proposed for the wildlife underpass.

City Comment

Wedgewood creek is a significant natural corridor in SW Edmonton that provides connectivity into surrounding communities;

• The request above falls in line with current City objectives on maintaining (or restoring degraded) ecological linkages, most notably the following objectives as outlined in The Way We Grow; and

• This project falls within the North Saskatchewan River Valley Bylaw Area Redevelopment Plan (Bylaw 7188). This Bylaw provides the following direction when upgrading approved transportation corridors: "To support a transportation system which serves the needs of the City



and the Plan area, yet is compatible with the parkland development and the environmental protection of the River Valley and Ravine System."

CIMA+: This is all valid information to be acknowledged in moving this project forward to the next design stages.

Based on all that was discussed at our site meeting on October 30, 2014, we trust that we have addressed the City's comments and concerns for the crossing of the Wedgewood Creek Ravine such that the Conceptual design can be approved and to allow commencement of the Preliminary Design phase of this project. The Preliminary Design phase will continue to refine the design and further address many of the comments that have been discussed in these communications

If you have any questions or concerns feel free to contact the undersigned.

Yours sincerely,

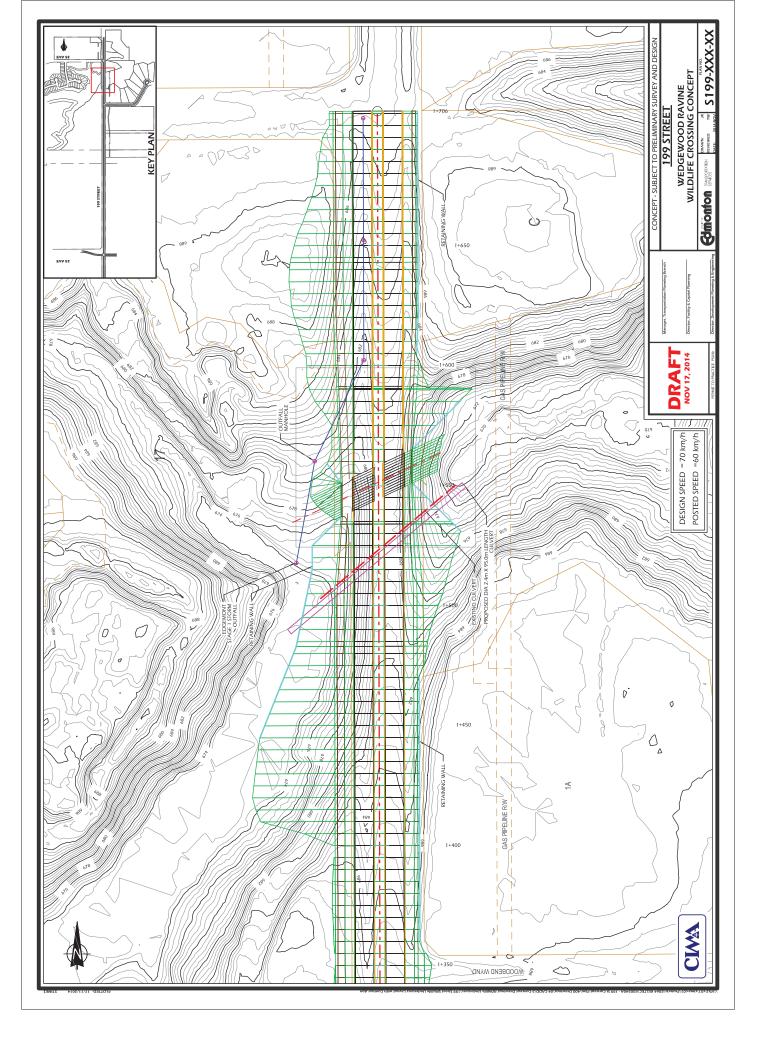
CIMA+

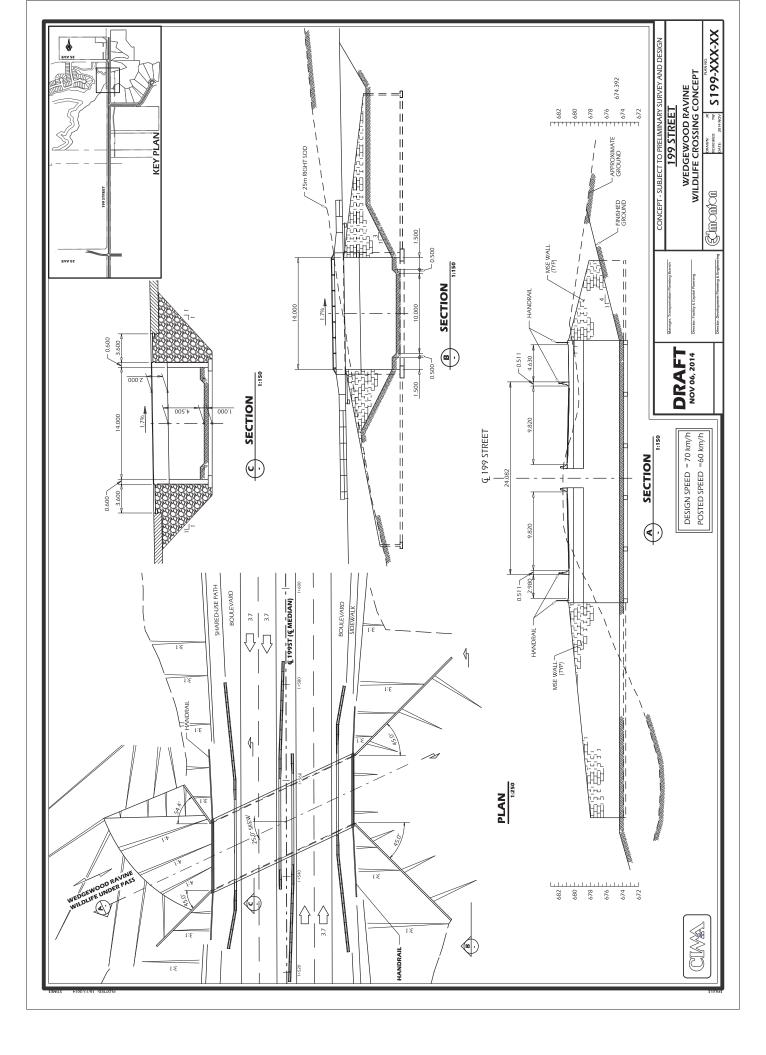
Slampher

Glen Campbell, P.Eng. Project Manager, Highway Engineering

Encl. Original Bridge Concept report (May 9, 2014) Wildlife Passage Design recommendations_(May 20, 2014) Letter from the City of Edmonton (August 6, 2014) Letter from CIMA+ addressing City comments (Sept 19, 2014) Wildlife Passage Design recommendations_(Sept 19, 2014) Comments from the City of Edmonton (Oct 15, 2014) Appendix A – additional information supporting this letter.







Appendix A – Evaluation of November 2014 Conceptual Design November 2014

Appendix A EVALUATION OF NOVEMBER 2014 CONCEPTUAL DESIGN

1.0 BACKGROUND

Stantec Consulting Ltd. (Stantec) was retained by Riverview Owners Group (the Client) to provide environmental consulting services and recommendations for wildlife passage as part of the 199 Street Widening within the Riverview Neighbourhood 1 (the Project).

As part of the Riverview Neighbourhood 1 development, 199 Street will be widened (CIMA+ 2014). The widened road, along with projected increases in traffic volume and vehicle speed, will increase the barrier effect of the road on wildlife. For these reasons, and to reduce animal-vehicle collisions, provisions for wildlife movement where 199 Street crosses the Wedgewood Ravine were considered.

2.0 **OBJECTIVES**

The City of Edmonton has requested additional information pertaining to wildlife passage associated with the Project (City of Edmonton 2014a and 2014b; site visit on October 30, 2014). The objective of this report is to evaluate the potential for the two proposed wildlife crossing structures to maintain landscape permeability for the Ecological Design Groups (EDGs) predicted to occur in the area, and to respond to questions/concerns outlined by the City of Edmonton (2014b).

This report should be considered as follow-up to two earlier reports on wildlife passage design dated May 20, 2014 (Stantec Consulting Ltd. 2014a) and September 18, 2014 (Stantec Consulting Ltd. 2014b).

3.0 LARGE, MEDIUM AND SMALL TERRESTRIAL WILDLIFE BELOW-GRADE WILDLIFE CROSSING STRUCTURE

The November 2014 concept design utilises a standard bridge cross section with an opening that is 14 m wide and 4.5 m deep under the structure. The total length of the structure is estimated at 30.9 m (Figure 1). There is also a "sky light" in the median between the traffic lanes to increase natural light inside the structure.

Open-span structures such as this have been shown to be effective for both large wildlife (e.g., deer, bears) and a variety of smaller species (Ruediger and DiGiorgio 2007). The dimensions of



Appendix A – Evaluation of November 2014 Conceptual Design November 2014

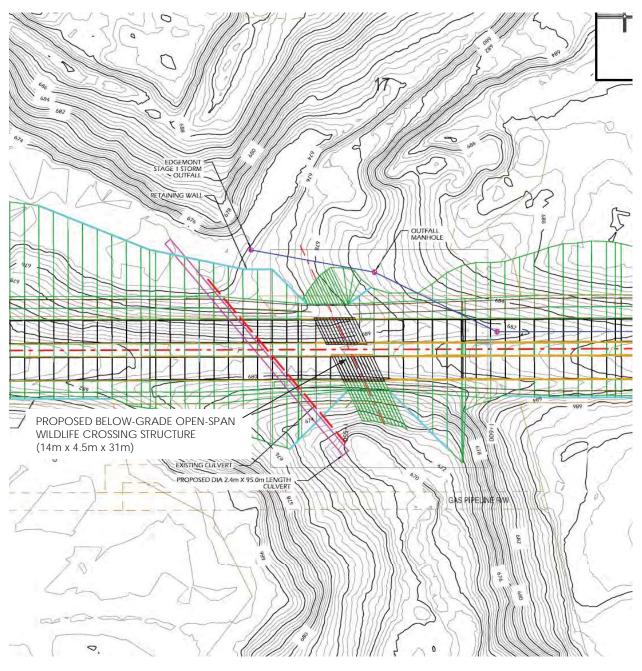


Figure 1 Wildlife Crossing Concept – Wedgewood Ravine (Draft Nov 17, 2014)



Appendix A – Evaluation of November 2014 Conceptual Design November 2014

this large below-grade crossing structure is within the large animal design recommendations for length (<37 m; Cramer 2012), width (>12 m; Clevenger and Huijser 2011), and height (>4 m Clevenger and Huijser 2011).

The Wildlife Passage Engineering Design Guidelines (WPEDG; City of Edmonton 2010) indicate an "optimal passage openness" of 1.5 is preferred for the Large Terrestrial EDG. The openness index for the November 2014 concept design of the large below-grade crossing structure is 2.04, which is above the City of Edmonton (2010) recommendation. Deer appear to prefer more open underpasses, and an openness index has been used to design underpasses since the early 1970s (Reed et al. 1975). However, more recent literature questions the validity of the openness index, and Clevenger and Huijser (2011) do not recommend its use in planning and designing wildlife crossing structures. The rationale behind Clevenger and Huijser (2011) questioning the validity of the openness index is as follows:

- There is changing understanding of how openness is measured. Is it an index, a ratio, or simply a state or concept?
- Wildlife crossing structures are not always rectilinear. There is no guidance on how different shaped underpass designs (arched, circular, elliptical) affect the openness index.
- Problems have been identified with an inconsistent use of metric vs. Imperial units.
- The relationship between openness and underpass performance is likely species-specific and time dependent.
- Despite the appeal and popularity of openness indices, there has never been a critical evaluation of the measure for designing wildlife underpasses.
- Openness is highly correlated to underpass length. Similarly, the three main underpass structural measures (length, width, height) exhibit multicollinearity (they tend to be redundant and highly correlated with one another).

Clevenger and Huijser (2011) do recommend the use of underpass measures (length, width, height) in conjunction with a critical evaluation of structural factors (e.g., highway configuration) and environmental factors (e.g., habitat quality, target species) when designing wildlife crossing structures.

As indicated in the May 2014 conceptual design report (Stantec 2014a), passage requirements for Large Terrestrial, Medium Terrestrial, and Small Terrestrial EDGs will be addressed in this large below-grade crossing structure. Provision of hiding cover (e.g., tree branches and tree trunks) inside the structure will be required to encourage use of this structure by small mammals, reptiles and amphibians (Connolly-Newman 2013). Specifications for small animal hiding cover will be provided during preliminary design.



WILDLIFE PASSAGE DESIGN -199 STREET WIDENING PROJECT WITHIN RIVERVIEW NEIGHBOURHOOD 1

Appendix A – Evaluation of November 2014 Conceptual Design November 2014

4.0 SMALL TERRESTRIAL AND AQUATIC WILDLIFE BELOW-GRADE CROSSING STRUCTURE

The November 2014 concept design proposes a 2.4 m diameter x 95 m long drainage culvert under 199 Street (Figure 1). The May 2014 conceptual design report (Stantec 2014a) suggested that passage requirements for the Small Terrestrial, Amphibian, and Aquatic Species EDGs could be addressed in the modified drainage culvert. Wood frog and boreal chorus frog have been detected in the vicinity of Wedgewood Ravine (Ecoventure 2013).

Due to the high levels of beaver activity in the area, it is very likely that modifications to the inlet and outlet of the drainage culvert will be required to prevent beavers from accessing and blocking the drainage culvert. This will preclude Medium Terrestrial EDG use of this structure.

This small below-grade crossing will be modified with the addition of a raised platform to allow for dry passage of small-sized animals when water is flowing through the culvert. Specifications for small animal dry passage will be provided during preliminary design.

5.0 **RESPONSE TO CITY OF EDMONTON COMMENTS**

The City of Edmonton has requested additional information pertaining to wildlife passage associated with the Project (City of Edmonton 2014b). The following is in response to the questions/concerns with the earlier conceptual design.

City Comment:

How does the wildlife crossing interact with the newly installed outfall west of 199 Street on the north bank of the creek?

Stantec: The realignment of the underpass will improve wildlife access on the west side of 199 Street . The location of the outfall is not anticipated to adversely affect wildlife use of this structure.

City Comment:

It is currently unclear how wildlife is intended to move west of this passage. Most notably, after going over (or around) the rip rap of the outfall (which, for access reasons, is likely to remain devoid of significant vegetation), they would need to cross over a small tributary (which is often flooded by beaver dams making passage difficult) and then up a steep slope to continue to move west.

Stantec: The natural topography on the west side of passage is not expected to prevent wildlife movement on the west side of the structure. Fill slopes associated with the road will require



Appendix A – Evaluation of November 2014 Conceptual Design November 2014

benching and a 3 m wide wildlife path to provide north-south movement. Details on wildlife paths and benching will be provided during preliminary design.

City Comment:

Line of sight: the structure should be located at near equal contour sites on either side of the road and be angled to fit the line of the creek bottom. This would provide for a more appropriate line of sight.

Stantec: Line of sight has been improved by skewing the large crossing structure 25 degrees.

City Comment:

There is reference in this report that the proposed structure is comparable to a large open-span bridge that was installed near Lake Louise, AB. (5 differences were notes, refer to the memorandum from Catherine Shier, October 15, 2014 in Appendix A)

Stantec: The proposed structure is very similar in engineering design to the large open-span bridge that was installed near Lake Louise, AB. It is expected that the proposed structure will function similarly to the Lake Louise structure for wildlife passage.

City Comment

Appendix A of the report speaks to the passage requirements of small terrestrial, amphibian and aquatic EDGs being adequately addressed in the proposed modified drainage culvert. Has this culvert been modified from what was presented formerly? Please outline the difference.

Stantec: The latest design shown in Figure 1 is shorter in length (95 m) than the previous design (approximately 150 m). Specifications for small animal dry passage will be provided during preliminary design.

City Comment

The unique site challenges of this location (e.g. culvert, small flooded tributary, road crossing angle, steep slope on west side of road) could be overcome by the installation of a wider bridge.

Stantec: The natural topography of Wedgewood Ravine does not pose a barrier to wildlife movement. The width and height of the proposed large below-grade crossing structure is more than adequate to provide wildlife passage. An earlier design 7 m wide was increased to 14 m to improve the openness of this structure. Further increases in the width of this structure are unnecessary and unwarranted.



WILDLIFE PASSAGE DESIGN -199 STREET WIDENING PROJECT WITHIN RIVERVIEW NEIGHBOURHOOD 1

Appendix A – Evaluation of November 2014 Conceptual Design November 2014

6.0 CONCLUSION

The City of Edmonton (2010) has identified 11 Ecological Design Groups (EDGs) to be addressed when planning and designing wildlife passage: Large Terrestrial, Medium Terrestrial, Small Terrestrial, Amphibians, Aerial Mammals, Aquatic Species, Scavenger Birds, Birds of Prey, Water Birds, Ground Dwelling Birds, and Other Birds. It is expected that one or more species within all 11 EDGs are predicted to occur in the vicinity of Wedgewood Creek (Stantec 2014a).

The current concept design is adequate to accommodate the passage requirements for all of the EDGs identified in the Stantec (2014a) report. Passage requirements for the Large Terrestrial, Medium Terrestrial, and Small Terrestrial EDGs are adequately addressed in concept design for the large open-span wildlife crossing structure (Figure 1). The proposed location approximately 5 m below the roadway is near the natural travel area of deer at the top of Wedgewood Ravine that was observed during the field assessment (Stantec 2014b).

Passage requirements for the Small Terrestrial, Amphibian, and Aquatic Species EDGs are adequately addressed in the proposed modified drainage culvert associated with Wedgewood Creek. Passage requirements for the Aerial Mammals, Scavenger Birds, Birds of Prey, Ground Dwelling Birds, Water Birds and Other Birds EDGs will be adequately addressed above-grade in the Recommendations for Reducing Bird and Bat Vehicle Collision Risk (see Stantec 2014a).

7.0 CLOSURE

This evaluation of conceptual design for wildlife passage on the 199 Street Widening Project within Riverview Neighbourhood 1 was prepared by Stantec Consulting Ltd. for the Riverview Owners Group. The material in it reflects Stantec's best judgment in light of the information available to it at the time of preparation. Any use which a third party makes of this report, or any reliance on or decisions made based on it, are the responsibilities of such third parties. Stantec Consulting Ltd. accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report



Appendix A – Evaluation of November 2014 Conceptual Design November 2014

Stantec has endeavored to incorporate the principles of the WPEDG into the 199 Street wildlife passage design and the constraints associated with the physical site characteristics and available materials. We trust that this information is sufficient to support the submission of the initial concept.

Respectfully submitted,

STANTEC CONSULTING LTD.

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William L. Harper, M.Sc., R.P.Bio. Senior Wildlife Biologist



WILDLIFE PASSAGE DESIGN - 199 STREET WIDENING PROJECT WITHIN RIVERVIEW NEIGHBOURHOOD 1

Appendix A – Evaluation of November 2014 Conceptual Design November 2014

8.0 **REFERENCES**

- CIMA+. 2014. 199 Street concept planning report: 23 Avenue to 35 Avenue draft submission. Draft concept plan prepared by G. Campbell, P.Eng. for the Riverview Ownership Group, April 2014. 88 pp.
- City of Edmonton. 2010. Wildlife passage engineering design guidelines. Report prepared by Stantec Consulting Ltd. for the Office of Natural Areas, City of Edmonton, AB. 249 pp. Available:

http://www.edmonton.ca/environmental/documents/WPEDG_FINAL_Aug_2010.pdf Accessed September 17, 2014.

- City of Edmonton. 2014a. Review of Stantec's Wildlife Crossing Report by Facility and Capital Planning (FCP) and Office of Biodiversity (OBD). Letter to CIMA+ dated August 6, 2014 by N. Lazurko, Transportation Services, City of Edmonton, AB. 3 pp.
- City of Edmonton. 2014b. Comments for document titled 199 Street (23 Avenue to 35 Avenue). Memo to N. Lazurko dated October 15, 2014 from C. Shier, City of Edmonton, AB. 3 pp.

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Appendix A – Evaluation of November 2014 Conceptual Design November 2014

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- Stantec Consulting Ltd. 2014a. Wildlife passage design recommendations—199 Street widening project within Riverview Neighbourhood. Report prepared for the Riverview Owners Group, dated May 20, 2014. 15 pp.
- Stantec Consulting Ltd. 2014b. Wildlife passage design—199 Street widening project within Riverview Neighbourhood 1. Report prepared for the Riverview Owners Group, dated September 18, 2014. 11 pp.



MEMORANDUM

December 4, 2014

TO:	Natalie Lazurko, P.Eng. Transportation Planning
FROM:	Catherine Shier Ecology Unit, Parks + Biodiversity
CC:	Francis Wambugu, P.Eng., MBA Development Planning and Engineering
SUBJECT:	Comments for 199 street crossing of Wedgewood Creek (May 15, 2014 concept drawings from CIMA)

Dear Natalie and Chris,

The Ecology Unit (Parks + Biodiversity) has reviewed CIMA's November 18, 2014 letter (Subject: *Comments to your correspondence dated October 15, 2014*) and associated attachments on the 199 street crossing of Wedgewood Creek.

We appreciate both the ability to meet with this team in the field and the additional work that they have completed in an attempt to address our office's concerns. While we are still not entirely satisfied with the line of site of the passage (and have concerns about the impact the large retaining walls will have on the "openness" of the passage) our office is comfortable approving this current concept which incorporates a dual passage system of:

- a) A bridge structure that will be designed to promote large mammal passage (openness ratio of 2.0) as well as accommodation of other EDG passage requirements and
- b) A culvert that allows for both aquatic and small terrestrial passage.

Moving forward to Preliminary Design, we wanted to take this opportunity to let the proponent know that the key to our support of the final design of the passages will depend on:

- Suggested changes to improve line of sight: Grading leading to (and out of) the passage should be further reviewed. We will be looking for an evaluation of other ways to improve the line of sight is maximized, for example, through potential modifications to the wing walls and additional earth work with respect to grading. As expressed in the field, our concerns lie mainly with the western opening of the passage and its steep slope, its relation to the outfall, and any restrictions that may result due to a need for maintenance access to the outfall.
- An understanding of how "open" the structure truly is: While the passage itself (4.5m x 14m) produces an openness ratio of 2.0, we are interested to know what impact, if any, such large wing walls have on the functionality of the passage (or the perception of openness by wildlife).

- Vegetation/landscaping of the wing walls and leading up to the structure to make the passage appear as natural as possible. Also, please confirm the type of maintenance access required for the outfall and how this will impact potential revegetation/restoration of the area. Is permanent access to this area required?
- Given the passage is directly under the road (and is more enclosed than a full span bridge would be), is noise to be a deterrent to wildlife use?
- An open median will be a requirement (thank you for including it) and we will be looking for the applicant to safely reduce the width of each road profile.
- Include design considerations in the bridge structure for the use of this passage for small/medium EDGs.
- Minimize light pollution.
- Ensure appropriate fencing for both wildlife and people management.
- With respect to aquatic passage, open-bottom culverts with natural substrate are preferred (both in the literature and by our office) to the option presented (2.4m corrugated pipe). Analysis on this option needs to be completed. Note also that there is conflicting information between the letter (indicates culvert length is 112.5 m long) versus the Appendix (95 m long).

In the past we have also requested the following at the appropriate drawing review phase and/or associated with the environmental review as per Bylaw 7188:

- Draft mitigation plan to address impact of construction activities on wildlife movement and use of the area (e.g. timing of construction)
- Outline potential locations for habitat restoration around proposed crossings to further offset the negative impacts of having the road widened to 4 lanes.

Thank you for the opportunity to comment. Please contact Catherine Shier at 780-442-4531 with any questions or concerns.

Catherine Shier Senior Ecological Planner, Ecology unit Parks + Biodiversity Sustainable Development Ph: 780-442-4531 Catherine.shier@edmonton.ca

APPENDIX K

Wildlife Passage Guidelines Checklist

Appendix D – User Checklists

The checklist presented in this section is designed as a tool to highlight the important questions that must be answered when designing a wildlife passage and to provide a place to organize the information obtained during the process. Section references have been provided throughout the checklist should additional information be required for a specific question.

Some of the items that will be helpful to have in advance of completing this checklist are:

- A shadow map of the project overlain on the most recent aerial photo of the area
- Existing and future land use maps (e.g. ASP and NSP concept maps) to get an understanding of surrounding land uses
- Wildlife collision data
- Search local wildlife databases (see Section 3.2.4.1 of Guidelines)

Transportation engineers may have difficulty answering some questions with certainty. As a result, it is strongly advised that the process of designing a wildlife passage be a joint effort between both ecologists and engineers. Please note that if "unknown" or "suspected" is checked for any of the questions additional study may be required.

To ensure that a project is not delayed due to missing information, it is highly recommended that this checklist be completed and submitted to the Office of Biodiversity in conjunction with any proposed wildlife passage at concept and reconfirmed at the design phase of the project.

A) PROJECT DESCRIPTION

Project:	199 Street Concept Plan
Road Type	Arterial
Date:	November 20, 2014
Location:	199 Street from 35 Avenue to 23 Avenue in the Riverside area



A.1 CURRENT ROAD CONDITION

Current number of lanes	2	Lanes
Current Traffic Speed	80	Km/Hr
Current Traffic Volume	5600	AADT
Culverts with dry passage area	□ Yes	No
Culverts without dry passage area	Yes	□ No
Retaining walls	□ Yes	No
Jersey barriers and/or noise barriers	□ Yes	No
Number of wildlife collisions in the last 5 years	8	
Number of deer collisions in the last 5 years	N/A	-
Other		
A.2 PROPOSED ROAD UPGRADES		
Branasad number of lanas	1	Lanac

Proposed number of lanes	4	Lanes
Proposed Traffic Speed	60	Km/Hr
Projected Traffic Volume	35650	AADT
Proposed Culverts with dry passage area	🗆 Yes	No No
Proposed Culverts without dry passage area	Yes	🗆 No
Retaining walls	Yes	🗆 No
Jersey barriers and/or noise barriers	Yes	🗆 No
Other – Bridge wildlife crossing dry passage structure	Yes	

A.3 IDENTIFY PROPOSED LAND USE

Check any of the land uses that will apply to both the project area and adjacent area. Assess both current and future land uses. Please refer to Section 3.2.1 for additional information

Residential		Industrial	
Commercial		Institutional	
Agricultural		Conserved/Natural Area	•
Rights-of-way	•	Water Bodies	

A.4 PROJECT AREA SHADOW PLAN

Please attach project area shadow plan to this checklist



B) HABITAT DESCRIPTION

B.1 IDENTIFY ECOLOGICAL COMPONENTS WITHIN PROJECT AREA (i.e. within a 100m buffer)

Indicate whether any of the following ecological components are located in the project area and will be affected by the proposed activity. Refer to Section 3.2.2 for assistance

North Saskatchewan River (NSR)	□ Yes	No
Water courses (excluding the NSR)	Yes	□ No
Natural Areas (Geowest 1993, Spencer 2006)	Yes	□ No
Wildlife corridors (refer to question B.3)	Yes	□ No
Wetlands (natural or constructed)	□ Yes	No
Lakes	□ Yes	■ No
Woodland (i.e. a freestanding unit of trees that is >0.5 ha)	Yes	□ No

B.2 IDENTIFY ECOLOGICAL COMPONENTS OF ADJACENT AREA (i.e. > 100m from project)

Indicate whether any of the following ecological components are located on land adjacent to the proposed activity. Refer to Section 3.2.2 for assistance

North Saskatchewan River (NSR)	Yes	□ No
Water courses (excluding the NSR)	Yes	□ No
Natural Areas (Geowest 1993, Spencer 2006)	Yes	□ No
Wildlife corridors (refer to question B.3)	Yes	□ No
Wetlands (natural or constructed)	Yes	□ No
Lakes	□ Yes	No
Woodland (i.e. a freestanding unit of trees that is >0.5 ha)	Yes	□ No

B.3 IDENTIFY POTENTIAL WILDLIFE CORRIDORS

A corridor may be present if your project area contains one of the following:			
Linear landscape features (Ridges, valleys, rivers, sharp breaks in vegetative cover)	Yes	□ No	
Identified Natural Areas (within 1 km of the project)	Yes	□ No	
Water bodies (wetlands, lakes, rivers, streams)	Yes	□ No	
Known migratory pathways	🗆 Yes	■ No	
Hedgerows, shelterbelts, windbreaks	Yes	□ No	
Greenways (a corridor of undeveloped land preserved for recreational use or environmental protection)	Yes	□ No	

Please note that some corridors are more important ecologically than others and will have greater wildlife use. For example, a natural riparian corridor will likely have a greater diversity and frequency of wildlife use than a greenway. Please refer to Section 3.2.2 for additional resources that may be used to identify wildlife corridors.



B.4 IDENTIFY HABITAT IN THE PROJECT AREA

Referencing the ecological components outlined above, please indicate the types of habitat located within 100m of the project area

Riparian (interface between land and a river or stream)	Yes	□ No	Unknown
Permanent Water Body (Stream/Lake)	Yes	□ No	🗆 Unknown
Wetland/Slough/Marsh	□ Yes	■ No	🗆 Unknown
Trees or Forested Land	■Yes	🗆 No	🗆 Unknown
Grassland/Pasture Land/ Hay Field	■Yes	□ No	🗆 Unknown

Please note: Each habitat type identified above has a corresponding species list found in Appendix B. If "unknown" is checked future studies will be required

B.5 IDENTIFY CONFLICTS WITH HABITAT

Wildlife-vehicle conflicts may occur if the project area involves the items listed below:				
Natural Area within 1 km	Yes	🗆 No	Unknown	
Upland-Wetland Habitat is Bisected	🗆 Yes	No	Unknown	
Wetland-Wetland Habitat is Bisected	🗆 Yes	■No	🗆 Unknown	
Riparian Habitat is Bisected (i.e. North Saskatchewan River Valley and any of its Tributaries)	∎Yes	□ No	🗆 Unknown	
The project has high speed (>50 km/hr)	Yes	🗆 No	Unknown	
The project has high traffic volume (non-local roads)	Yes	🗆 No	🗆 Unknown	

Wildlife mitigation will likely be required if yes is checked; additional studies may be required if unknown is checked

B.6 HABITAT: SUMMARY

Will the activity have a substantial adverse effect by habitat modifications on sensitive natural areas identified in local or regional policies or regulations?	🗆 Yes	■ No	🗆 Unknown
Will the activity have an adverse effect on locally or provincially significant wetlands through removal, filling, hydrological interruption, or others activities?	□ Yes	■No	🗆 Unknown

*Please note: Checking 'Yes' or 'Unknown' to one or more of the questions stated above, may result in the requirement for further biological studies and/or correspondence with various governing agents to determine regulatory requirements

C) WILDLIFE

C.1 ECOLOGICAL DESIGN GROUP - EDG (i.e. major species groupings that are categorized according to the type and frequency of mitigation that will be effective)

Please identify the Ecological Design Group(s) located in the project area (Refer to Section 4.3.1)						
Large Terrestrial (e.g. moose, deer)	Yes	□ No	□ Suspected	🗆 Unknown		
Medium Terrestrial (e.g. coyote, rabbit)	Yes	□ No	□ Suspected	🗆 Unknown		
Small Terrestrial (e.g. weasel, vole)	□ Yes	□ No	■Suspected	🗆 Unknown		
Amphibian (e.g. toad, salamander)	□ Yes	■No	□ Suspected	🗆 Unknown		
Aquatic (e.g. fish, mollusks)	Yes	□ No	□ Suspected	🗆 Unknown		
Aerial Mammal (e.g. bats)	□ Yes	□ No	■Suspected	Unknown		
Scavenger Birds (e.g. raven, magpie)	□ Yes	□ No	■Suspected	Unknown		
Birds of Prey (e.g. hawks, owls)	□ Yes	□ No	■Suspected	🗆 Unknown		
Water Birds (e.g. shorebirds, waterfowl)	□ Yes	■No	□ Suspected	Unknown		
Ground Dwelling Birds (e.g. grouse)	□ Yes	■No	□ Suspected	🗆 Unknown		
Other Birds (e.g. woodpeckers, songbirds)	Yes	□ No	□ Suspected	🗆 Unknown		

If suspected or unknown is checked, please refer to Appendix B for additional studies. Consult an ecologist for assistance.

C.2 RARE AND PROTECTED SPECIES

Please identify any rare or protected species (Red and Blue Listed or COWSEWIC Listed) (see Section 3.2.4.1 for further information on identifying species with status.)

There were no rare or protected species found in the vicinity of the Wedgewood creek crossing..

If any rare or protected species have been identified additional studies will be required to determine specific crossing requirements. Regulatory agencies must be contacted if rare or protected species are identified.

C.3 WILDLIFE NEEDS AND PREFERENCES

Please identify any specific needs that are required by the Ecological Design Group(s). (Refer to Section 4.3.2 for group information and Appendix B species information)

	<u>Prim</u>	ary Habit	at_		over for ement		ness/ f sight	Passage	e Type
Ecological Design Group	Wetland	Upland	Both	Yes	No	High	Low	Wet	Dry
1) Large Terrestrial									
Special requirements:									



2)Medium Terrestrial					
Special requirements:					
3)Small Terrestrial					
Special requirements:					
4)Aquatic					
Special requirements:					
Require Stream habitat Riparian zone to be vegetated					
5)Aerial Mammals					
Special requirements:					
Vegetation and tall lighting structures along the roadway will help direct bats up and over the road.					
6)Scavenger Birds					
Special requirements:					
Remove road kill off roadway					
7)Birds of Prey					
Special requirements:					
Vegetation and tall lighting structures along the roadway will help direct birds up and over the road.					
8)					
Special requirements:				tormino	

If any rare or protected species have been identified additional studies will be required to determine specific crossing requirements. Regulatory agencies must be contacted if rare or protected species are identified.

C.4 IDENTIFY PHYSICAL BARRIERS

Please identify the presence of any potential barr	iers to wi	ldlife mo	vement	
High traffic speed (>50 km/hr, see Section 3.3)	Yes	□ No	□ Suspected	🗆 Unknown
High traffic volume (i.e. arterial roads for fast moving wildlife, local roads for slow moving wildlife, Section 3.3)	■Yes	□ No	□ Suspected	🗆 Unknown
Perched culverts (see Section 3.3.4)	□ Yes	■No	□ Suspected	🗆 Unknown
Insufficient water depth for aquatic passage (i.e. water is not deep enough for organism to physically pass)	□ Yes	■No	□ Suspected	🗆 Unknown
Water velocity in excess of upstream and downstream velocity	□ Yes	■No	□ Suspected	🗆 Unknown

Page 6

Culverts without dry passage area	□ Yes	■No	□ Suspected	Unknown
Undersized Culverts (not physically large enough to accommodate EDG or becomes blocked with debris)	□ Yes	■No	□ Suspected	🗆 Unknown
Retaining walls	Yes	🗆 No	□ Suspected	🗆 Unknown
Traditional jersey barriers and/or noise barriers	Yes	🗆 No	□ Suspected	Unknown
Other	🗆 Yes	🗆 No	□ Suspected	🗆 Unknown

Please note: These barriers will affect different EDGs in different ways. Some barriers may not be applicable to your project (e.g. Jersey barriers may not be a barrier if only Large Terrestrial species are present)

C.5 WILDLIFE AND TRANSPORTATION CONFLICTS

Will the activity have a substantial adverse effect by habitat modifications on any species with status identified in local or regional policies or regulations?	□ Yes	■ No	🗆 Unknown
Will the activity interfere with previously existing wildlife corridors?	■Yes	□ No	🗆 Unknown
Will the activity interfere with the movement of any resident or migratory fish species?	□ Yes	■No	🗆 Unknown
Will the activity interfere with the movement of any non-fish wildlife species?	■Yes	□ No	🗆 Unknown
Please note: Checking 'Yes' or 'Unknown' to one or more of the questions stated for further biological studies and/or correspondence with various governing ager requirements			
C.6 WILDLIFE: SUMMARY			
a) Please summarize whether a conflict will exist between the pr	-		
a) Please summarize whether a conflict will exist between the pr (Refer to Section 3.3.5)	oject and ■ Yes		in the area?] No
	Yes] No
(Refer to Section 3.3.5)	Yes	e road be] No
 (Refer to Section 3.3.5) b) Can this conflict be avoided (Refer to Section 3.4)? For examp avoid the habitat feature that is attracting wildlife passage? 	■ Yes le, can th □ Yes	e road be	∃ No e realigned to ∎No
(Refer to Section 3.3.5) b) Can this conflict be avoided (Refer to Section 3.4)? For examp	■ Yes le, can th □ Yes	e road be	∃ No e realigned to ∎No

Wildlife mitigation will be required if "no" is checked for 3.6b or "yes" is checked for 3.6c.

D) PROPOSED SOLUTIONS

Please indicate what types of solutions will be used to mitigate for the disturbance to wildlife in the project area (include activities for before, after, and during project implementation).



Retention of existing habitat	Yes	□ No
Habitat protection during construction	Yes	□ No
Ensuring functionality of wildlife corridors during construction	■Yes	□ No
Wildlife passage (continue with Section E of this checklist)	Yes	□ No
Restoration or enhancement of existing habitat (provide initial recommendations in Section F of this guideline)	∎Yes	□ No
Management Plan	🗆 Yes	No
Monitoring	□ Yes	No

Please note: plans for proposed solutions are to be described in greater detail at detailed design phase

E) POTENTIAL MITIGATION OPTIONS TO MINIMIZE WILDLIFE - TRANSPORTATION CONFLICTS

E.1 IDENTIFY APPROPRIATE MITIGATION (Section 4.0 and Checklist 12.2 of guidelines)

a) Please indicate which mitigation possibilities meet the ecological, transportation, and regulatory requirements for your project (refer to Section 4.4 and 4.5). This table corresponds to Table 4.4 and is designed to help determine what mitigation options meet the needs of wildlife and transportation as well as regulatory requirements. If an option does not meet all three then a discussion with interested parties may be required to prioritize the proposed mitigation strategy. More than one mitigation option may meet all three requirements. In this case, the best option should be chosen or a combination of several should be considered.

	Needs and/or Requirements				
Mitigation Tool (Section of Guidelines)	Ecological	Transportation	Regulatory		
Signage and/or Reflectors (4.5.1)					
Fencing (4.5.2)					
Altered Lighting (4.5.3)					
Altered Sight Lines (4.5.4)					
Public Education (4.5.5)					
Traffic Calmed Areas (4.5.6)					
Reduced Speed Limits (4.5.7)					
Wildlife "Crosswalk" (4.5.8)					
Diversionary Methods (4.5.9)					
Reduce/Remove Roadkill (4.5.10)					
Vegetation Management (4.5.11)					
Noise Barriers (4.5.12)					
Curb Improvements (4.5.13)					
Closed Bottom Culvert (4.5.14)					
Amphibian Tunnel (4.5.14)					
Open Bottom Culvert (4.5.14)					

48

Box Culvert (4.5.14)		
Bridges (4.5.15)		
Tunnel/Overpass (4.5.16)		
Passage Required for multiple species (4.6)		

b) Please identify the crossing mitigation(s) that will BEST meet all the requirements

Wildlife underpass (bridge structure for terrestrial species

Culvert for aquatic species

E.2 MITIGATION SIZE

If culvert or bridge-like structures are selected, please calculate the size of mitigation required. This will vary depending on the Ecological Design Group (EDG) and the size of the road. Use the openness calculation to help assess mitigation size (Refer to Section 4.3.3)

	Openness	Ratio (m)			
Openness = Height x Width Length	Large Terrestrial	Medium Terrestrial	Small Terrestrial	Amphibian	Aquatic
Length	1.5	0.4	≤0.4	0.16	Encompasses entire channel width

EDG Preferred Openness	1.5
Structure Length	31.0m
Structure Width	10.33m
Structure Height	4.5m

E.3 MITIGATION FREQUENCY

If the project area encompasses a large portion of the EDGs home range, several structures may be required to reduce vehicle-wildlife collisions and provide habitat connectivity. Please refer to Section 4.3.5 for assistance in determining if multiple structures are required and how close they must be placed.

N/A

F) IDENTIFY POTENTIAL LOCATIONS FOR HABITAT RESTORATION

Please identify any possibilities for restoration of habitat and connectivity. This could include



restoring portions of a damaged creek or re-planting trees. Refer to Section 3.2.3.

Construction activities will be closely monitored & mitigation techniques will be in place.

A new culvert will be installed.

Any trees that need to be removed for construction can be replanted.

Wildlife underpass concept has been designed, to mitigate wildlife/vehicle collisions

Open bottom wildlife passage will encourage natural habitat

Retailing walls for passage to be landscaped/vegetated or disguised with strategic plantings

G) COST-BENEFIT ANALYSIS

A cost-benefit analysis may be completed to determine the relative need for a structure. Please note that a cost-benefit analysis may not adequately reflect the value of important habitat and rare species. Please refer to Section 4.3.6 for additional information

H) REGULATORY CHECKLIST

This checklist provides a summary of common legislation that may be applicable to the project. Additional legislation may apply depending on the area. Please refer to Appendix C for additional information on regulatory requirements.



I) IMPORTANT REFERENCE TABLES

The reference tables below have been taken directly from the Wildlife Passage Engineering Design Guidelines. They are reproduced here only for ease of reference.

Table 4.1 - Species and Design Groups Summary

Design Group*	Example	General Habitat Information		
Large Terrestrial	 Moose ** Deer 	Need forested area for cover, and ungulates require considerations for grazing needs. Primary ungulate activit occurs at dawn or dusk. Ungulate activity near roads peak during the fall and spring. Ungulates are more aggressive and less cautious during the fall rut.		
Medium Terrestrial	 Porcupine Coyote Rabbit 	Mixture of habitat requirements: Porcupines require forested habitat; badgers require open habitat; and coyotes or hares may live in either.		
mall Terrestrial	 Mouse Red Squirrel Weasel 	Mixture of habitat requirements: Red squirrels require forested habitat, while ground squirrels require open habitat. Weasels and some mice may inhabit either.		
Amphibians	 Canadian toad Tiger salamander 	Requires moist substrates and semi- permanent to temporary water for tadpole stage depending on species. Also need access between lowland and upland habitat for feeding and dispersal.		
Aquatic	 Lake Sturgeon Northern Pike Longnose Sucker Mollusks 	Need aquatic habitats with flow velocities low enough to allow for upstream movement and dispersal. Substrate in habitat must allow for cover and resting locations, and appropriate substrate may be needed for breeding. Access to overwintering habitats for most fish is essential. For mollusks, substrates must be conducive for attachment.		
Aerial Mammals	 Little Brown Bat Northern Long-eared Bat 	Require feeding and nesting locations with access in between. Nesting site needs vary by species. Nesting sites must remain undisturbed during winter hibernation.		
Scavenger Birds	 Raven Crow Magpie 	Need sufficient habitat for nesting and safe foraging. Mos populations are not at risk; however their overpopulation may put other species at risk.		
Birds Of Prey	 Red Tailed Hawk Great Horned Owl 	Requirements vary; many species require relatively undisturbed nesting sites, while others may nest near human habitation. Require safe foraging habitat, and safe migration routes and destinations.		
Water Birds	 Seasonal Ponds: Mallard, Shorebirds Permanent Water: Golden Eye, Bufflehead 	Require open water and/or appropriate shoreline for feeding and nesting, varying by species. Most are ground- nesting and thus require safe, undisturbed sites for nesting. Nesting habitat requirements varies by species. Require safe migration routes and destinations.		



*Please be advised that these groupings are very general and that variations in requirements for each species within the design groups may exist. Also note that these groupings do not take into consideration feeding habitat, breeding habitat, or seasonality.

A single species may fall into more than one Ecological Design Group.

** Moose may be more common on the outskirts of the City while deer are more common in the river valley.

Design Group*		Example	General Habitat Information		
	Ground Dwelling Birds	 Gray Partridge Sharp-tailed Grouse 	Require safe open habitats for foraging and nesting. Nesting requires safe open grassy or shrubby areas. Require safe migration routes and destinations. Ground nesting birds should be included in this category during nesting season.		
		1. Downy woodpecker (Core Forested)			
	Other Birds	 Black Capped Chickadee (Edge/Woodland) 	Requirements vary significantly by species. Most species require at least some forested habitat for nesting and perching, although some are ground nesting or nest in		
×		3. Grasshopper Sparrow (Grassland)	wetland vegetation or shrubs. Most are migratory and require safe migration routes and destinations.		
		 Red-winged Blackbird (Wetland) 			

Table 4.4 - Mitigation Summary Table

Option	Mitigation	Ecological Requirements	Transportation Requirements
1	<u>Signage and/or</u> <u>Reflectors</u>		Lower volume roads. If it is going to be used on roads with higher volume or speed, it should be combined with other mitigation.
2	Fencing*		Can be used on any road but may not be cost effective for minor roads.
3	Altered Lighting*		ALL
4	Altered Sight Lines		Multi-use trails. May also be used if sight of human activity deters use of a crossing
5	Public Education		ALL
6	Traffic Calmed Areas		Suitable for roads with average speed below 50km/hr or in an area with high bird breeding densities.
7	Reduced Speed Limits		Useful in areas of high wildlife-vehicle collisions
8	Wildlife "Crosswalk"		Roads with low traffic volume. Should be used in conjunction with signs.

9	Diversionary Methods	Other birds using bridges as habitat	Effective for bridges and any road with wildlife foraging along the right-of-way
10	Reduce/Remove Road kill		Suitable for all roads
11	Vegetation Management		Suitable for all roads
12	Noise Barriers		Roadway that is near valuable nesting habitat for birds (eg. near a wetland). Note: this will behave as a barrier to terrestrial wildlife.
13	Curb Improvements		Useful in all areas where small wildlife may be trapped on the road.
14	Closed Bottom Culvert [†]		Suitable for roads crossing minor drainage channels. May also be used in areas without drainage to assist small and medium terrestrials. In areas with drainage, ledges on the sides may be used to accommodate some terrestrial species.
15	Amphibian Tunnel		Any road running bisecting wetland-upland habitat or wetland-wetland habitat
16	Open Bottom Culvert**		Suitable for roads crossing minor drainage channels. May also be used in areas without drainage to assist small and medium terrestrials.
17	Box Culvert**		Suitable for roads crossing larger drainage channels. May also be used in areas without drainage to assist small and medium terrestrials
18	Bridges**		Requires grade separation
19	Tunnel/Overpass		Effective in sensitive natural areas, areas without grade separation, areas where the terrain on either side of the road is higher than the road.

Should be complementary to other mitigation and not used as a stand alone treatment

** Improvements are required for more than one Ecological Design Group to benefit from this crossing
 * Should only be used in areas that do not have critical fish habitat or species at risk. Stream widths must be less than 2.5 m and gradients less than 6%.

APPENDIX L

Open House Invite & Resident Comments



February 10, 2014 File: 1161102460

Dear Property Owner or Resident,

Reference: Open House Invitation - Riverview Neighbourhood Structure Plans

The Riverview Area Structure Plan (ASP) was approved by Council in July 2013. Stantec Consulting has now started work on Neighbourhood Structure Plans (NSPs) for three neighbourhoods within the Riverview area (see attached). These NSPs will provide additional details based on higher level policies in the Riverview ASP.

Stantec is pleased to invite you to attend an Open House to discuss the preliminary concepts for NSPs, review the associated planning and engineering requirements, and provide information on the planning process and timing.

Date:	Tuesday, February 25 th , 2014
Time:	6:30 pm – 8:00 pm
Location:	Edmonton Petroleum Golf & Country Club 51320 Range Road 260 (Winterburn Road SW) Spruce Grove, AB T7Y 1B1

If you have any questions or comments feel free to contact Nick Dyjach at nick.dyjach@stantec.com (780-917-6683).

STANTEC CONSULTING LTD.

Nick Dyjach Planner (780) 917-6683 nick.dyjach@stantec.com

 $dn \ (cd1001-c200) \ workgroup \ 1161\ (active \ 1161\ 102460) \ reports \ open \ house \ - \ feb.\ 25,\ 2014\ (and workgroup \ 1161\ active \ 1161\ 102460) \ reports \ (active \ 1161\ active \ 1161\$

Starter Starter	ATTENDEE SIGN IN SHEET	Your name and address are being collected by Stantec Consulting for future contact regarding information on the proposed application.	SIGNATURE	E-MAIL	780916 3030	This information is protected under the authority of section 33(c) of the Freedom of Information and Protection of Privacy Act. Your name and contact information WILL NOT be released to third parties, nor be used by the Stantec for unrelated purposes, without your express consent. To ensure your privacy, please drop this form in the secured box provided.	Should you have questions regarding the use of personal information collected, please speak to any Stantec staff present at this meeting or contact Stantec Consulting, 10160-112 Street, (780) 917-7000.	
Riverview Neighbourhood Structure Plan February 25, 2014	ATTENDEE	Your name and address are being collected by Stantec Co application.	SIGNATION CONTRACTOR SIGNATION CONTRACTOR SIGNATION SIGNATIO	ADDRESS & POSTAL CODE	104 West Seal Werd	This information is protected under the authority of section 33(c) of the Freedom Act. Your name and contact information WILL NOT be released to third parties, purposes, without your express consent. To ensure your privacy, please drop this form in the secured box provided.	Should you have questions regarding the use of personal information collected, p at this meeting or contact Stantec Consulting, 10160-112 Street, (780) 917-7000.	

Kiverview Neignbournood Suucture Fran Stakeholder Advisory Group February 25, 2014
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ATTENDEE SIGN IN SHEET

Your name and address are being collected by Stantec Consulting for future contact regarding information on the proposed application.

SIGNATURE	Brid	E-MAIL	
NAME (PLEASE PRINT)	The S. P. SINGH, BASANTI SINGH	ADDRESS & POSTAL CODE	

Act. Your name and contact information WILL NOT be released to third parties, nor be used by the Stantec for unrelated This information is protected under the authority of section 33(c) of the Freedom of Information and Protection of Privacy purposes, without your express consent.

To ensure your privacy, please drop this form in the secured box provided.

Riverview Neighbourhood Structure Plan Stakeholder Advisory Group February 25, 2014	S. 24 S. 25 S. 25
ATTENDEE SIGN IN SHEET	IGN IN SHEET
Your name and address are being collected by Stantec Const application.	Your name and address are being collected by Stantec Consulting for future contact regarding information on the proposed application.
NAME (PLEASE PRINT)	SIGNATURE
PAUL YUSYPCMUK	florall
ADDRESS & POSTAL CODE	E-MAIL
123-20558 5W	Faul. Yusypchule Nultr ca
This information is protected under the authority of section 33(c) of the Freedom of Information and Protection of Privacy Act. Your name and contact information WILL NOT be released to third parties, nor be used by the Stantec for unrelated purposes, without your express consent.	the authority of section 33(c) of the Freedom of Information and Protection of Privacy ation WILL NOT be released to third parties, nor be used by the Stantec for unrelated isent.
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Should you have questions regarding the use of personal information collected, please speak to any Stantec staff present at this meeting or contact Stantec Consulting, 10160-112 Street, (780) 917-7000.	ormation collected, please speak to any Stantec staff present eet, (780) 917-7000.

Structure Plan			
Riverview Neighbourhood Structure Plan	Stakeholder Advisory Group	February 25, 2014	



ATTENDEE SIGN IN SHEET

Your name and address are being collected by Stantec Consulting for future contact regarding information on the proposed application.

SIGNATURE	Bart	E-MAIL	Without a deliver a church con
NAME (PLEASE PRINT)	BRAN NELAAN	ADDRESS & POSTAL CODE	ILS Grandish Ways TLOM DN7

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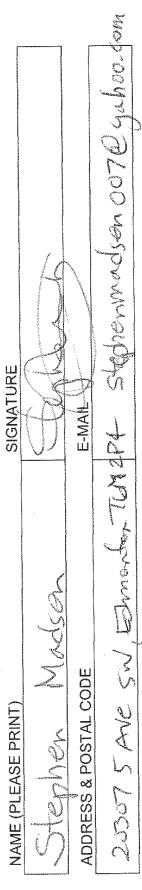
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Riverview Neighbourhood Structure Plan Stakeholder Advisory Group February 25, 2014



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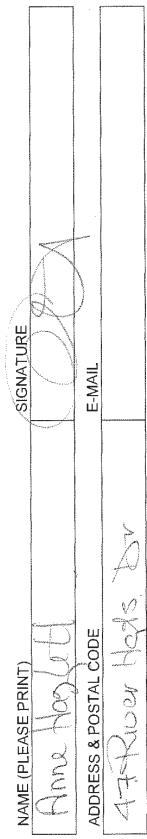
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Riverview Neighbourhood Structure Plan Stakeholder Advisory Group February 25, 2014



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Riverview Neighbourhood Structure Plan Stakeholder Advisory Group February 25, 2014	Stanto Stanto
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Should you have questions regarding the use of personal information collected, p at this meeting or contact Stantec Consulting, 10160-112 Street, (780) 917-7000.	Should you have questions regarding the use of personal information collected, please speak to any Stantec staff present at this meeting or contact Stantec Consulting, 10160-112 Street, (780) 917-7000.
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Riverview Neighbourhood Structure Plan February 25, 2014	ATTENDEE	Your name and address are being collected by Stantec Co application.	NAME (PLEASE PRINT)	ADDRESS & POSTAL CODE	This information is protected under the authority of section Act. Your name and contact information WILL NOT be rele purposes, without your express consent.	To ensure your privacy, please drop this form in the secured box provided.	Should you have questions regarding the use of personal information collected, p at this meeting or contact Stantec Consulting, 10160-112 Street, (780) 917-7000.	

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Riverview Neighbourhood Structure Plan	stakeholder Advisory Group	⁻ ebruary 25, 2014	
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Riverview Neighbourhood Structure Plan February 25, 2014	ATTEND	Your name and address are being collected by Stantec application.	NAME (PLEASE PRINT)	206-53302 RR 261 SPD 46 62005 774 117	This information is protected under the authority of sect Act. Your name and contact information WILL NOT be purposes, without your express consent.	To ensure your privacy, please drop this form in the secured box provided.	Should you have questions regarding the use of personal information collected, p at this meeting or contact Stantec Consulting, 10160-112 Street, (780) 917-7000.	

Riverview Neighbourhood Structure Plan	
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Riverview Neighbourhood Structure Plan Stakeholder Advisory Group February 25, 2014 ATTENDEE SIGN IN SHEET	
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HURS NAME (optional): WER FREIGHTS DRUGE ADDRESS (optional):

COMMENT FORM – Riverview Neighbourhood Structure Plan

We would appreciate your comments and concerns regarding any part of the proposal.

COMMENTS: Ġ

Please leave your comments form with staff tonight; or

Fax to Stantec (780) 917-7179 – Attention: Nick Dyjach Email to: nick.dyjach@stantec.com

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Luesday, February 25, 2014

NAME (optional): ADDRESS (optional):

COMMENT FORM - Riverview Neighbourhood Structure Plan

We would appreciate your comments and concerns regarding any part of the proposal.

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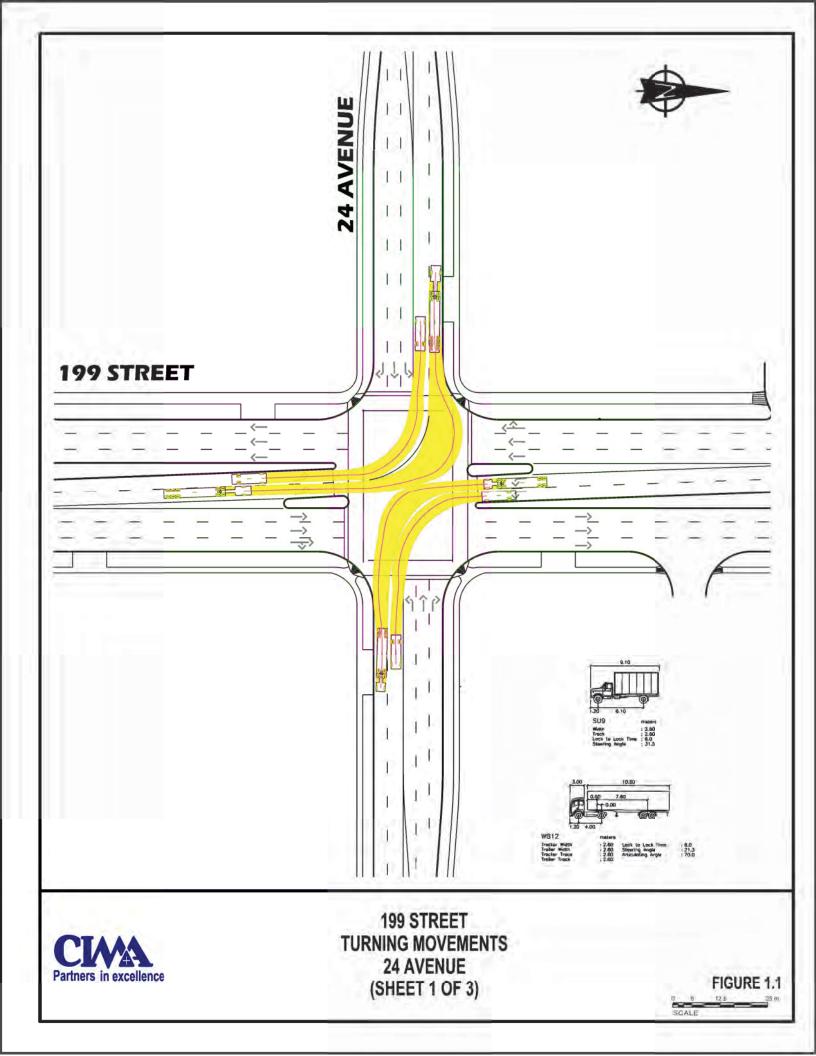
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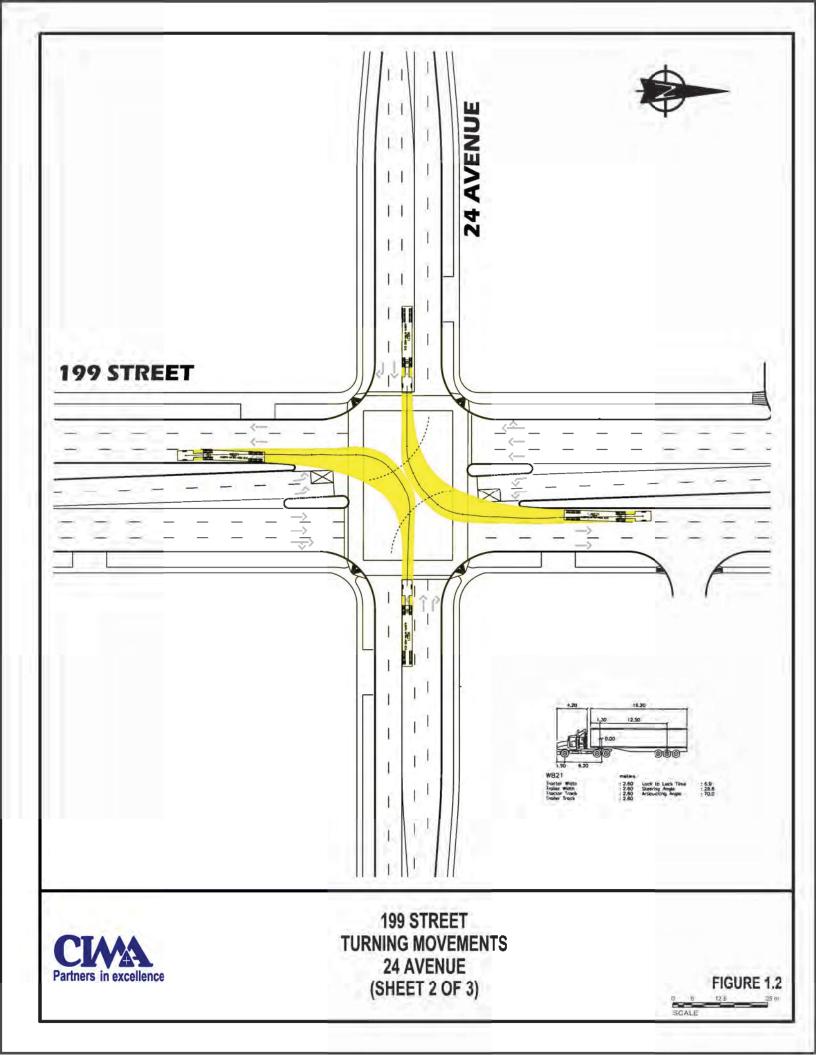
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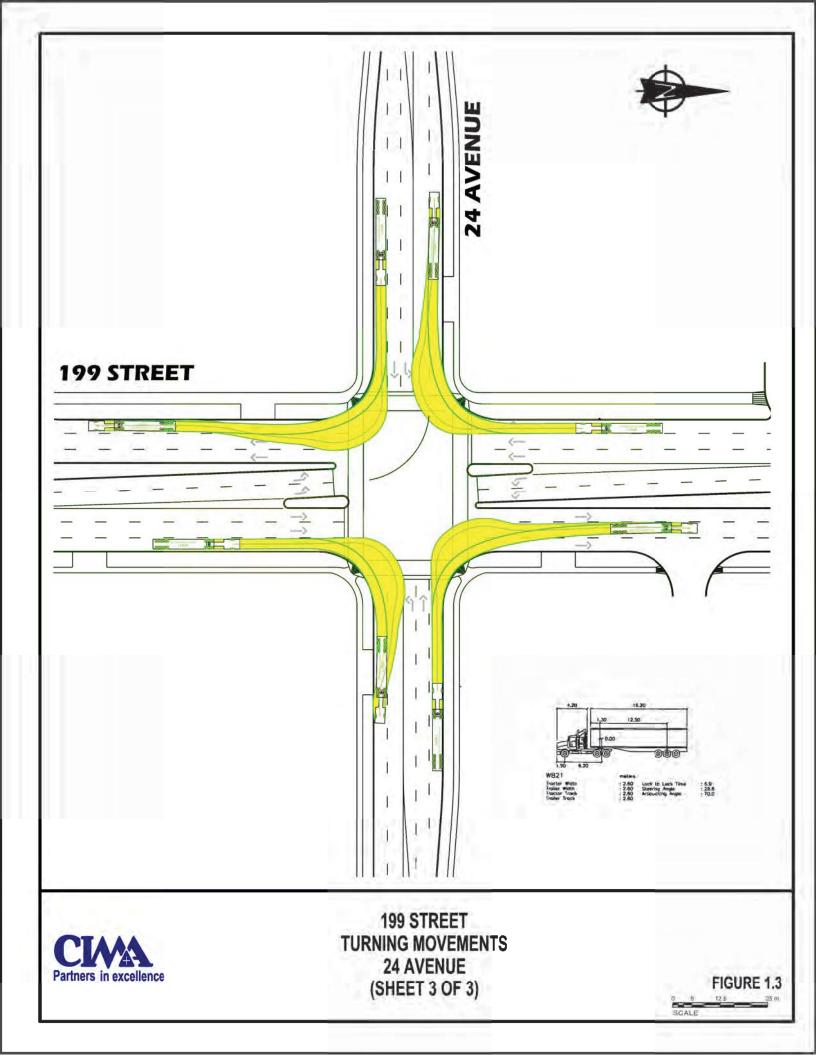
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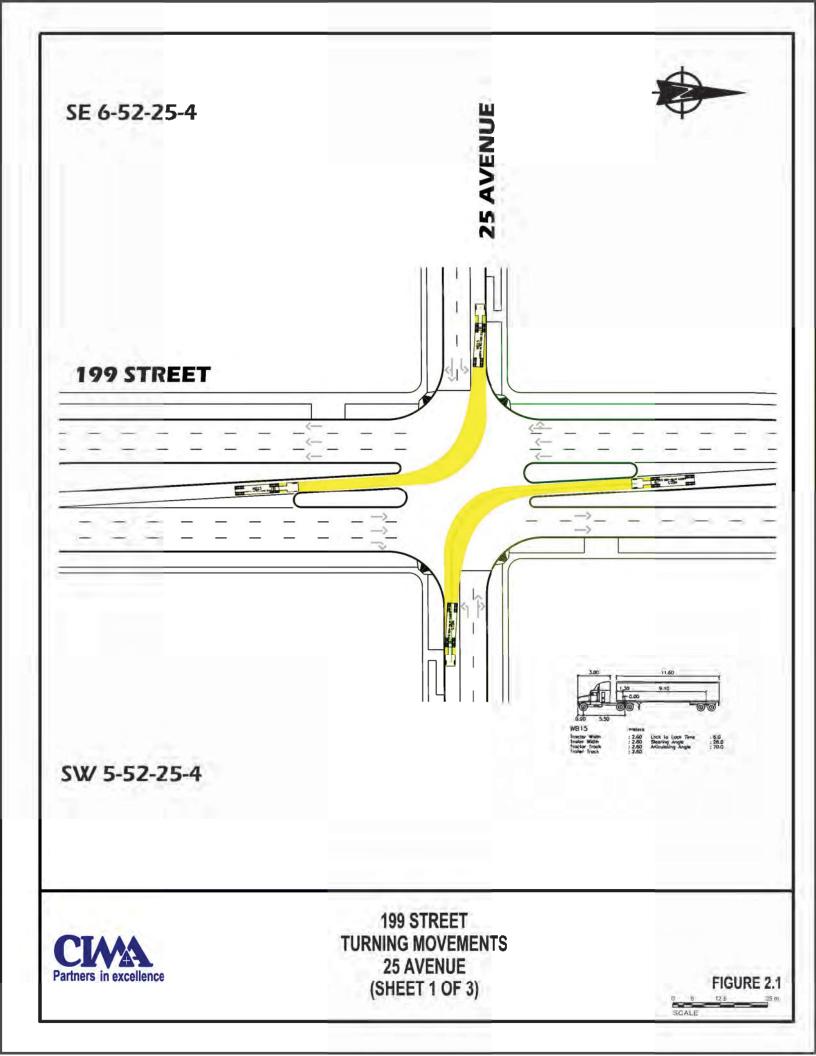
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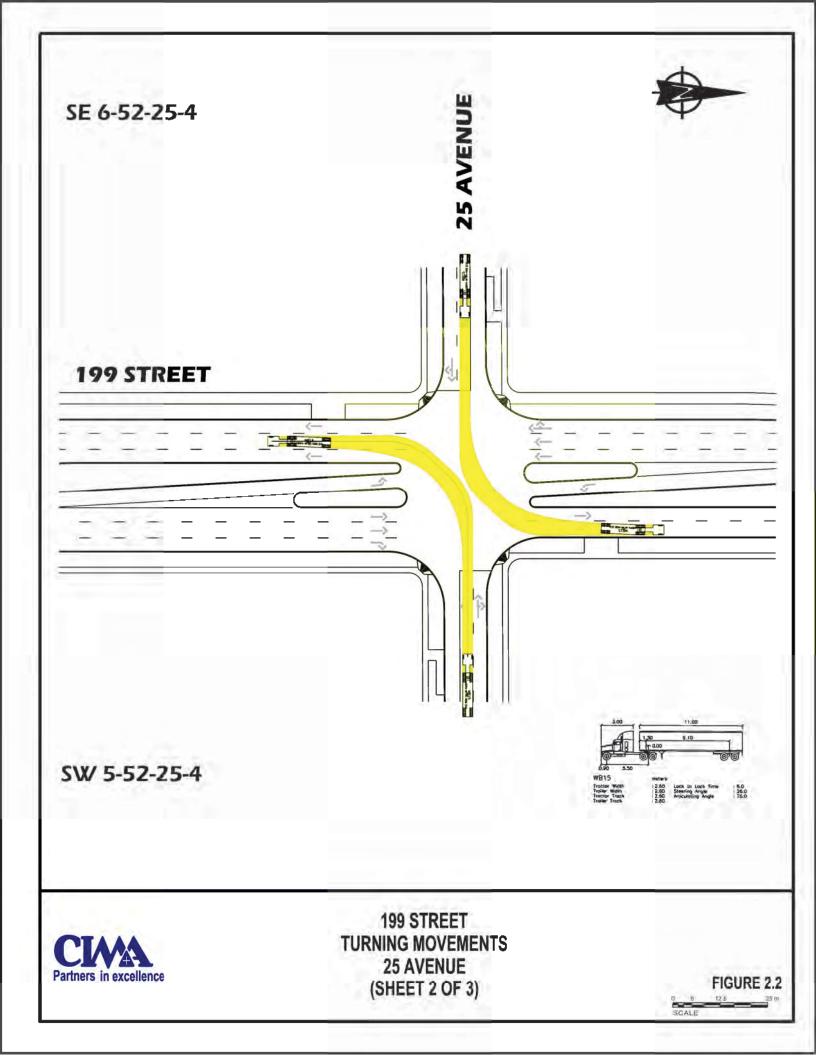
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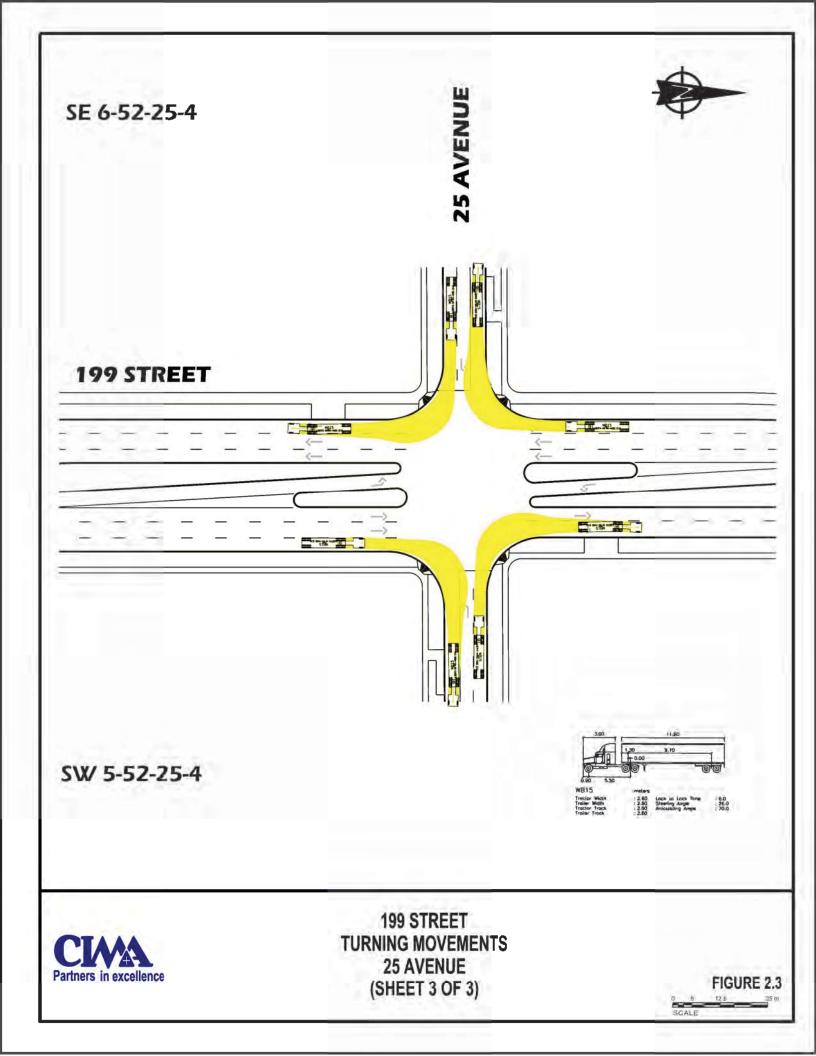


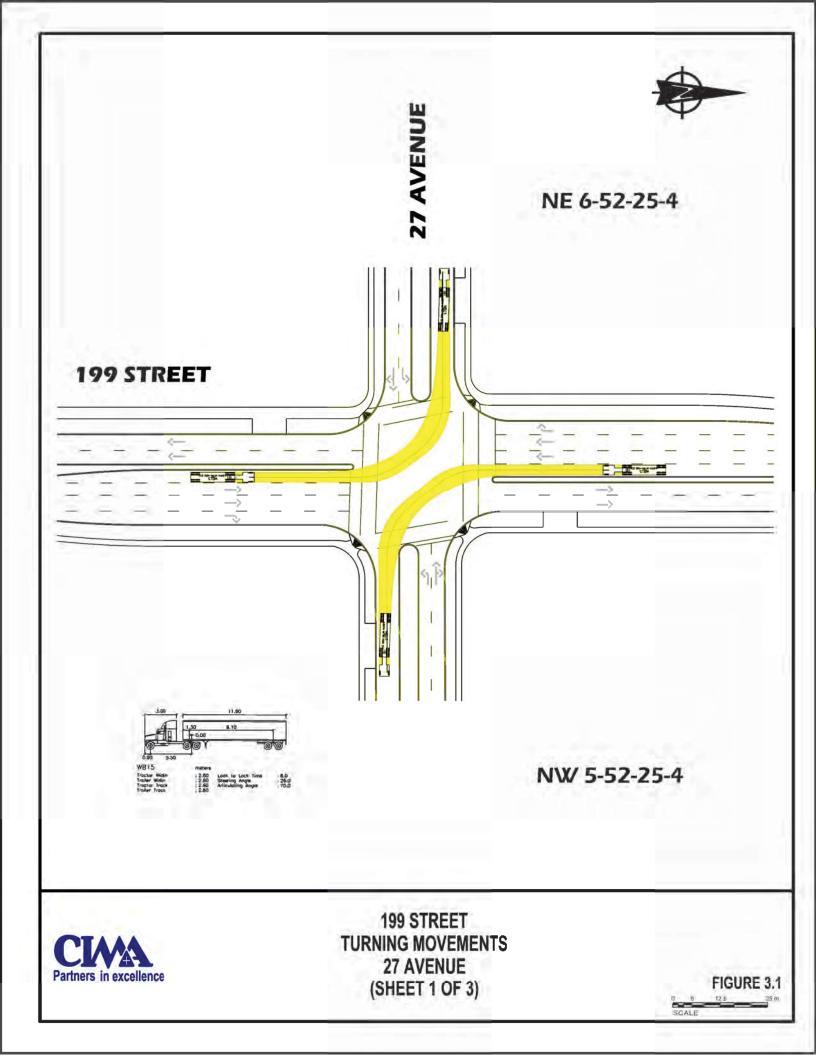


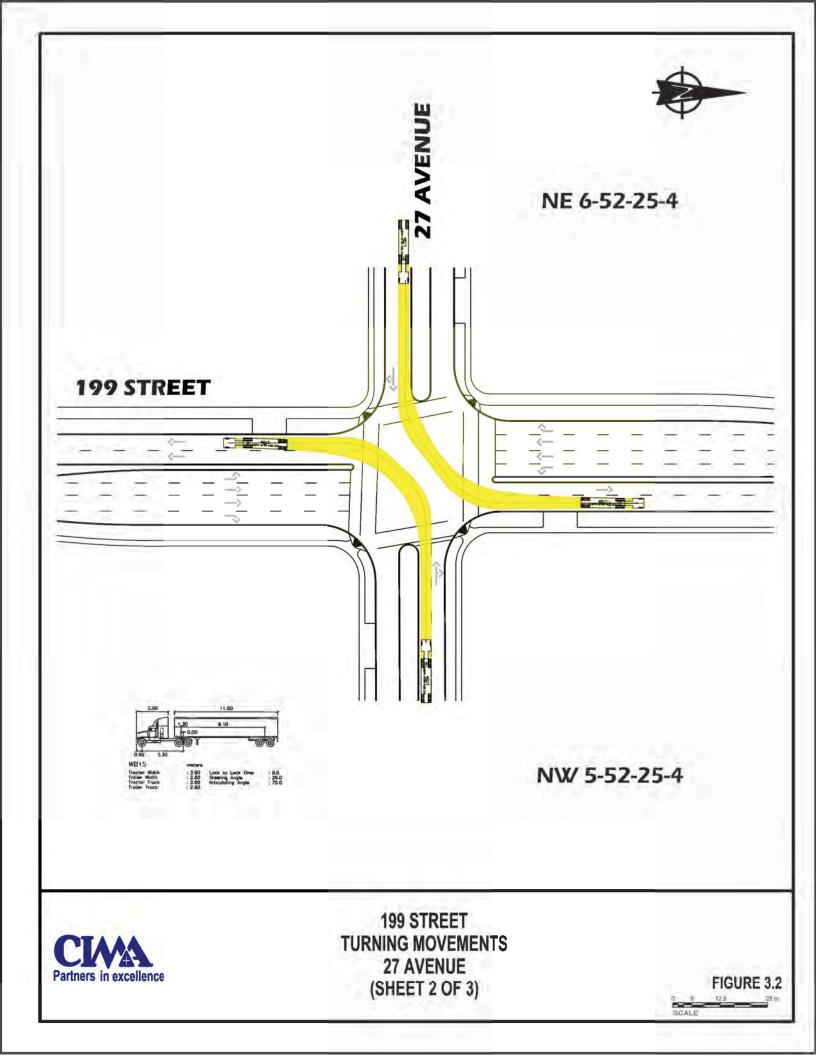


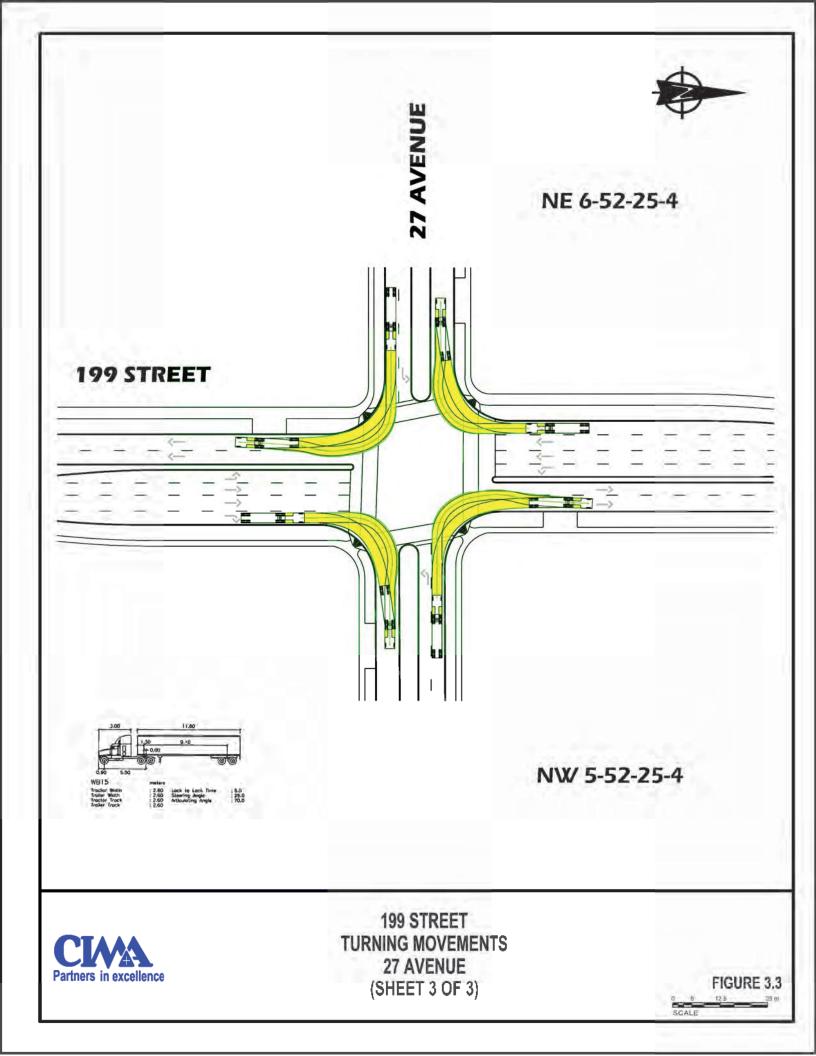


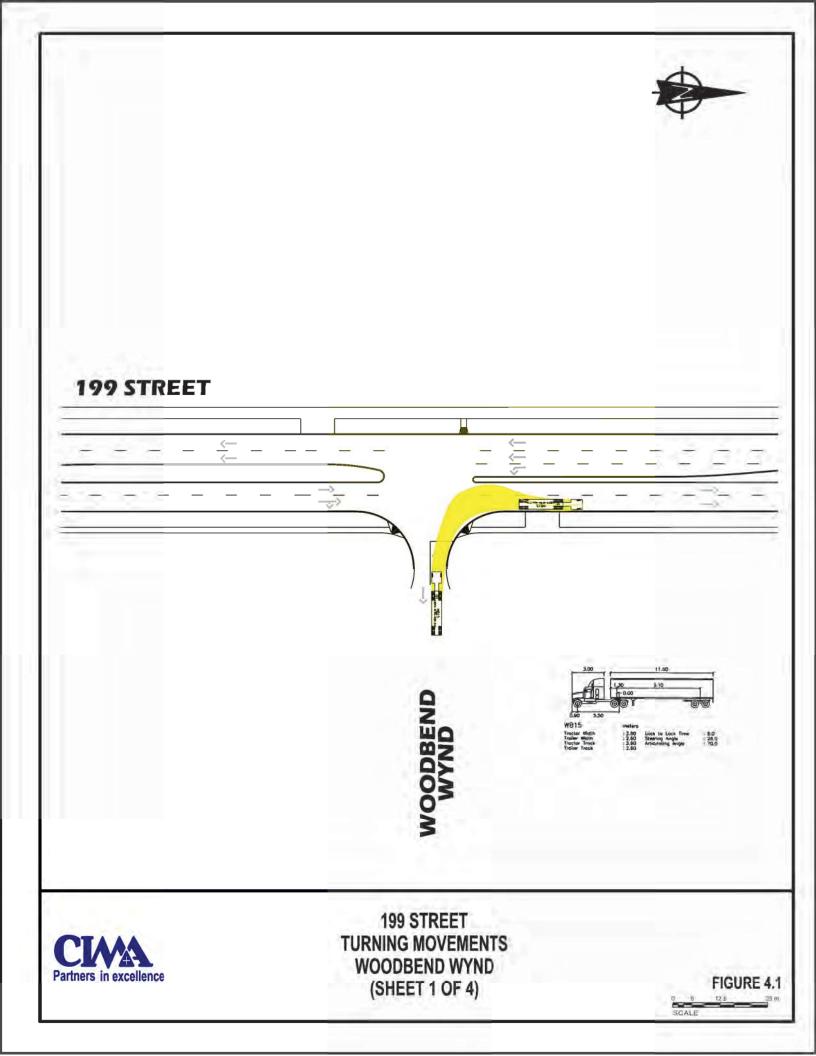


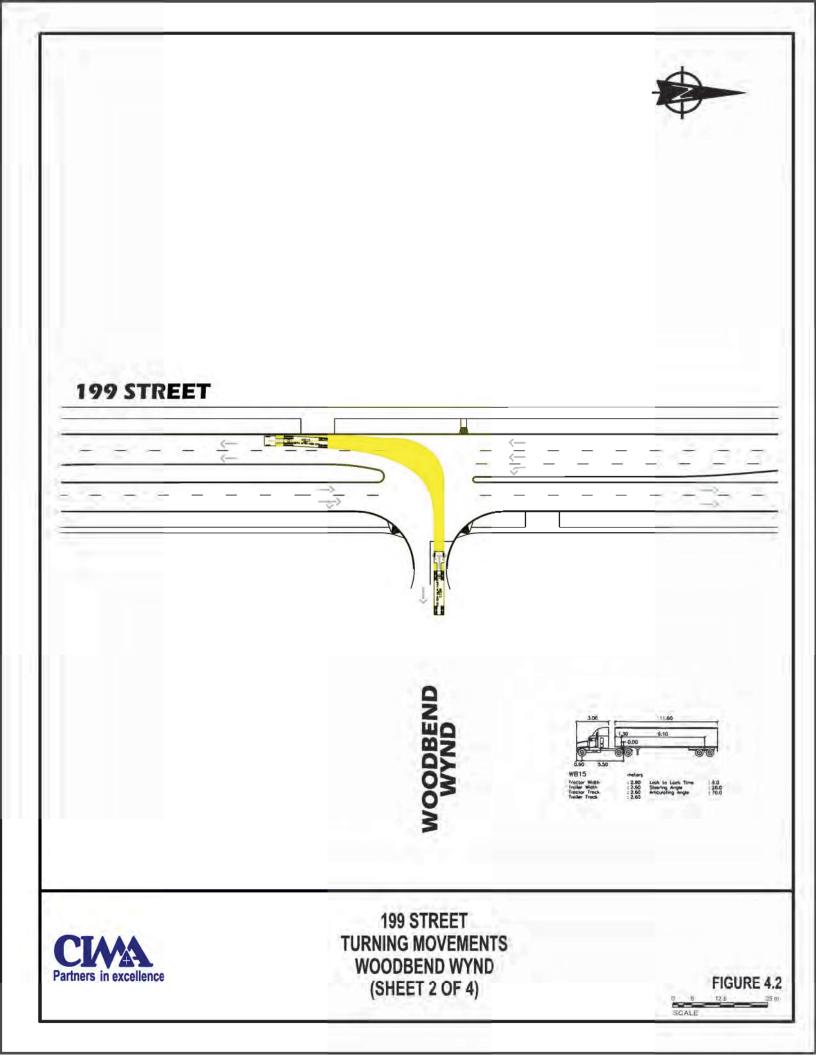


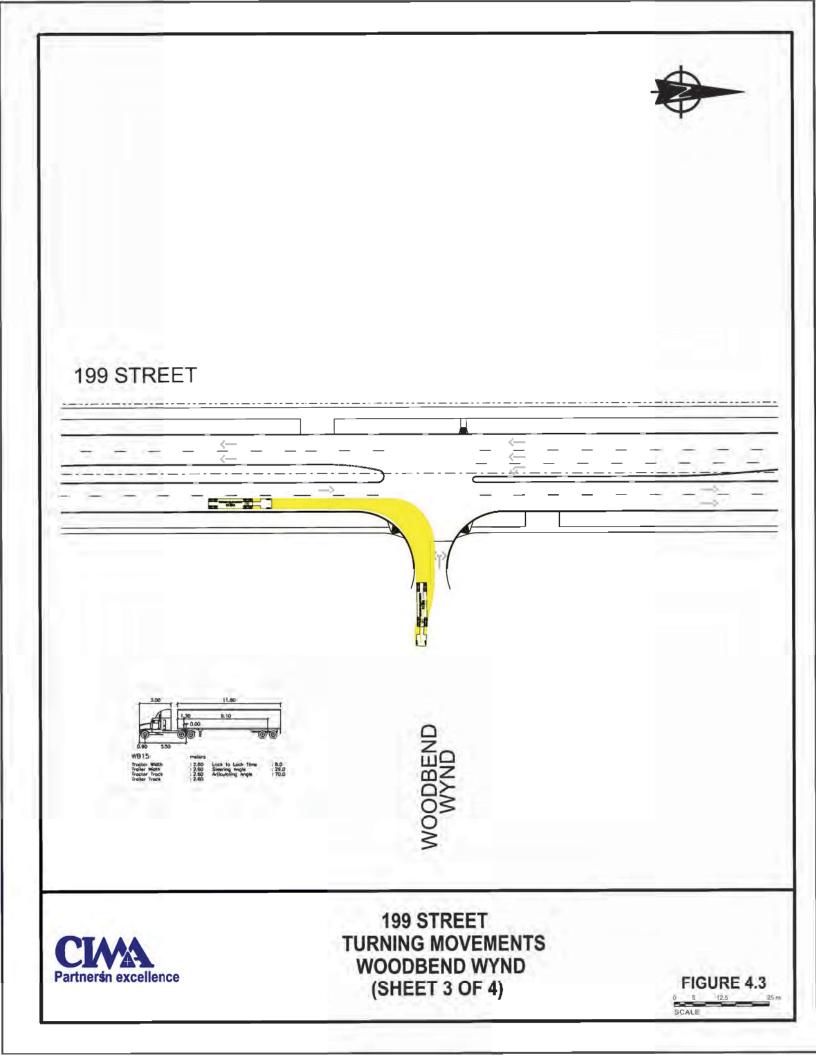


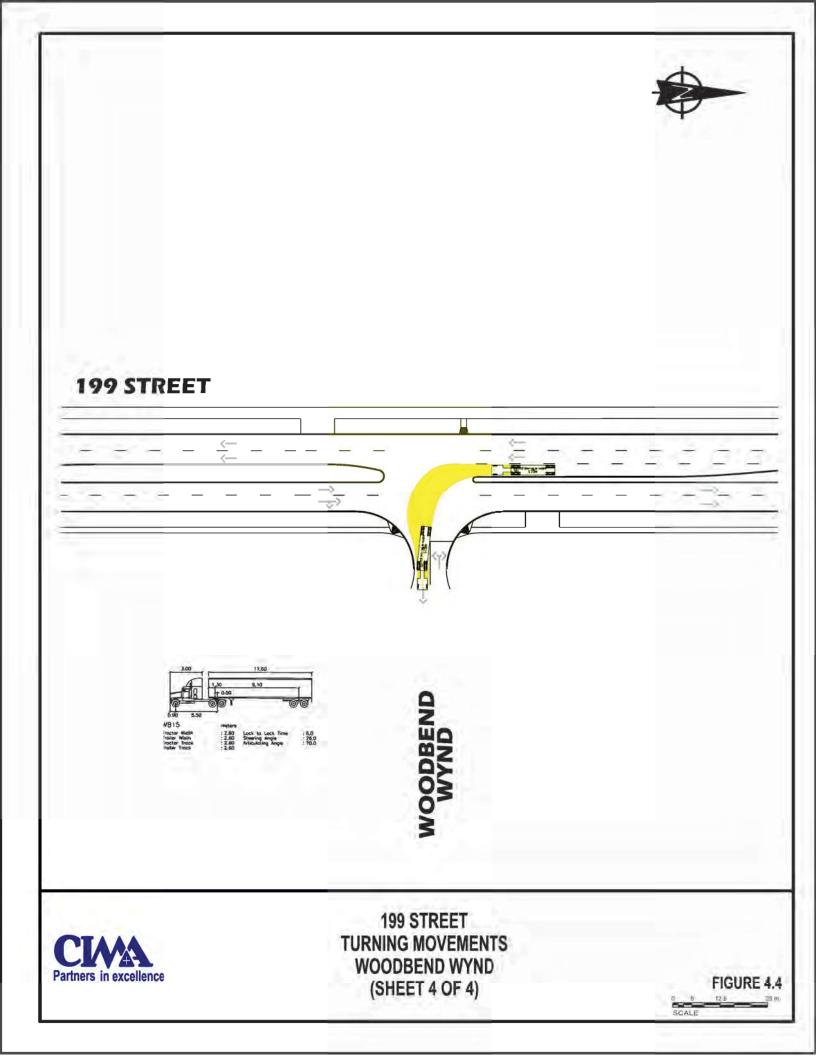








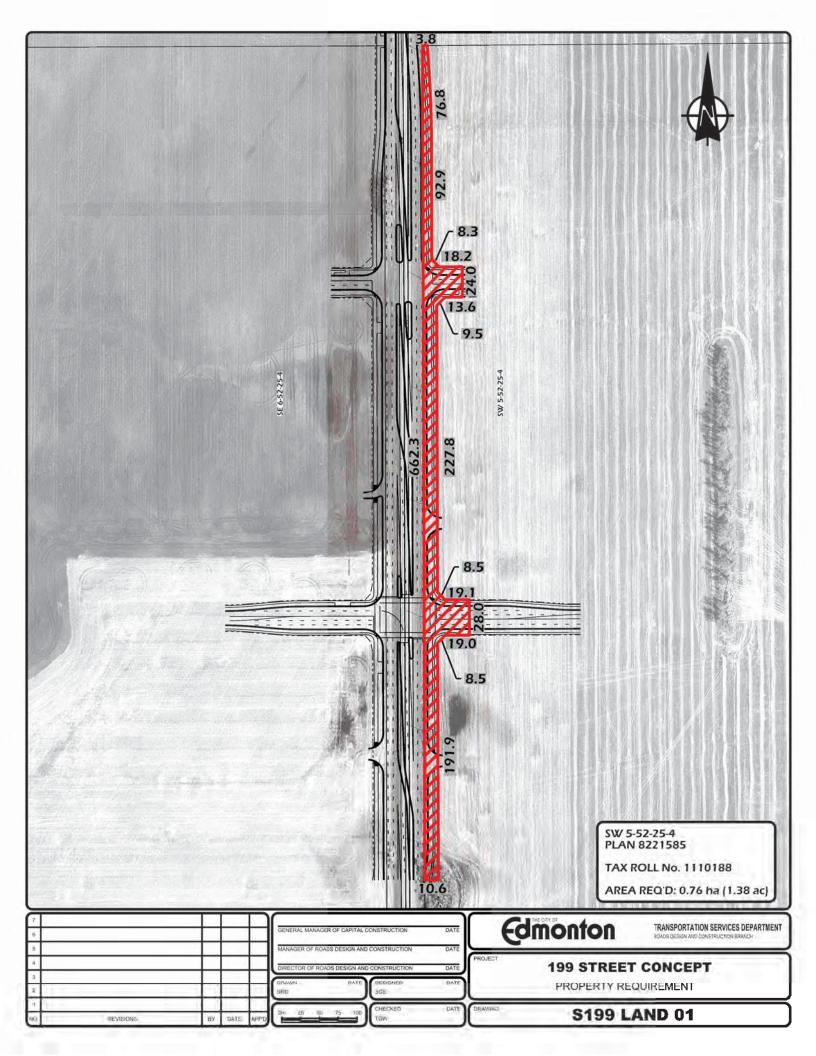


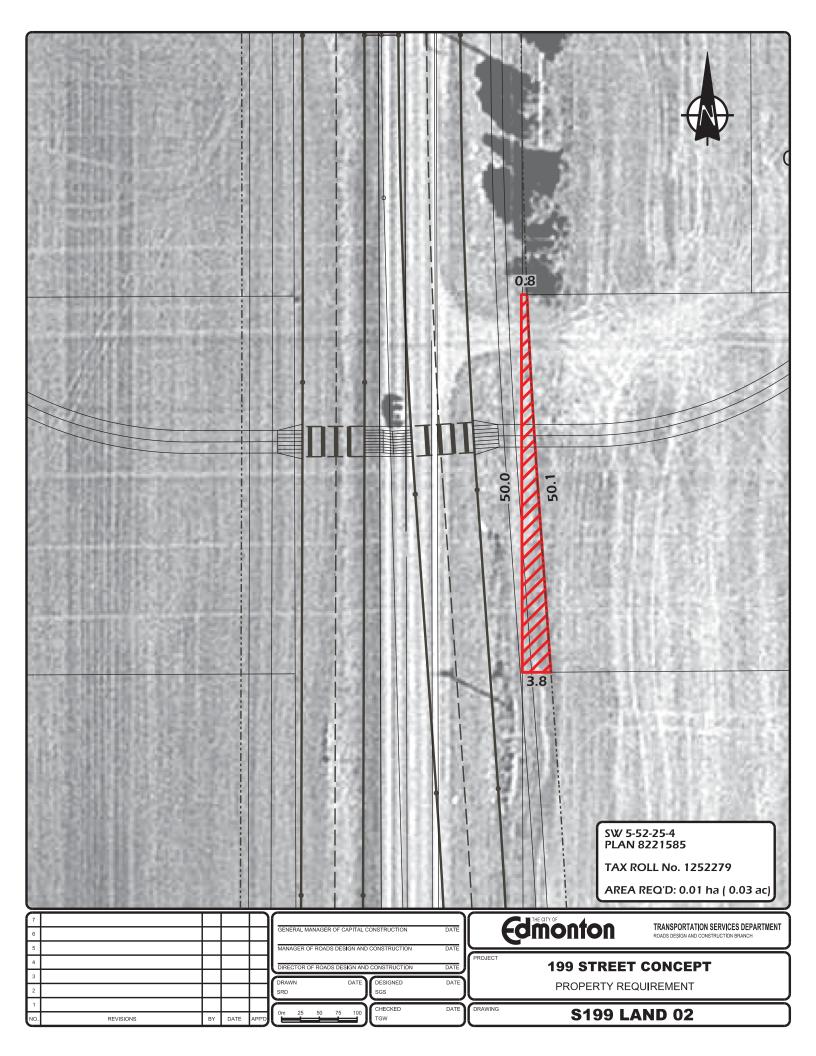


City of Edmonton 199 Street (23 Avenue to 35 Avenue) Concept Report – Final Submission | February 2015

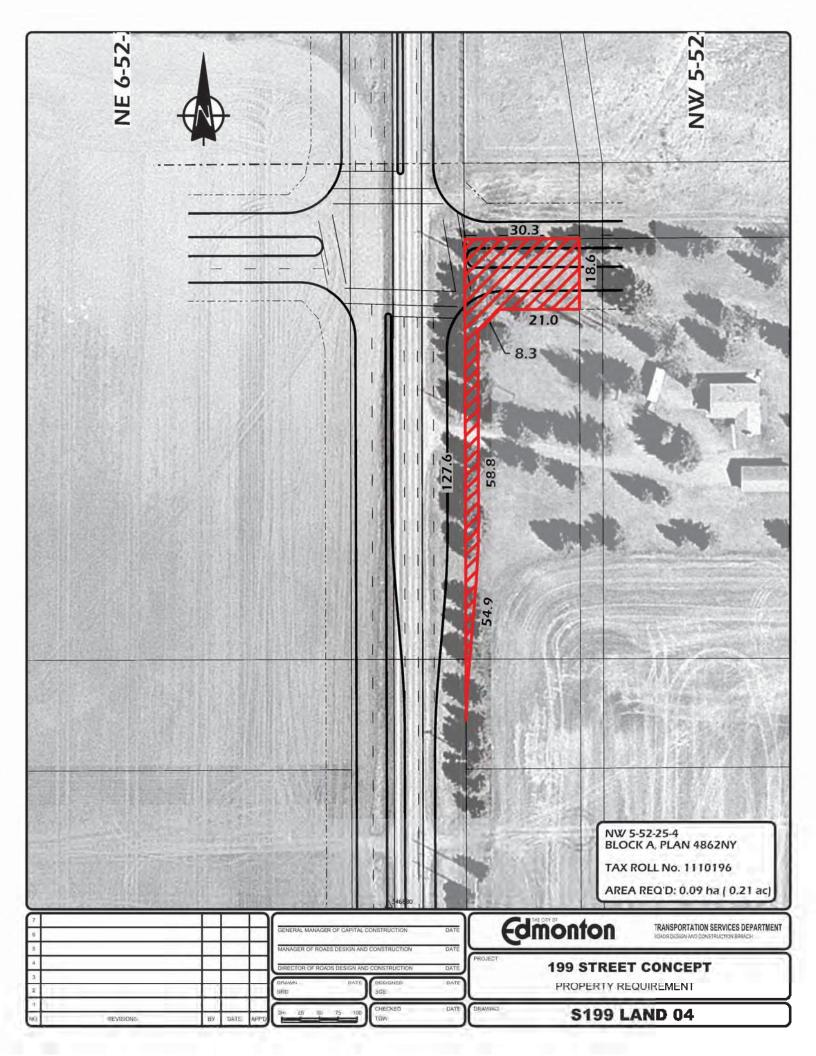


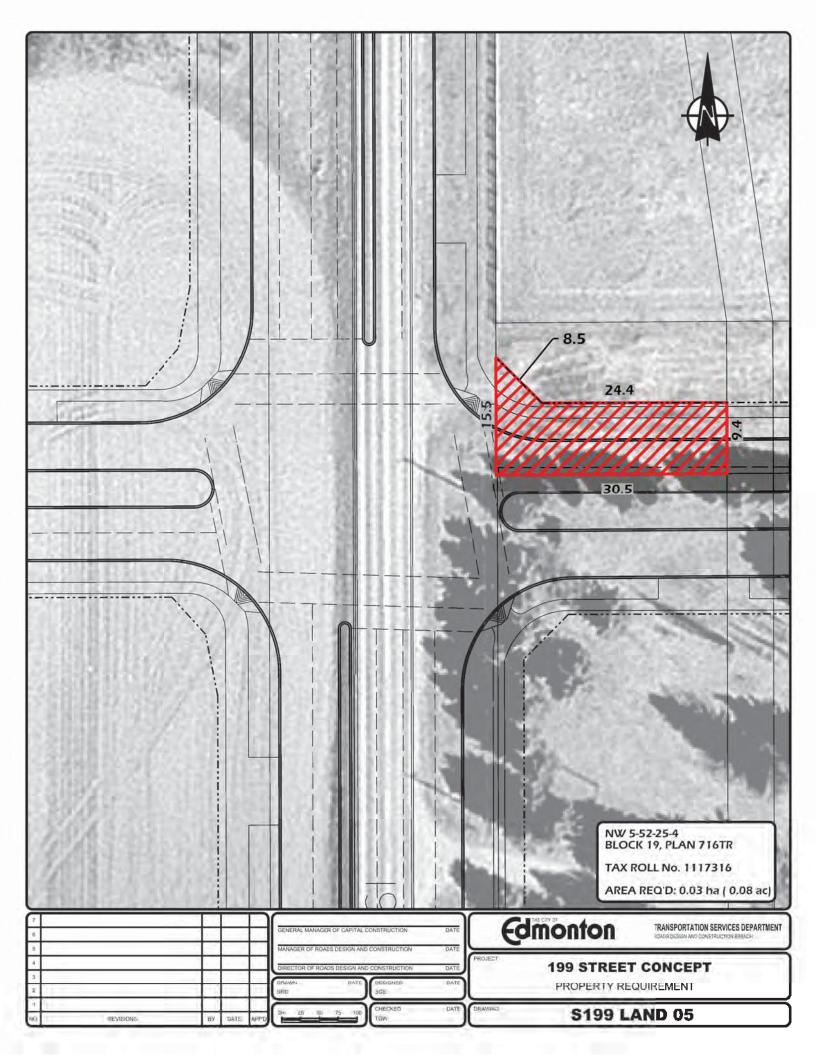
Right-of-Way Plans

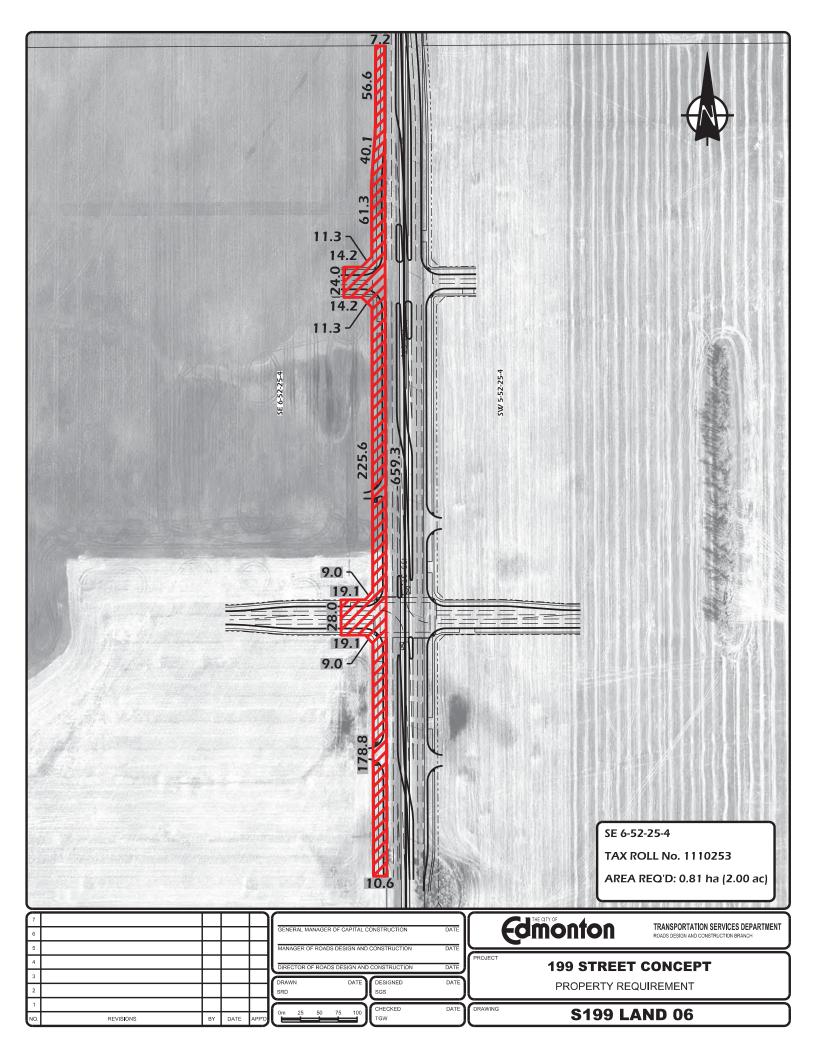


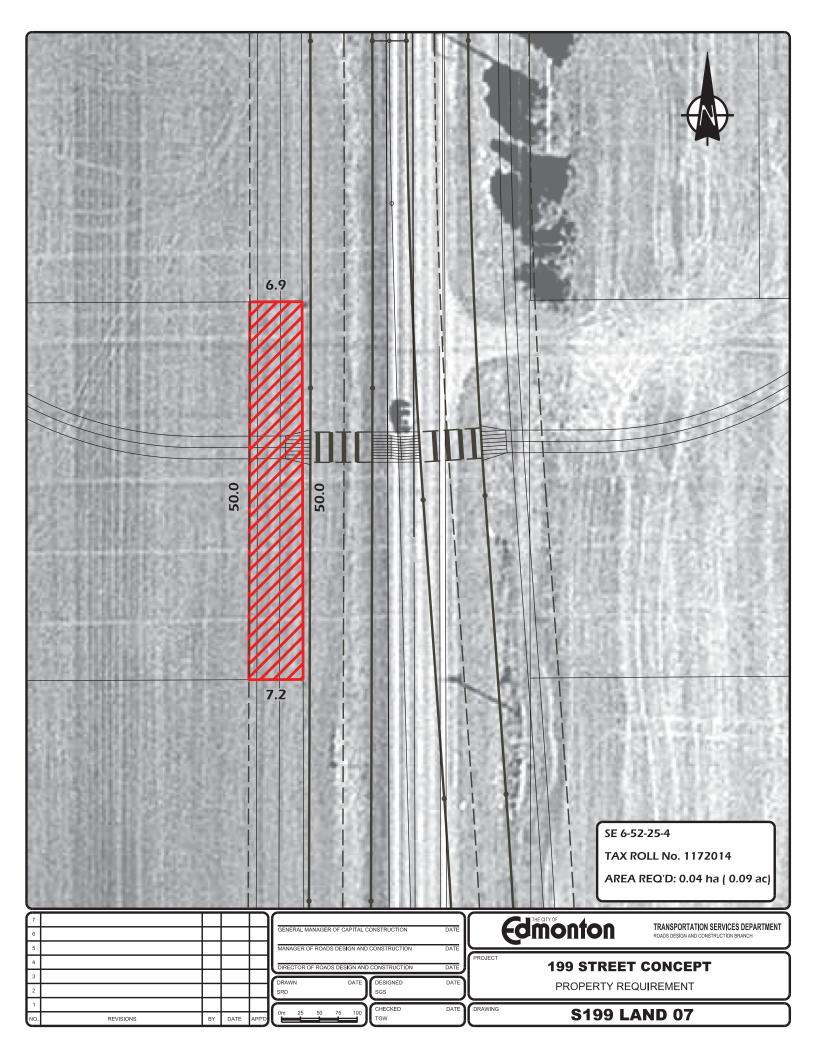


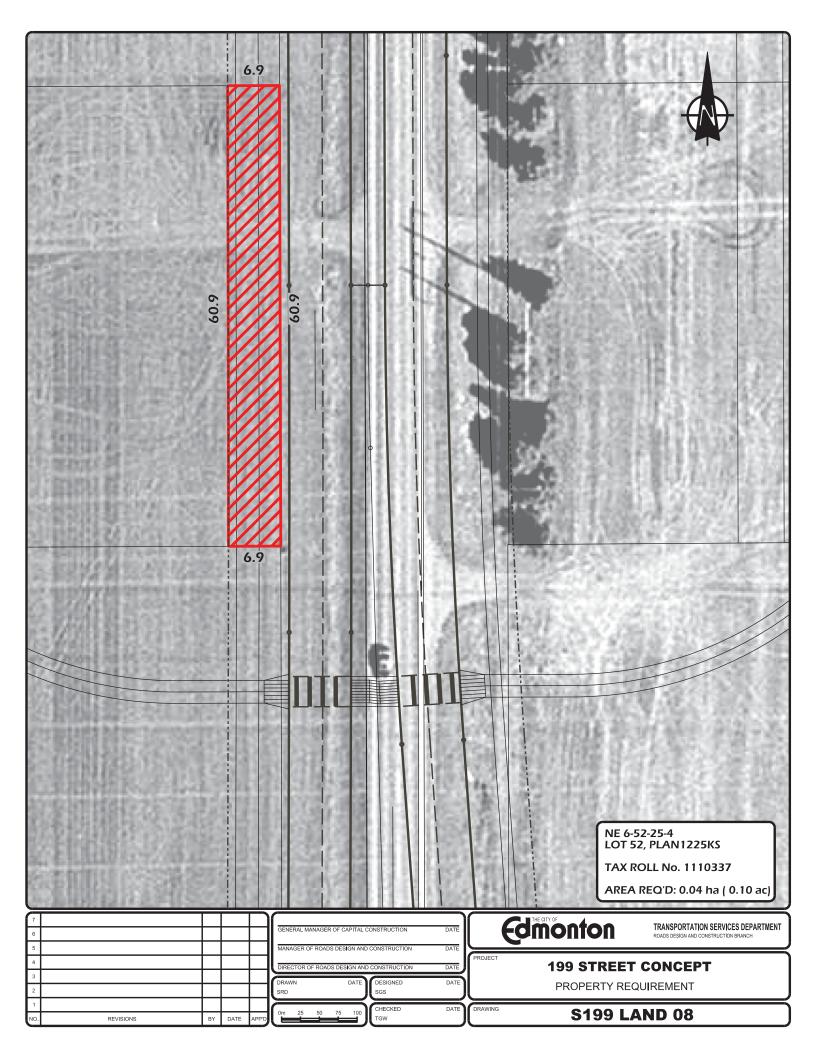
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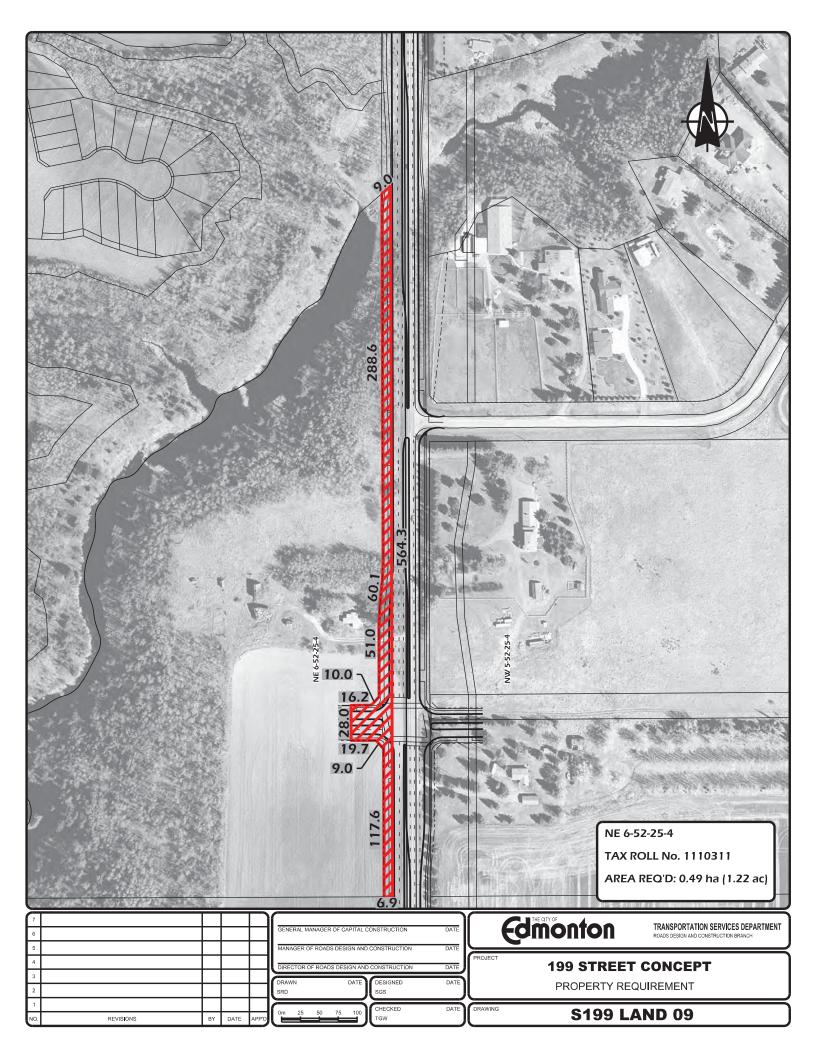


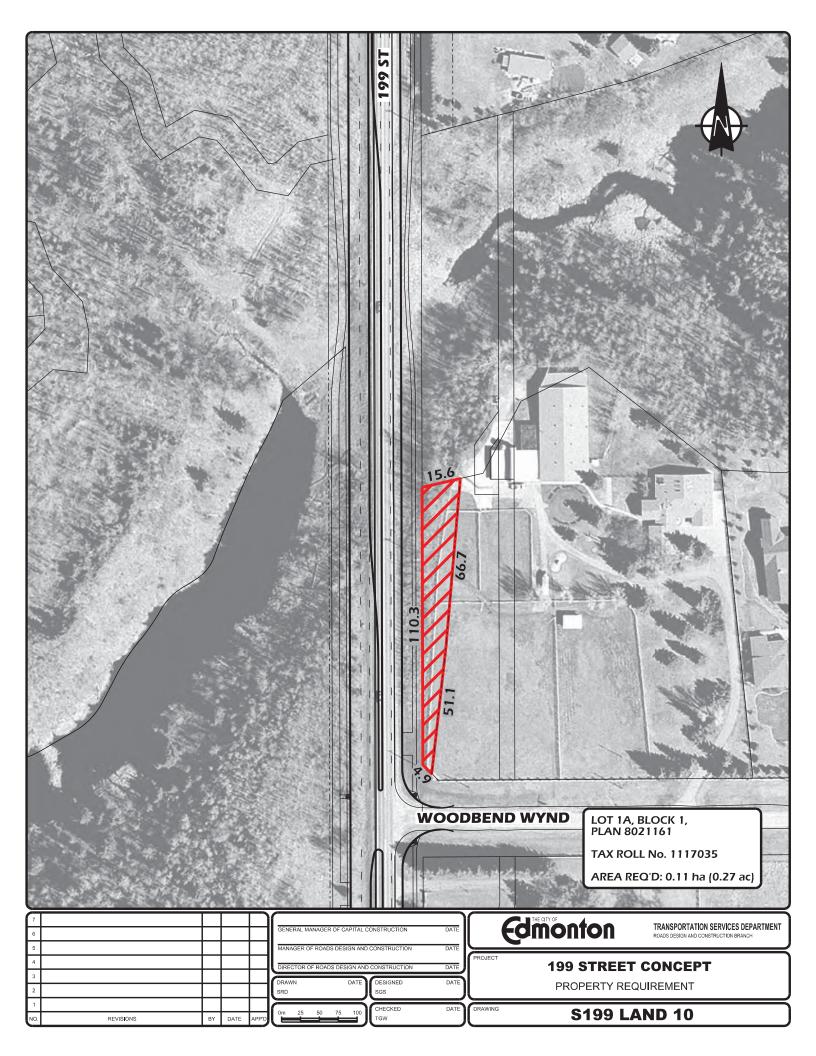


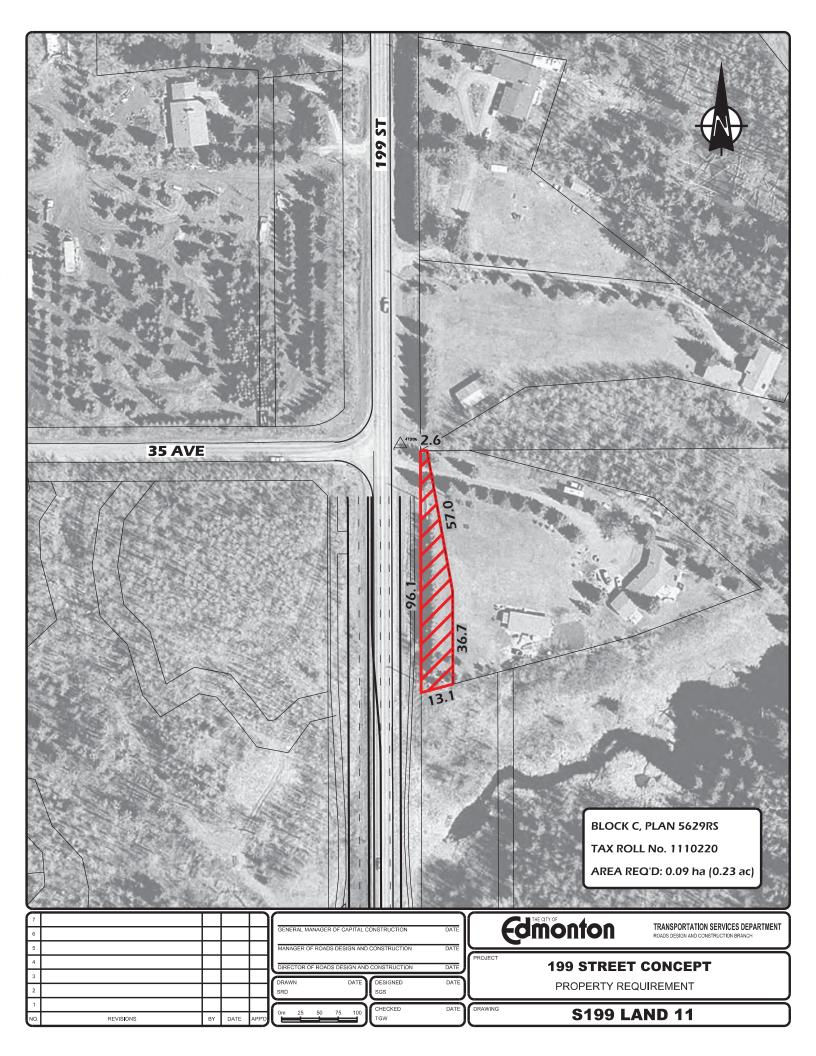










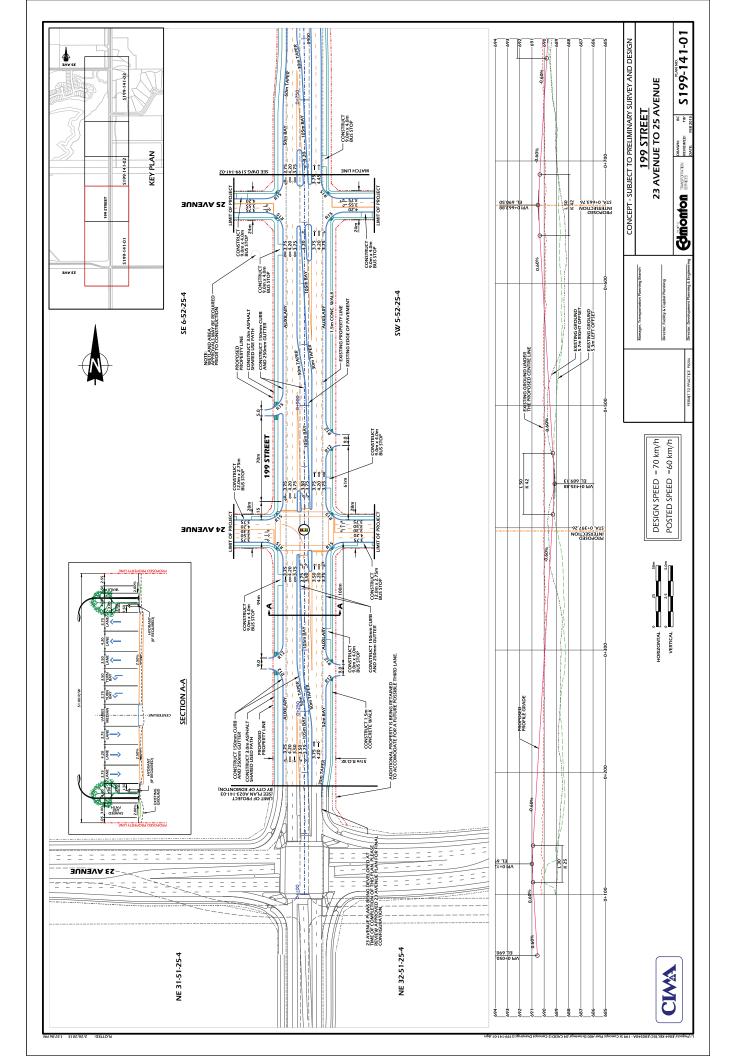


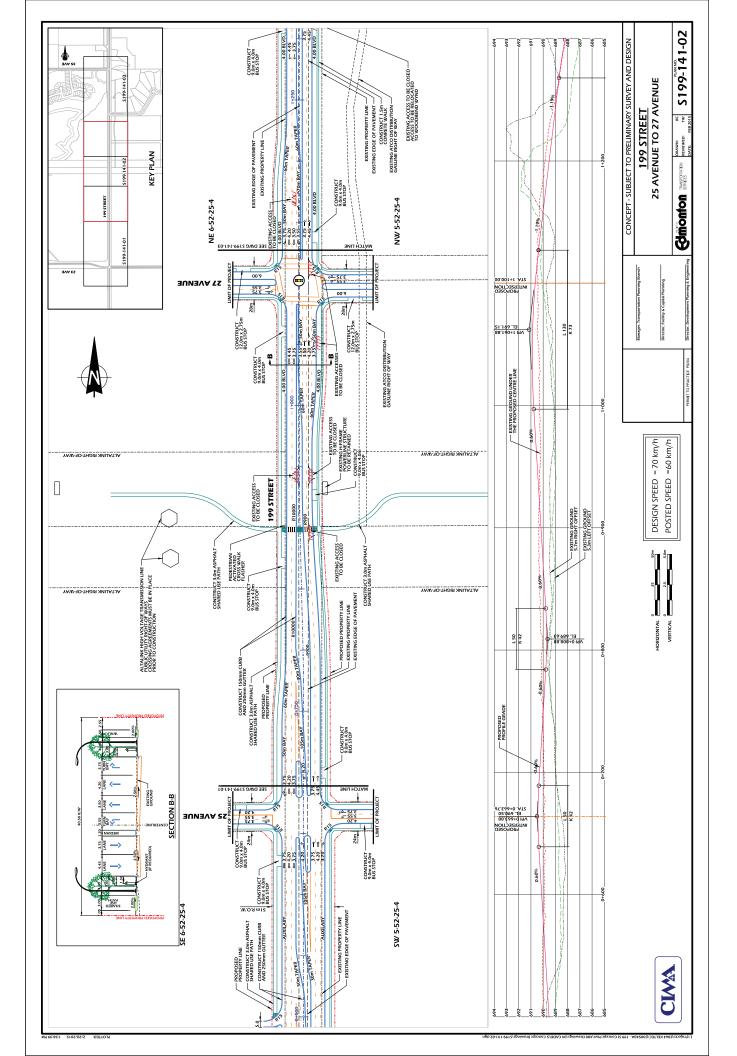
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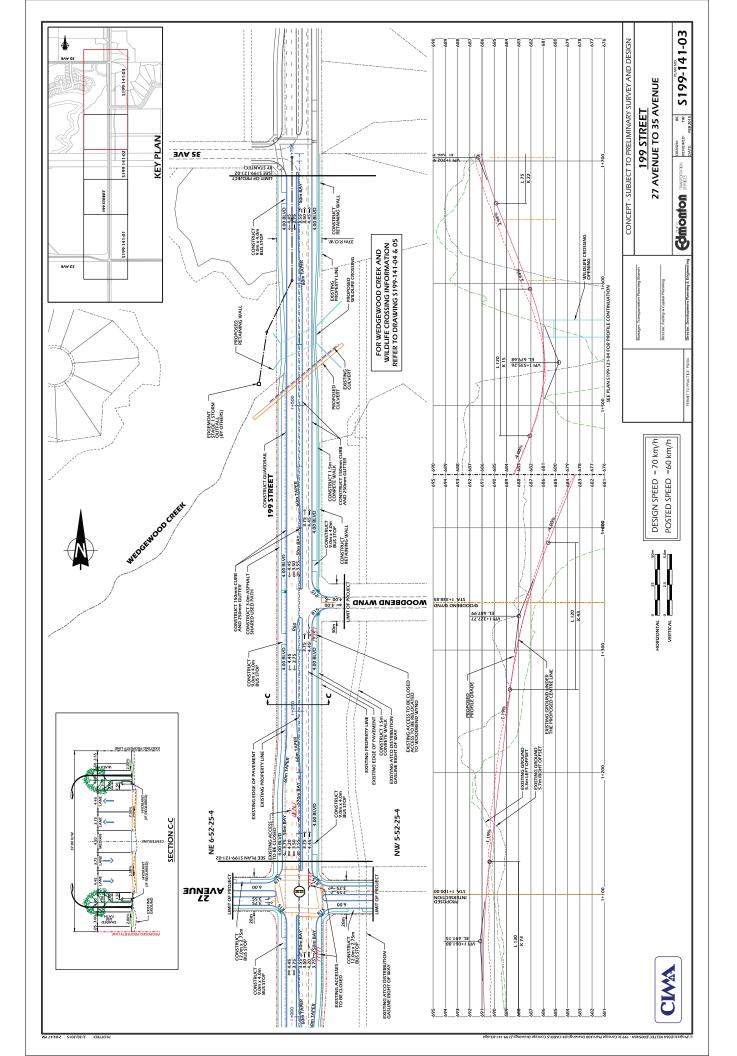
Wedgewood Creek Crossing: Retaining Wall Alternative

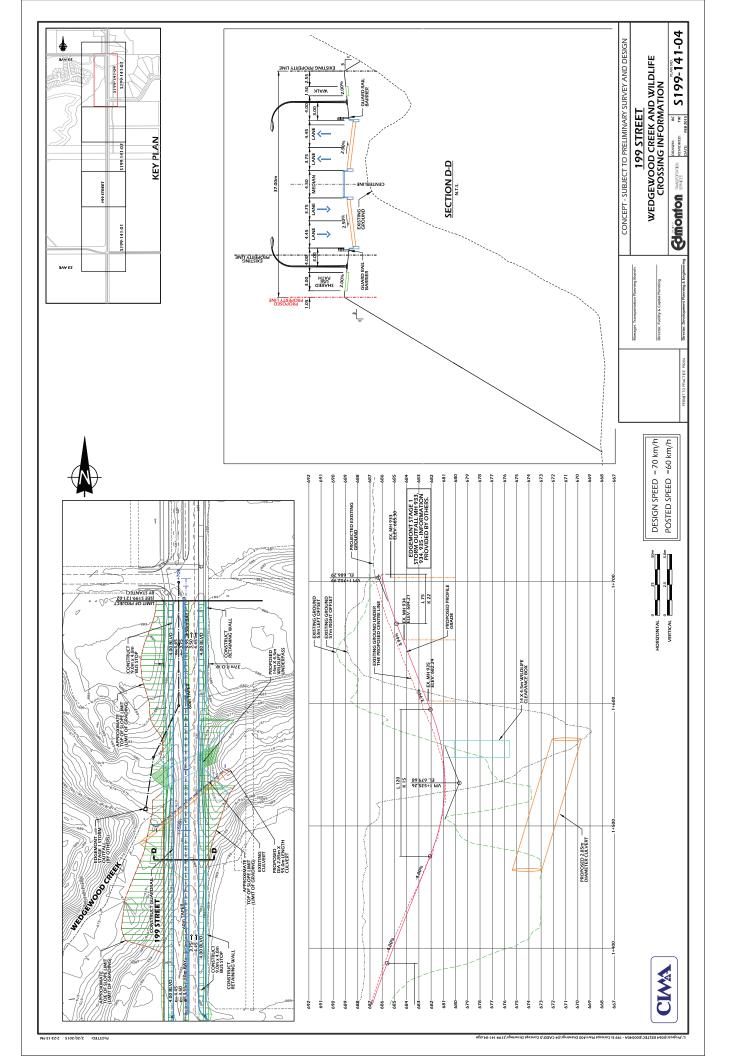


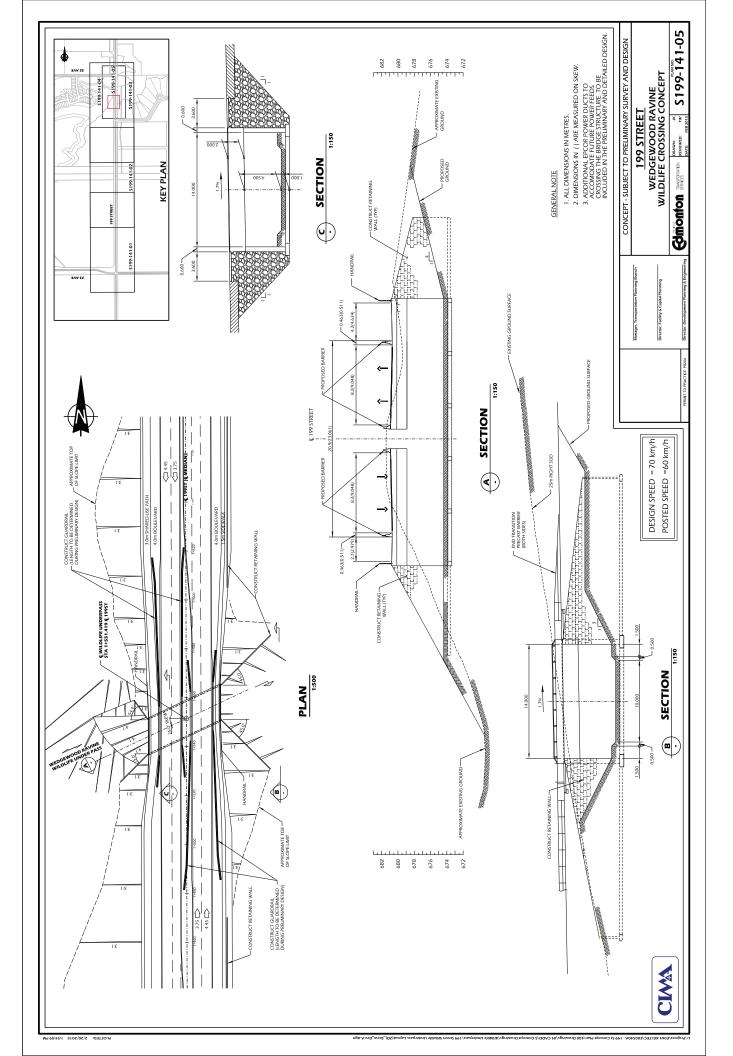
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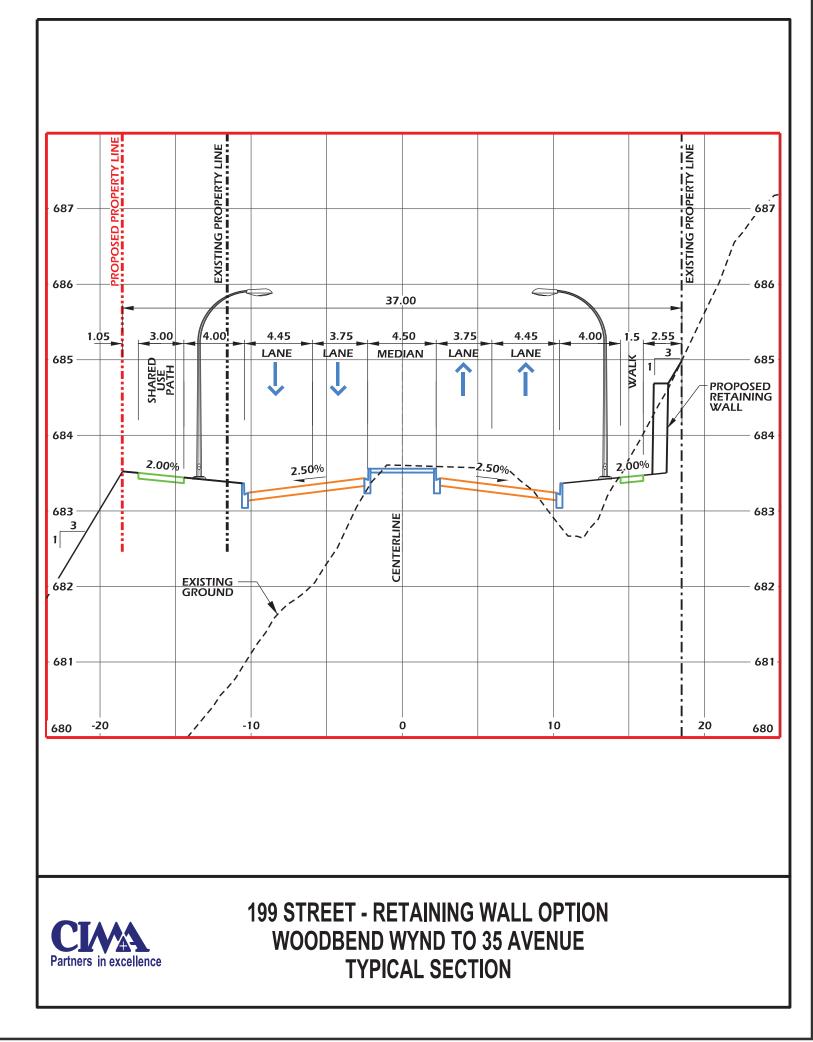












City of Edmonton 199 Street (23 Avenue to 35 Avenue) Concept Report – Final Submission | February 2015

APPENDIX P

Cost Estimate

||



Date: February 20, 2015 File: E00540A

Designed By: Ayden Smilski Checked By: Glen Campbell

Project: km to km = length (km) 199 Street Concept Plan (23 Avenue to 35 Avenue) 0.19 1.69 1.50

Item No.	Bid Item Description	Unit	Estimated Quantity	Estimated Unit Price	Estimated Cost
1	Straight Face Curb and Gutter	m	7,120	\$160.00	\$1,140,000.00
2	Shared Use Pathway (3.0 m width)	m	1,630	\$140.00	\$230,000.00
3	Concrete Sidewalk (1.5 m width)	m	1,630	\$120.00	\$200,000.00
4	Asphalt Concrete Pavement	m²	40,970	\$70.00	\$2,870,000.00
5	Granular Base Course	m²	43,820	\$35.00	\$1,540,000.00
6	Cement Stabilized Subgrade	m²	43,820	\$7.00	\$310,000.00
7	Street Lighting	Units	60	\$11,000.00	\$660,000.00
8	Traffic Signalization	Intersection	2	\$250,000.00	\$500,000.00
9	Pedestrian Crossing Signals	Units	1	\$80,000.00	\$80,000.00
10	Common Excavation	m ³	36,130	\$15.00	\$550,000.00
11	Borrow Excavation	m ³	43,360	\$25.00	\$1,090,000.00
12	Wildlife Underpass	Units	1	\$4,100,000.00	\$4,100,000.00
13	Culvert	Units	1	\$2,500,000.00	\$2,500,000.00
	-			Sub-Total:	\$15,770,000.00

Notes:

1. Wildlife underpass and culvert estimate based on conceputal bridge design report from Terrace Engineering.

2. Assumed street lights spaced every 60 m.

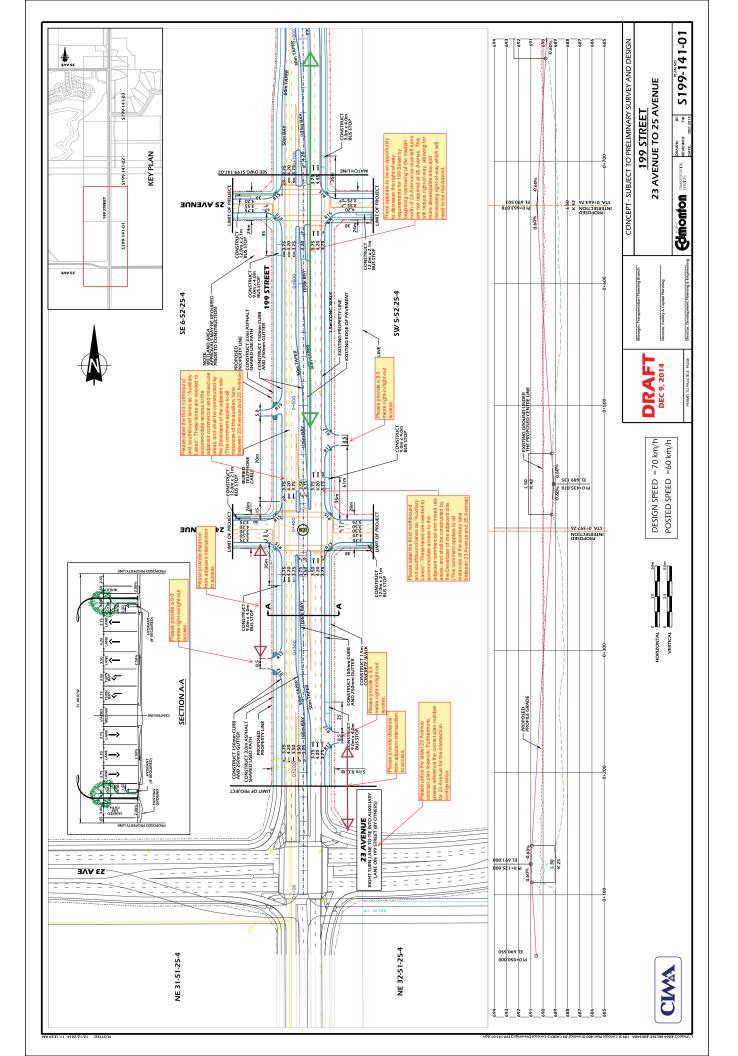
Estimated Constru	uction Cub Total	\$15,770,000.00
Estimated Constru	uction Sub-Total	\$15,770,000.00
Mobilization @	7%	\$1,103,900.00
Contingencies @	10%	\$1,687,390.00
	Engineering	\$0.00
	Utilities	\$0.00
	Right-of-Way	\$0.00
Total Estimat	ted Project Cost	\$18,561,290.00

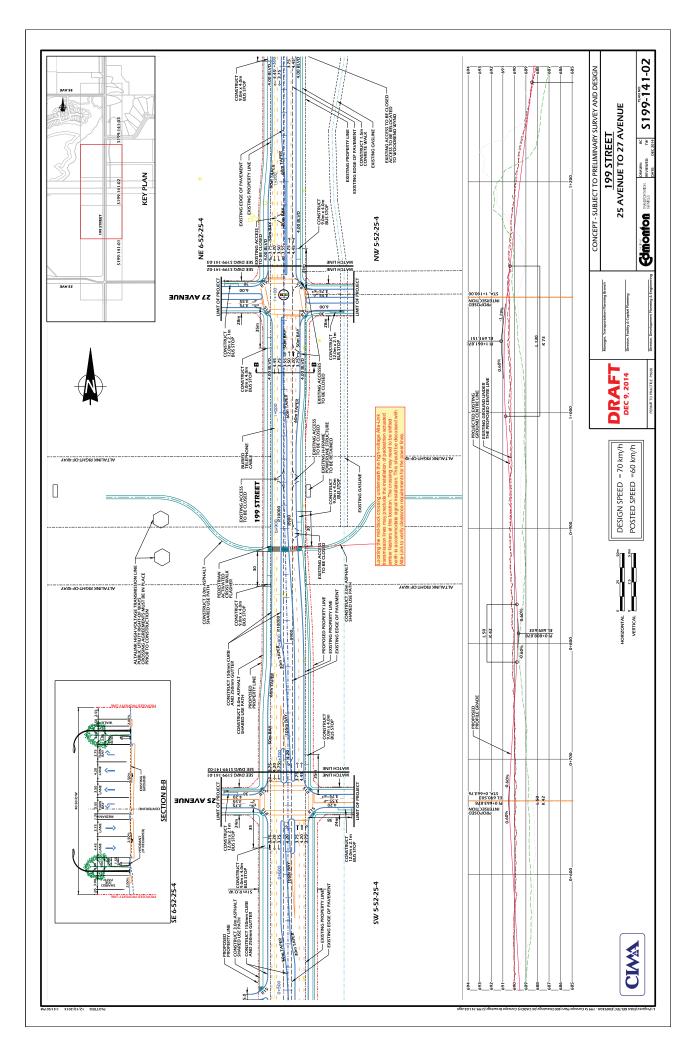


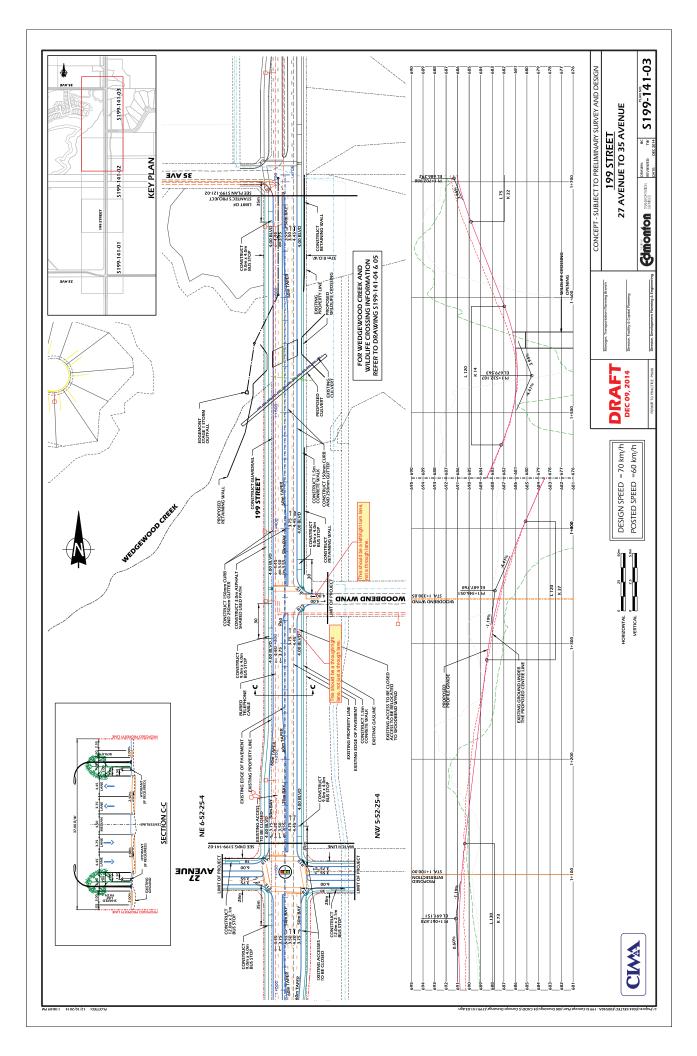
City of Edmonton Comments



Comment Number	Comment / Type of Comment	Facility and Capital Planning (FCP) Response
	General Remarks and Comments	
DP&E 1	The right-in/right-out accesses, as well as the right-in access along 199 Street north of 23 Avenue have not been reviewed or approved by Development Planning as part of a formal development application for the site. While the general location of the accesses is acceptable (subject to the comments below), the exact location and configuration of accesses will be determined at the subdivision and development permit stage.	Acknowledged. CIMA+ to note in report.
DP&E 2	Please ensure that the wildlife crossing requirements at the Wedgewood Creek crossing have been discussed with the Urban Ecology, and that they support the proposed design. Drawine 5-199-1401-01	Noted. Wildlife crossing treatment to be endorsed by OBD.
DP&E 3	As the 23 Avenue. Furthermore, the appropriate 23 Avenue As the 23 Avenue concept plans are nearing completion, the latest shadow plan should be utilized for 23 Avenue. Furthermore, the appropriate 23 Avenue plan number chould be referenced for the 23 Avenue/1000 Stream intersection.	Noted. CIMA+ to update drawing and FCP to confirm the right-turn cutoff treatment at 23 Avenue.
DP&E 4	promotion and a construction of the second	CIMA+ to wident access.
DP&E 5	The distances to the nearest adjacent intersections should be provided for the right-in/right-out accesses between 23 Avenue and 24 Avenue.	Acknowledged. CIMA+ to add dimension
DP&E 6	The TIA for Riverview identifies 199 Street as a four lane divided arterial roadway. The concept plans should clearly identify that the additional northbound and southbound lanes are "auxiliary lanes" that are required to facilitate access to the adjacent land uses, and do not represent a six lane divided arterial roadway. Furtheomore, as these are auxiliary lanes, the Developer of the adjacent connectial and miked use areas will be required to construct the auxiliary lanes.	Acknowledged. CIMA+ to update drawing, labelling auxillary lanes
DP&E 7	Given that single left turn lanes are adequate along 199 Street at 25 Avenue, consideration should be given to reducing the median along 199 Street north of 24 Avenue. This can reduce the right of-way trast needs to be maintained.	Noted. CIMA+ to provided justification for slotted left turns.
	Drawing S-199-1401-02	
DP&E 8	Locating the mid-block crossing underneath the high-voltage Alta-Link transmission lines may preclude the installation of pedestrian actuated amber flashers at this location. The crossing may need to be shifted north to accommodate signal installation. This should be discussed with Alta-Link to verify clearance requirements for the power lines.	Noted. CIMA+ review comments in more detail. Please discuss with Altalink and move trail to not be under the power lines.
	Drawing S-199-1401-03	
DP&E 9	The southbound left turn bay at 27 Avenue is non-standard and exceeds the requirements outlined in the TA. Given the possibility of higher than expected left Noted. Turn bay shown is ok, turn volumes at this location, Development Planning supports the construction of a longer left turn bay at this location.	Voted. Turn bay shown is ok.
DP&E 10	The northbound curb lane along 199 Street at Woodbend Wynd should be identified as a through right lane, not a through only lane.	Acknowleged. CIMA+ to update drawings
DP&E 11	The westbound lane along Woodbend Wynd should be identified as a left/right turn lane, not a through lane.	Acknowleged. CIMA+ to update drawings
	Drawing S-1401-04 and S199-1401-05	
DP&E 12	Please ensure that the wildlife crossings have been reviewed with the Office of Biodiversity.	Wildlife passage to be endorsed by OBD.
DP&E 13	Please note that FPCOR has expressed an interest in including power ducts in the Wedgewood Creak crossing bridge structure to accommodate future power feeds. Please ensure that additional duct work is included in the preliminary and detailed design of the structure to accommodate future ECOR installation. Please contact and coordinate with Jatinder Hayer of Great Northern Engineering Consultants Inc. (Direct: 780-490-7141, Cell: 780-920-4680 Email: haver@enec.ca).	Noted. CIMA+ to note this in the report.
ansportation O	Transportation Operations Comments and Responses	
T-Ops 1	Typically, marked and signed pedestrian crosswalks are considered for installation after a pedestrian and vehicle assessment has been completed to determine if it meets the criteria for the installation of a marked crosswalk except at intersections that are controlled by an all-way stop or a traffic signal. Please remove the marked crosswalk at the intersections of 199 St and 25 Ave, Woodbend Wyhd, and 35 Ave and and stop determine if would are going to be controlled by an all-way stop or a traffic signal. Please remove the marked crosswalks at the intersections of 199 St and 25 Ave, Woodbend Wyhd, and 35 Ave are going to be controlled by an all-way stop or a traffic signal. We stop or a traffic signal.	Noted. Please remove crosswalks. Note a crosswalk warrant may be completed at a later date.
T-Ops 2	Is there a reason to have a wide centre lane (4.2m wide) for the segment 99 St between 23 and 25 Ave.	Noted. Outside lanes are auxillary lanes. No action required.
ustainable Tran	<u>Sustainable Transportation Comments and Responses</u>	
ST 1	For all bus stop pads: if the pad is less than 1m from sidewalk, pour the concrete pad to the sidewalk otherwise provide a 3m walk connection at the head of the pad (as per standard drawing 4110)	Noted. CIMA+ to review all collector road stops and revise if required.
ST 2	insure adequate clear width of sidewalk from retaining wall (min 0.6m)	CIMA+ to review and increase distance if required.
ST 3	Classify in Draction Diametric and successing and successin	









Christopher Wintle <christopher.wintle@edmonton.ca>

Re: 199 St Submission 2 Developer Concept Plan

1 message

Ken Karunaratne <ken.karunaratne@edmonton.ca> To: Christopher Wintle <christopher.wintle@edmonton.ca> Fri, Jan 16, 2015 at 8:28 AM

Hi Chris,

The following are transportation Operations comments.

1. Typically, marked and signed pedestrian crosswalks are considered for installation after a pedestrian and vehicle assessment has been completed to determine if it meets the criteria for the installation of a marked crosswalk except at intersections that are controlled by an all-way stop or a traffic signal. Please remove the marked crosswalks at the intersections of 199 St and 25 Ave, Woodbend Wynd, and 35 Ave unless they are going to be controlled by an all-way stop or a traffic signal. Even though a marked crosswalk is not installed, curb ramp construction can still proceed.

2. Is there a reason to have a wide centre lane (4.2m wide) for the segment 99 St between 23 and 25 Ave.

Sorry for the delay in providing our comments.

Ken

Ken Karunaratne M.Eng., P.Eng, PTOE Senior Traffic Engineer Transportation Operations City of Edmonton 15th Floor, Century Place 9803 - 102A Avenue NW Edmonton Alberta T5J 3A3 Phone: 780-442-6435

On Wed, Jan 7, 2015 at 2:54 PM, Christopher Wintle <<u>christopher.wintle@edmonton.ca</u>> wrote: | Hi Craig,

Some time ago we circulated the first submission of a concept plan, being completed by CIMA+ on behalf of Walton, for 199 Street from 23 Avenue to 35 Avenue. We did not receive comments and due to unsatisfactory quality of the plans on the first submission did not follow up with and instead asked for submission 2.

We have received Submission 2, and I am requesting that T-ops review and provide comments to Submission 2 as soon as possible. We would usually request two weeks, but given the stage of the study we are at I hoping to get comments to the consultant next week, so if it is possible to provide comments within a week

City of Edmonton Mail - Re: 199 St Submission 2 Developer Concept Plan

(by Wednesday January 14) that would be much appreciated.

The plans are attached via Google Drive.

199 Street Submission 2

Thanks,

Christopher

Christopher Wintle, P.Eng. Project Engineer, Facility and Capital Planning City of Edmonton, Transportation Services Ph. 780-496-1792 christopher.wintle@edmonton.ca



MEMORANDUM

January 13, 2015

Your Reference: 199 St - 23 Ave to 35 Ave

SUBJECT:	Concept Plan for 199 Street, from 23 Avenue to 35 Avenue (Second Draft Submission)
FROM:	Jack Niepsuj, P. Eng Development Planning Transportation Planning Branch
TO:	Christopher Wintle, P. Eng Facility and Capital Planning Transportation Planning Branch

Development Planning has reviewed the above drawings and has the following comments. These comments are also provided on the attached concept plans.

General Remarks:

- The right-in/right-out accesses, as well as the right-in access along 199 Street north of 23 Avenue have not been reviewed or approved by Development Planning as part of a formal development application for the site. While the general location of the accesses is acceptable (subject to the comments below), the exact location and configuration of accesses will be determined at the subdivision and development permit stage.
- Please ensure that the wildlife crossing requirements at the Wedgewood Creek crossing have been discussed with the Urban Ecology, and that they support the proposed design.

Drawing No. S199-1401-01:

- As the 23 Avenue concept plans are nearing completion, the latest shadow plan should be utilized for 23 Avenue. Furthermore, the appropriate 23 Avenue plan number should be referenced for the 23 Avenue/199 Street intersection.
- The right-in/right-out accesses should be 9.0 metres to facilitate access by medium sized delivery vehicles, as is commonly done for commercial developments.
- The distances to the nearest adjacent intersections should be provided for the right-in/right-out accesses between 23 Avenue and 24 Avenue.
- The TIA for Riverview identifies 199 Street as a four lane divided arterial roadway. The concept plans should clearly identify that the additional northbound and southbound lanes are "auxiliary lanes" that are required to facilitate access to the adjacent land uses, and do not represent a six lane divided arterial roadway. Furthermore, as these are auxiliary lanes, the Developer of the adjacent commercial and mixed use areas will be required to construct the auxiliary lanes.
- Given that single left turn lanes are adequate along 199 Street at 25 Avenue, consideration should be given to reducing the median along 199 Street north of 24 Avenue. This can reduce the right-of-way required for 199 Street, as well as the amount of road right-of-way that needs to be maintained.

Drawing No. S199-1401-02:

• Locating the mid-block crossing underneath the high-voltage Alta-Link transmission lines may preclude the installation of pedestrian actuated amber flashers at this location. The crossing may need to be shifted north to accommodate signal installation. This should be discussed with Alta-Link to verify clearance requirements for the power lines.

Drawing No. S199-1401-03:

- The southbound left turn bay at 27 Avenue is non-standard and exceeds the requirements outlined in the TIA. Given the possibility of higher than expected left turn volumes at this location, Development Planning supports the construction of a longer left turn bay at this location.
- The northbound curb lane along 199 Street at Woodbend Wynd should be identified as a through right lane, not a through only lane.
- The westbound lane along Woodbend Wynd should be identified as a left/right turn lane, not a through lane.

Drawing No. S199-1401-04 and S199-1401-05:

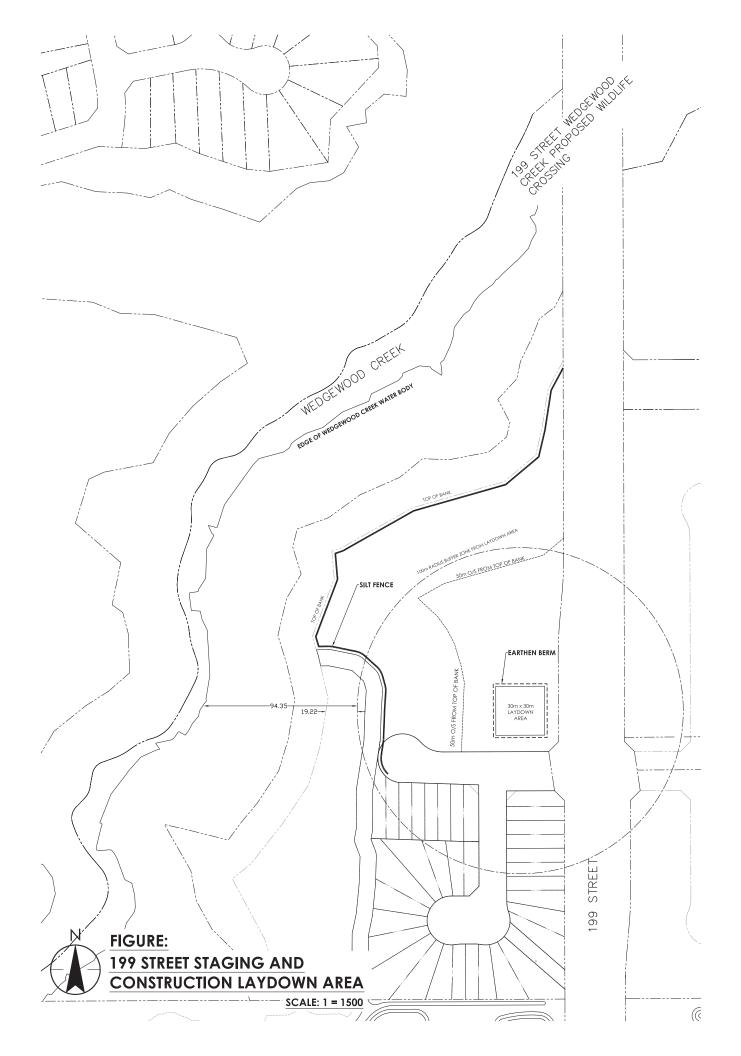
- Please ensure that the wildlife crossings have been reviewed with the Office of Biodiversity.
- Please note that EPCOR has expressed an interest in including power ducts in the Wedgewood Creek crossing bridge structure to accommodate future power feeds. Please ensure that additional duct work is included in the preliminary and detailed design of the structure to accommodate future EPCOR installation. Please contact and coordinate with Jatinder Hayer of Great Northern Engineering Consultants Inc. (Direct: 780-490-7141, Cell: 780-920-4680 Email: hayer@gnec.ca).

Should you require any additional information please contact Jack Niepsuj at 780-496-4127.

JN

Attachment – 199 Street Concept Plan Comments

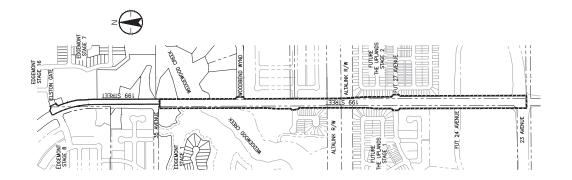
APPENDIX C PROJECT SPECIFIC DETAILS





RIVERVIEW LAND COMPANY LTD.

199 STREET 23 AVENUE TO 35 AVENUE JUNE 2016 PROJECT NUMBER: 1161-103725



SUBDIVISION FILE: LDA/14-0566 SUBDIVISION FILE: LDA/14-0567

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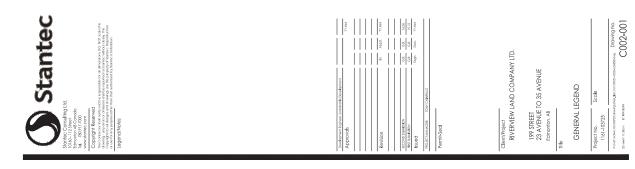
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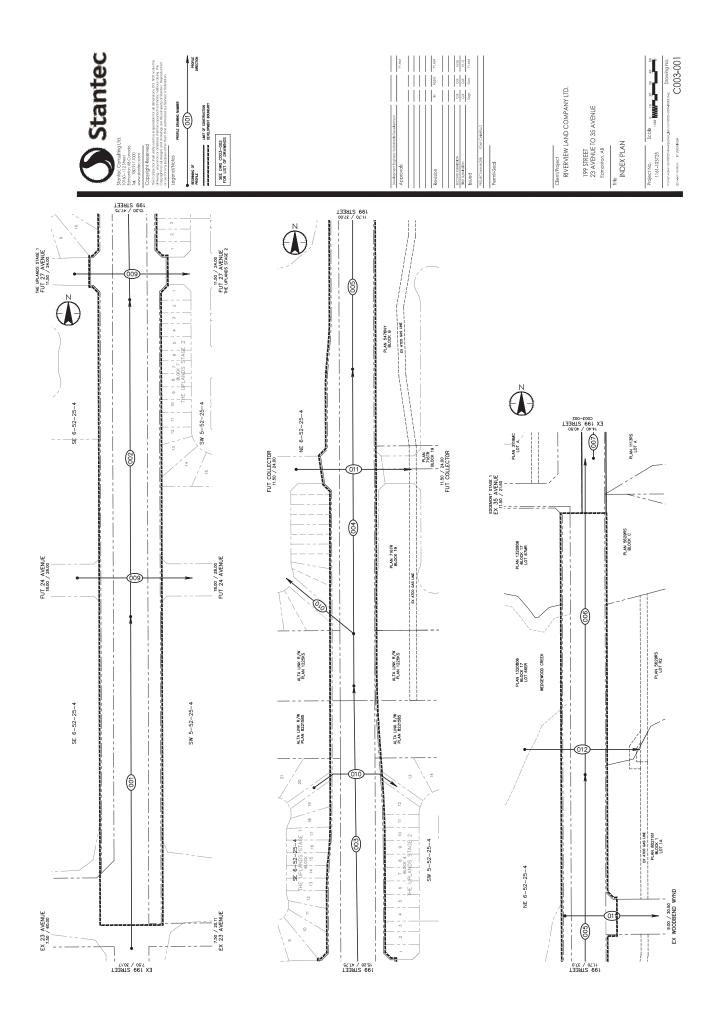
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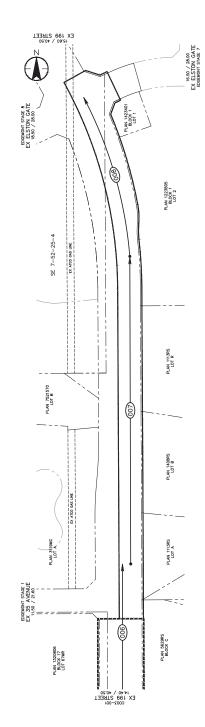
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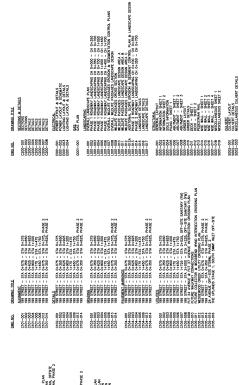
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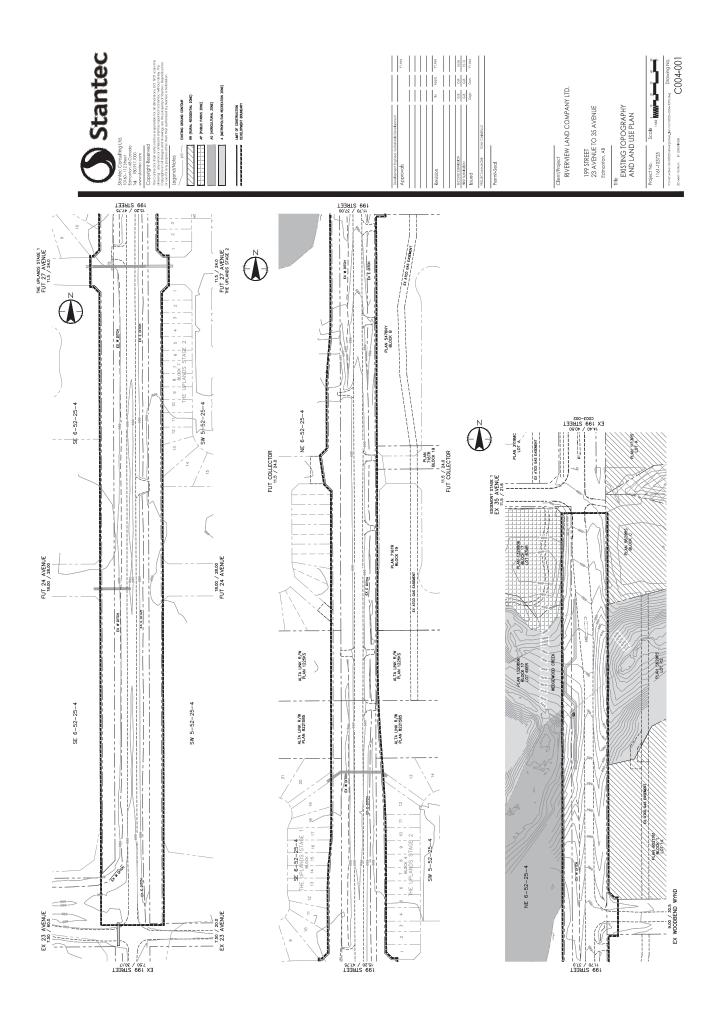


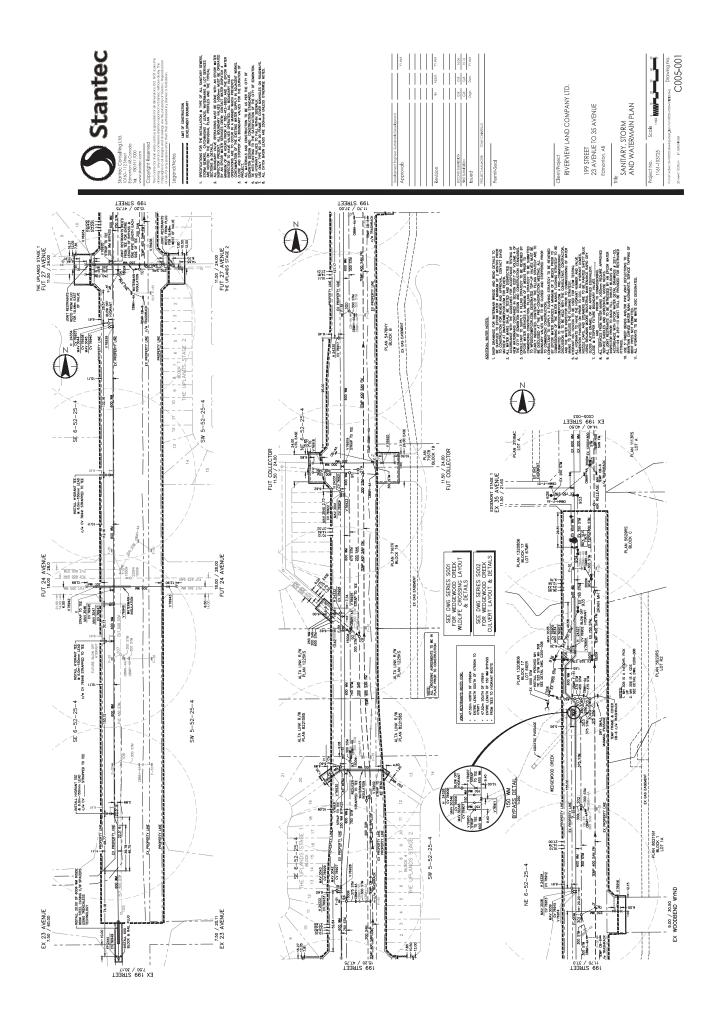


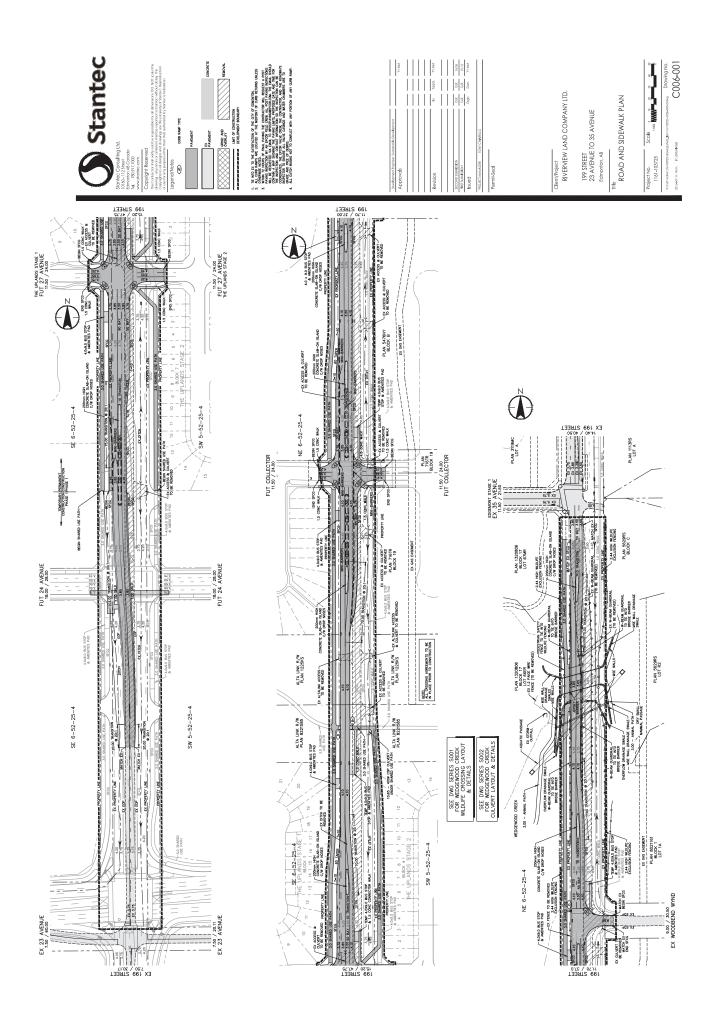


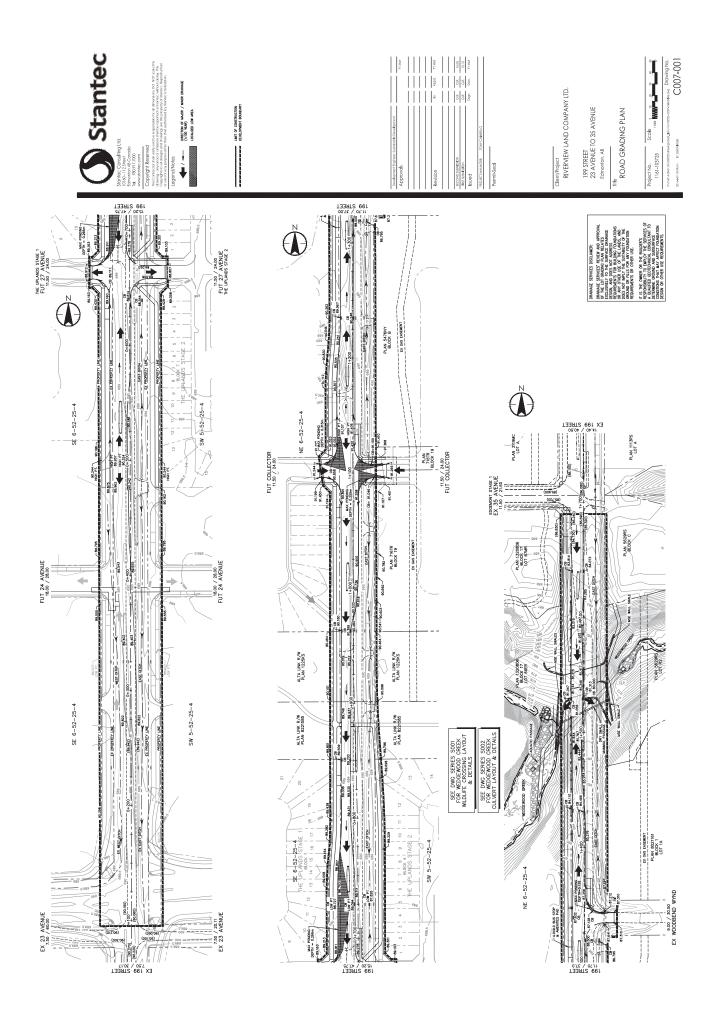


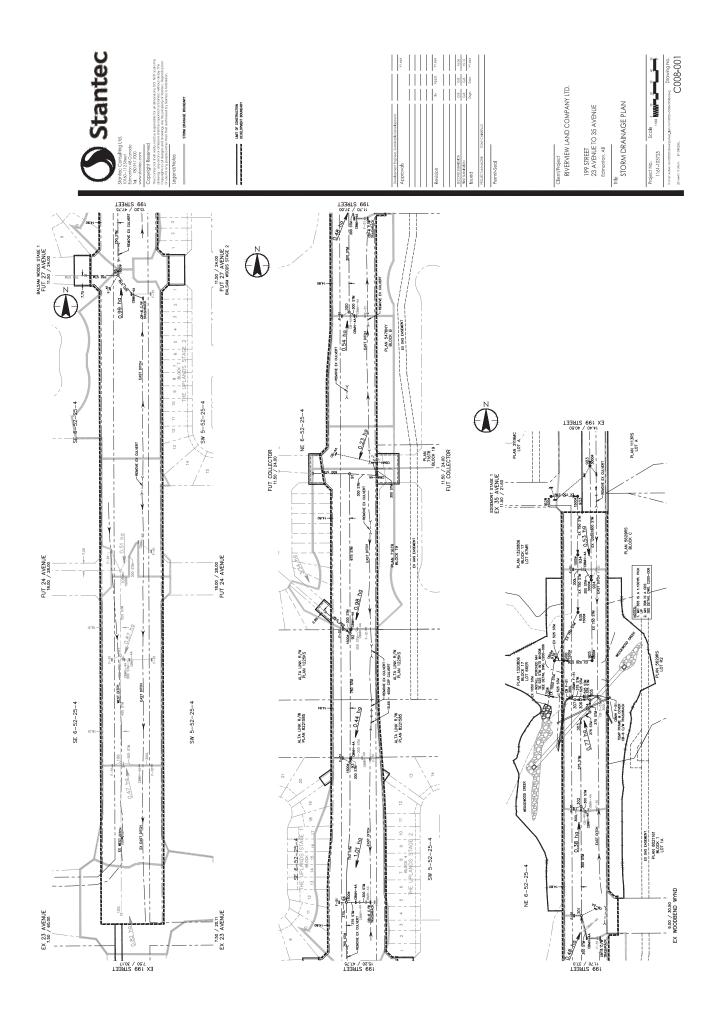
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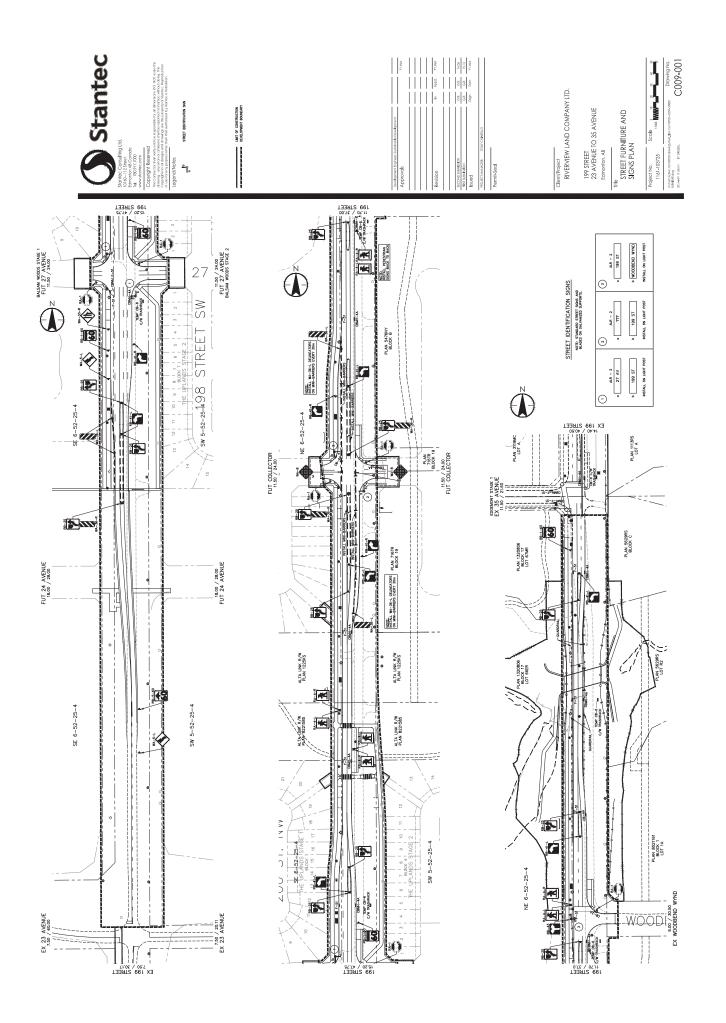


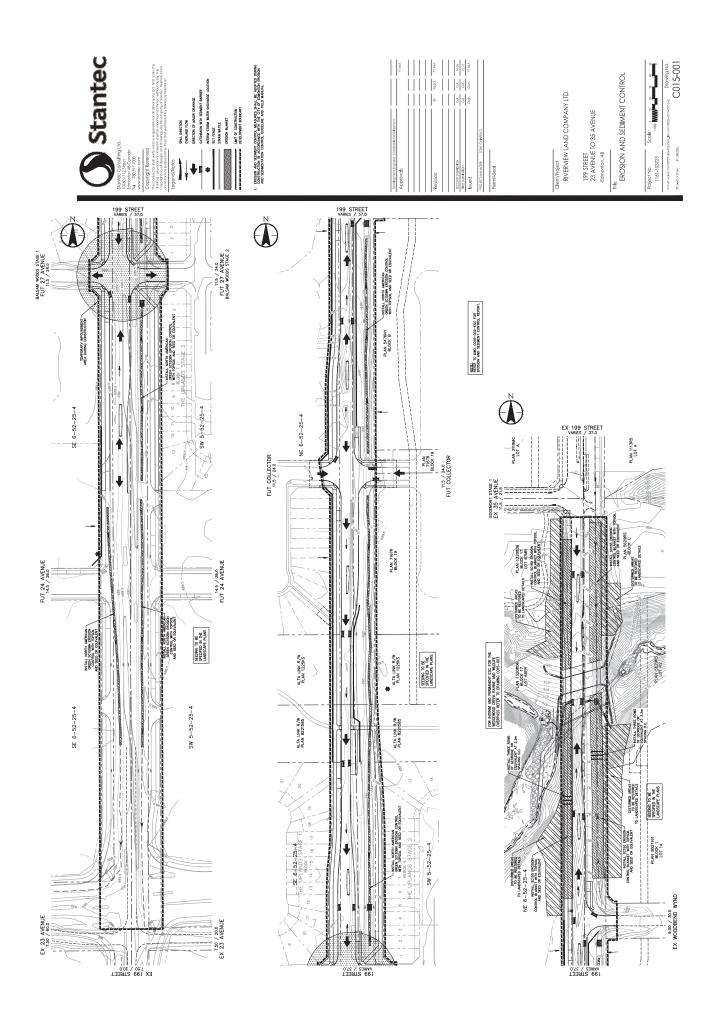


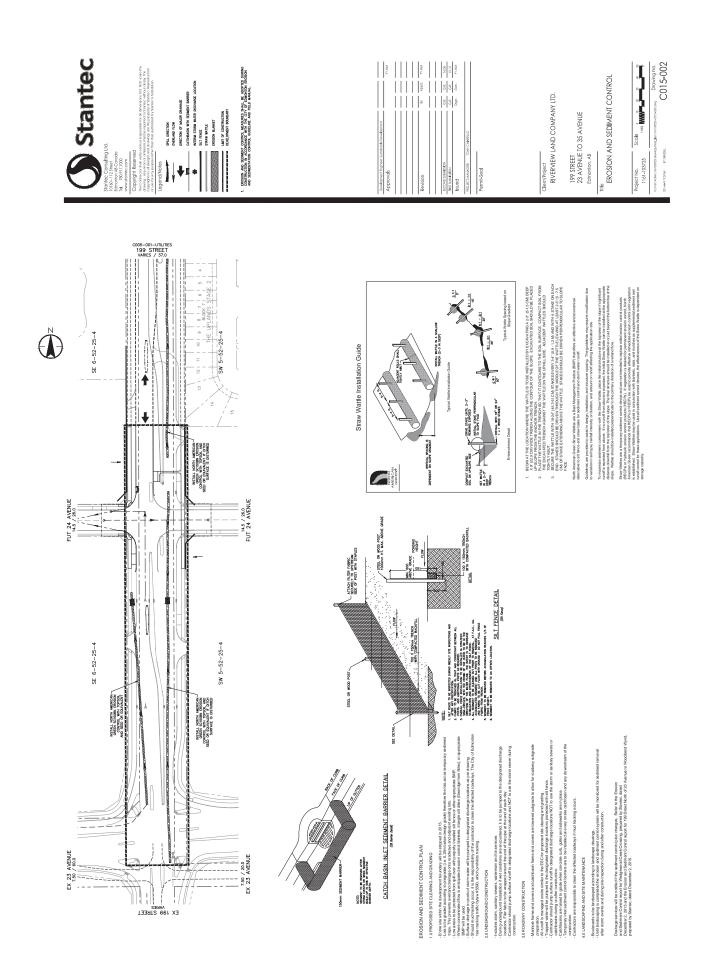


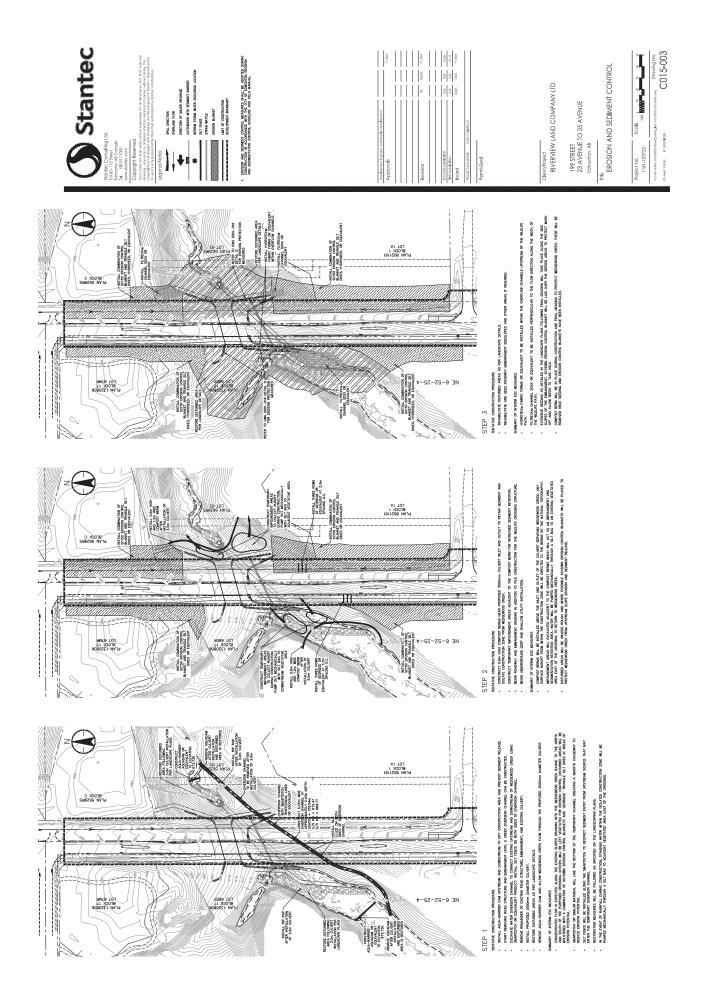


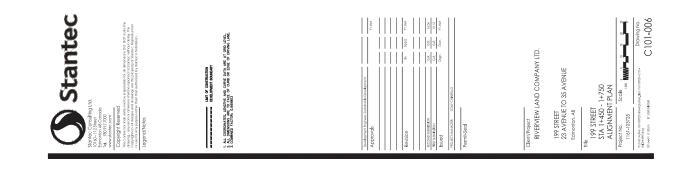


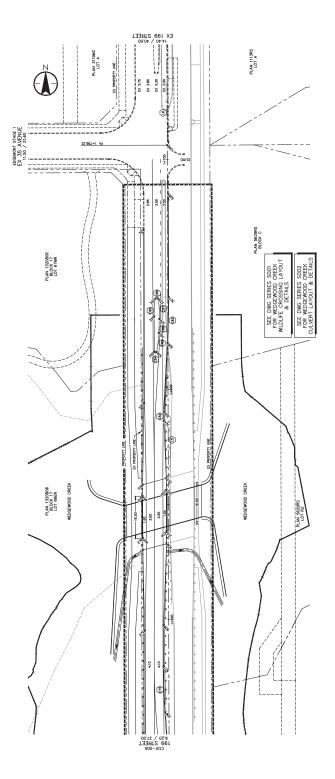




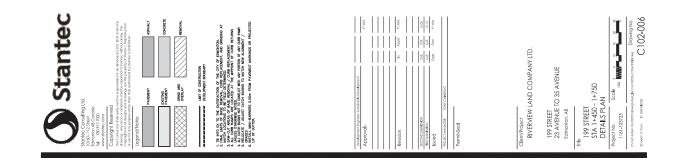


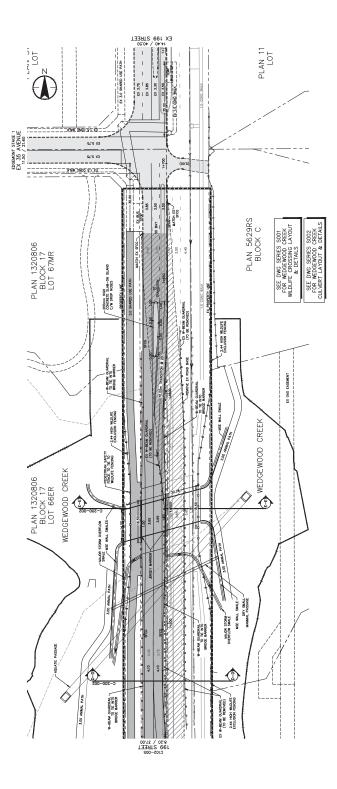


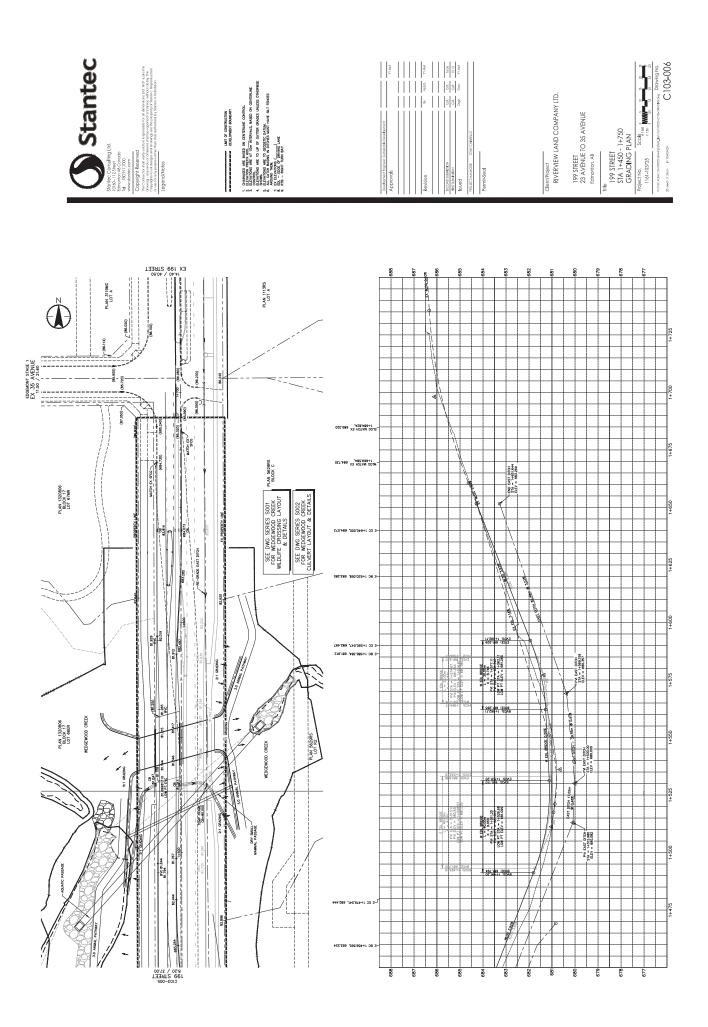


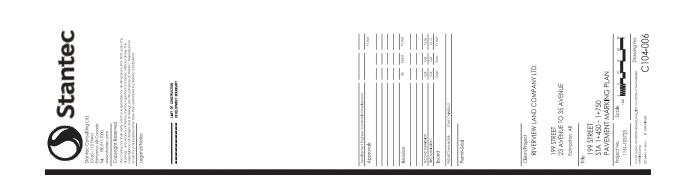


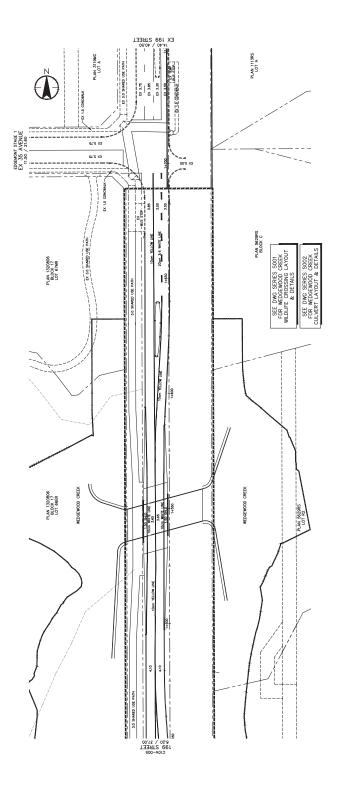
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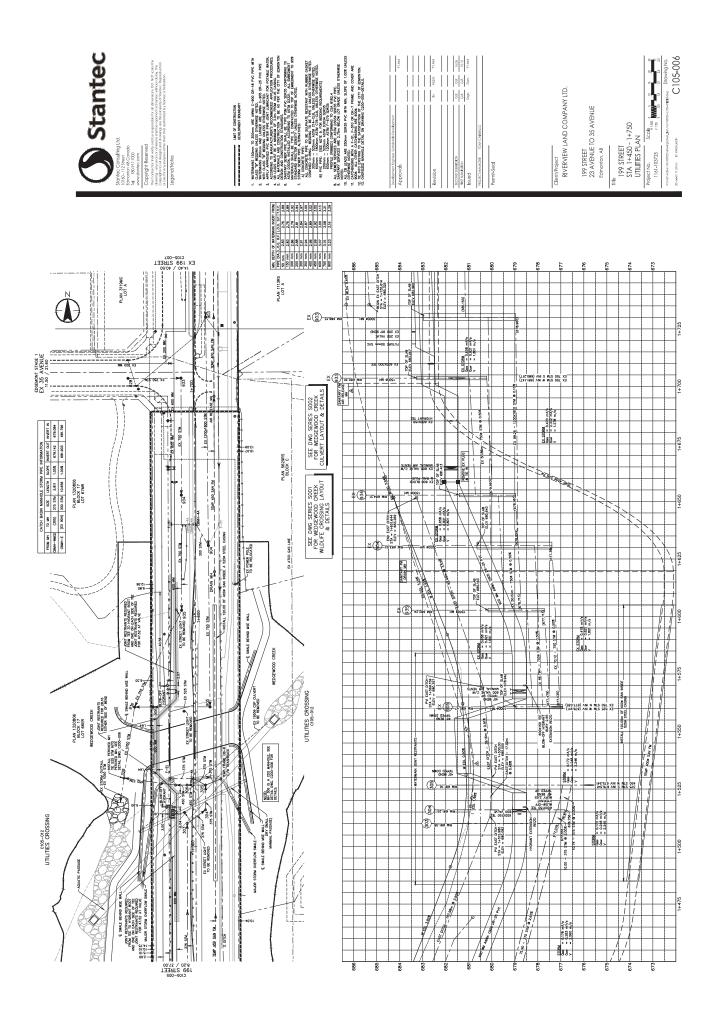


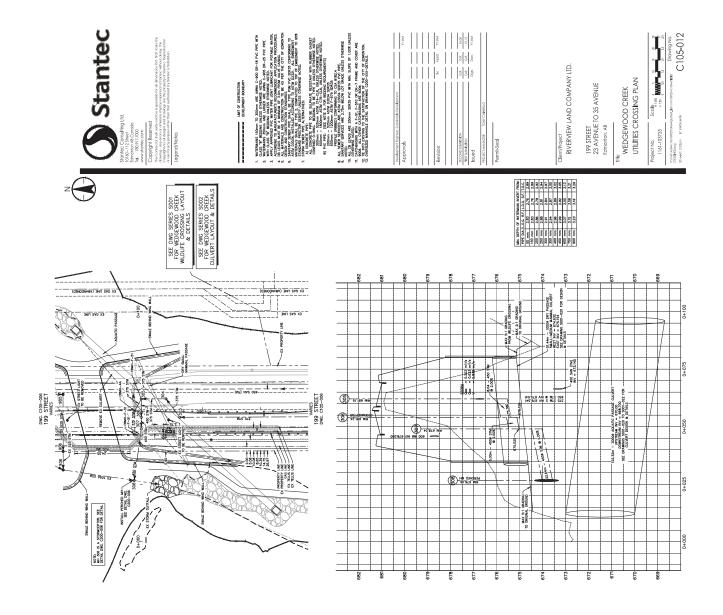


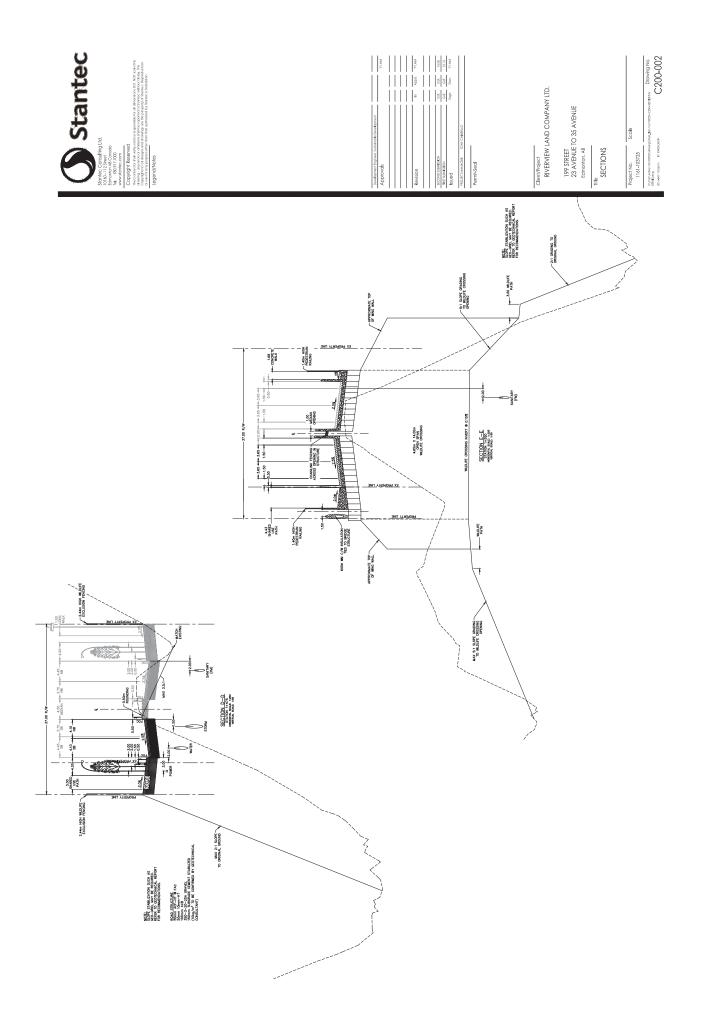


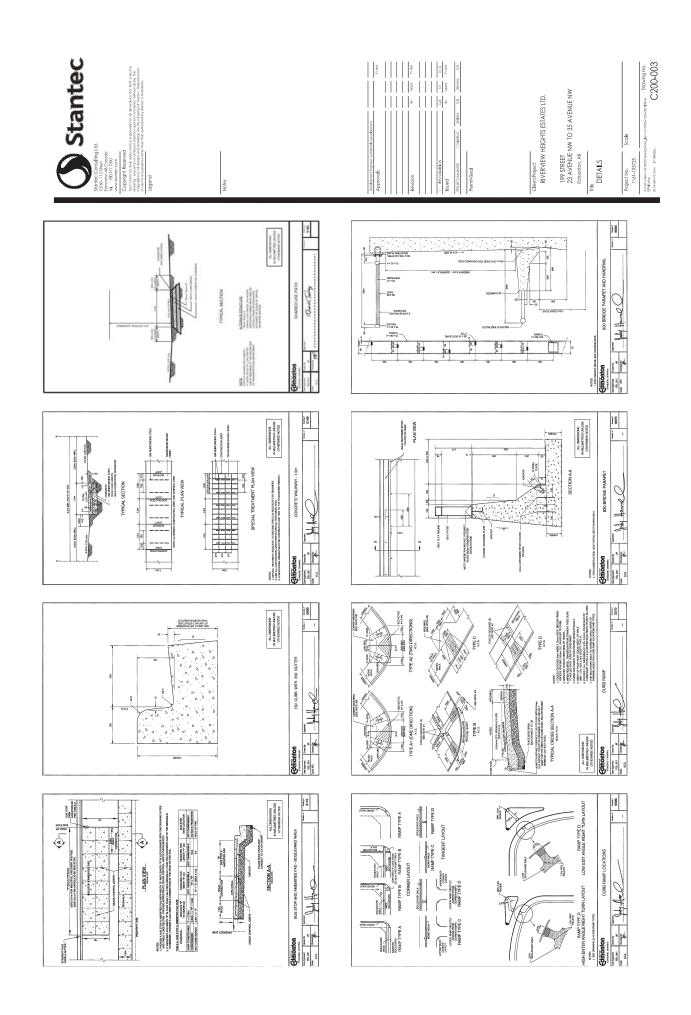




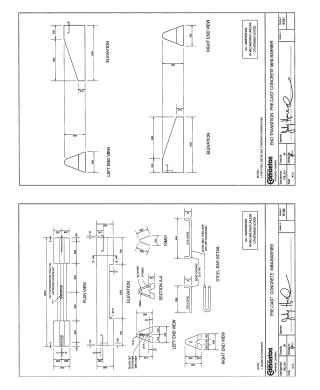


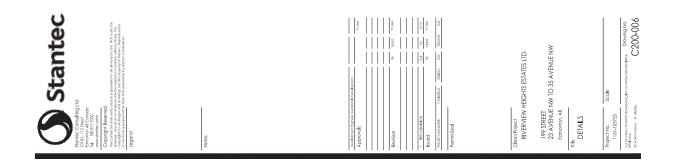


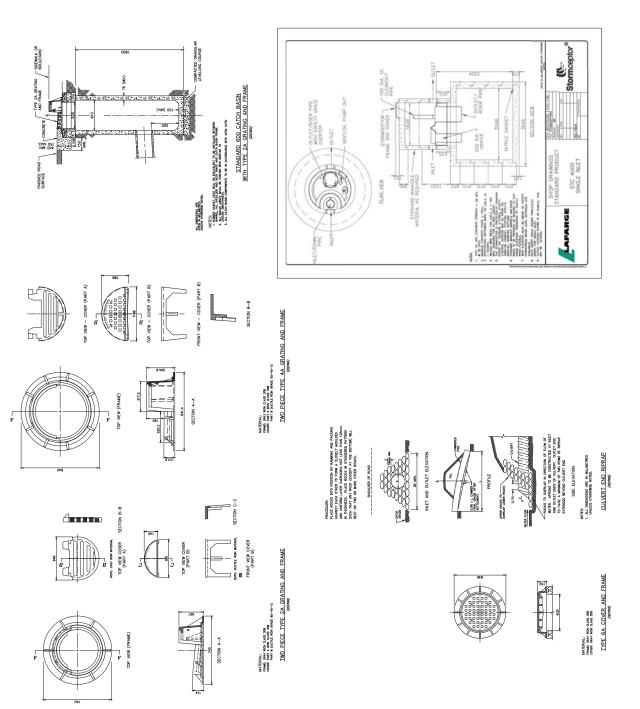


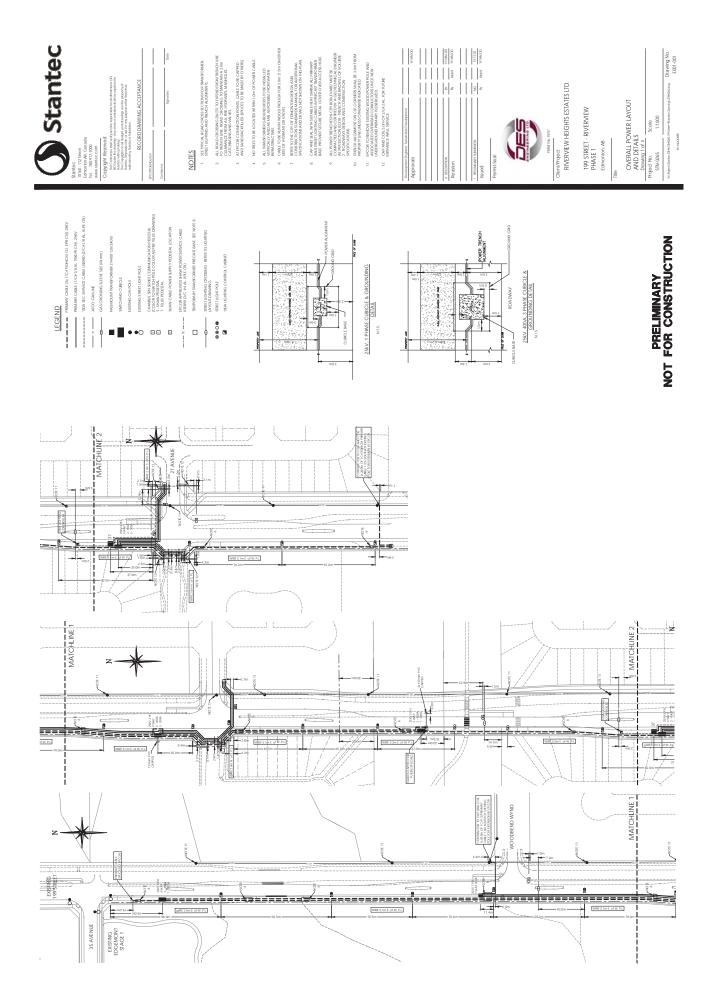


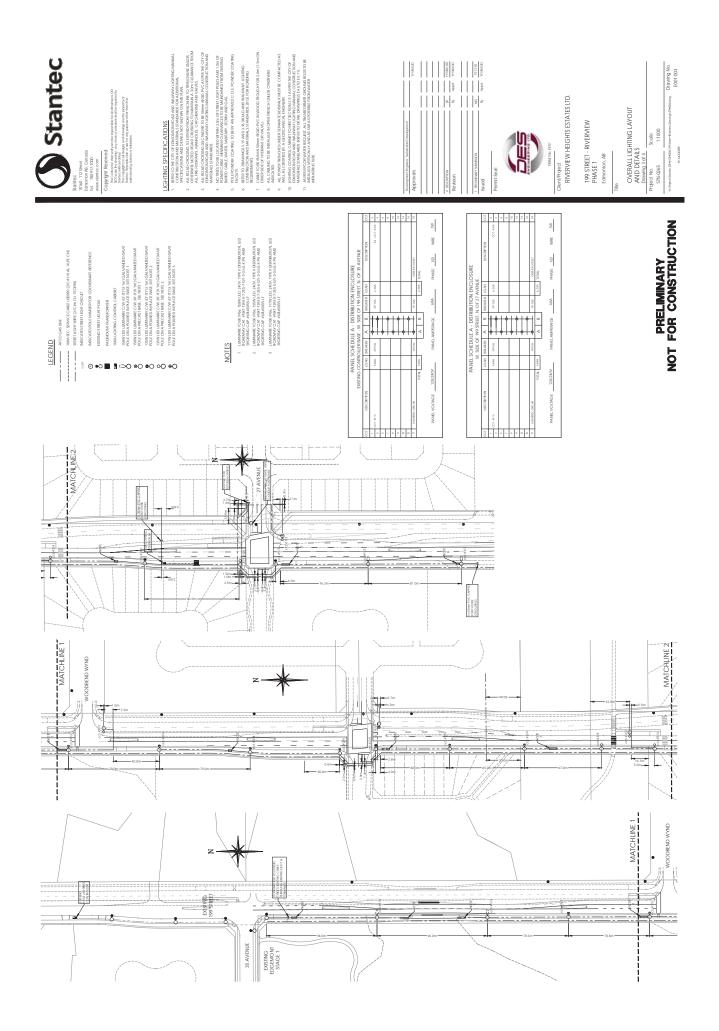
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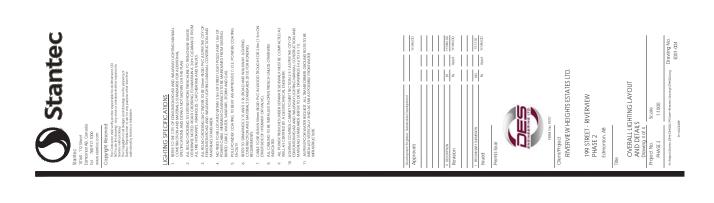




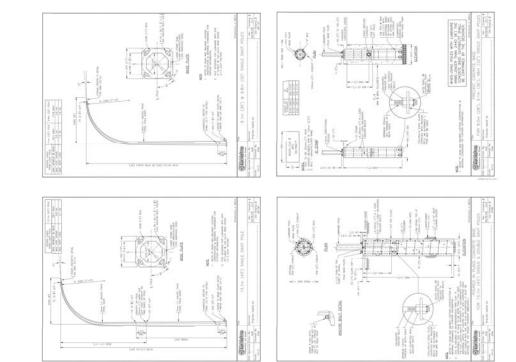


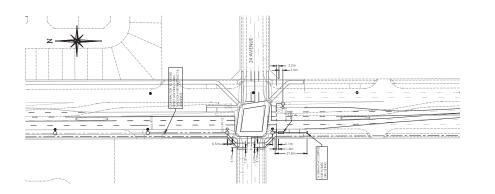




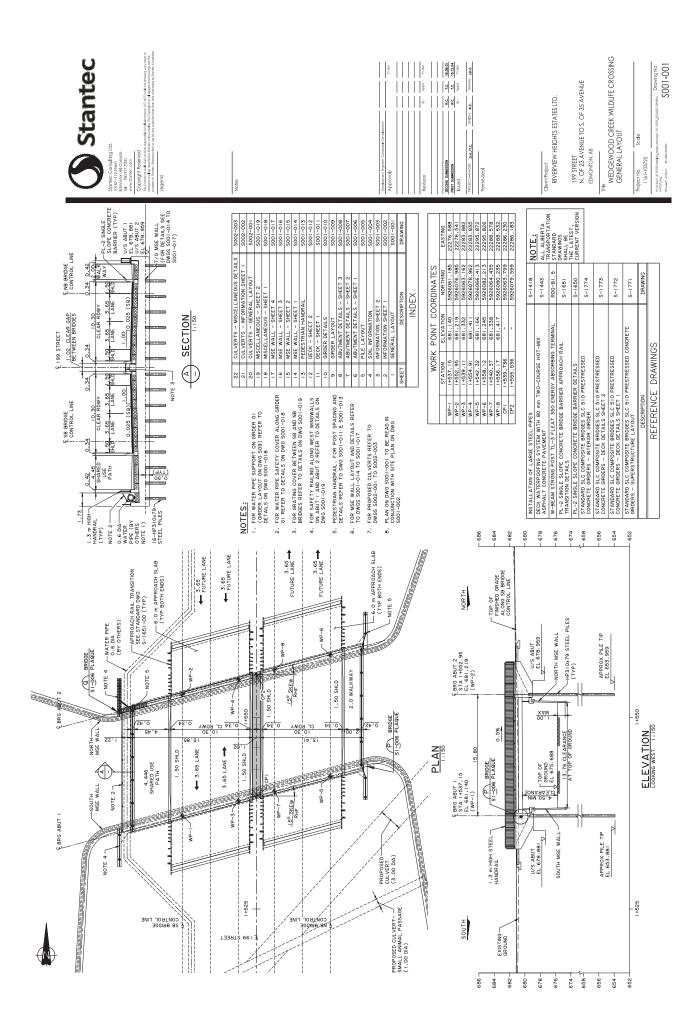


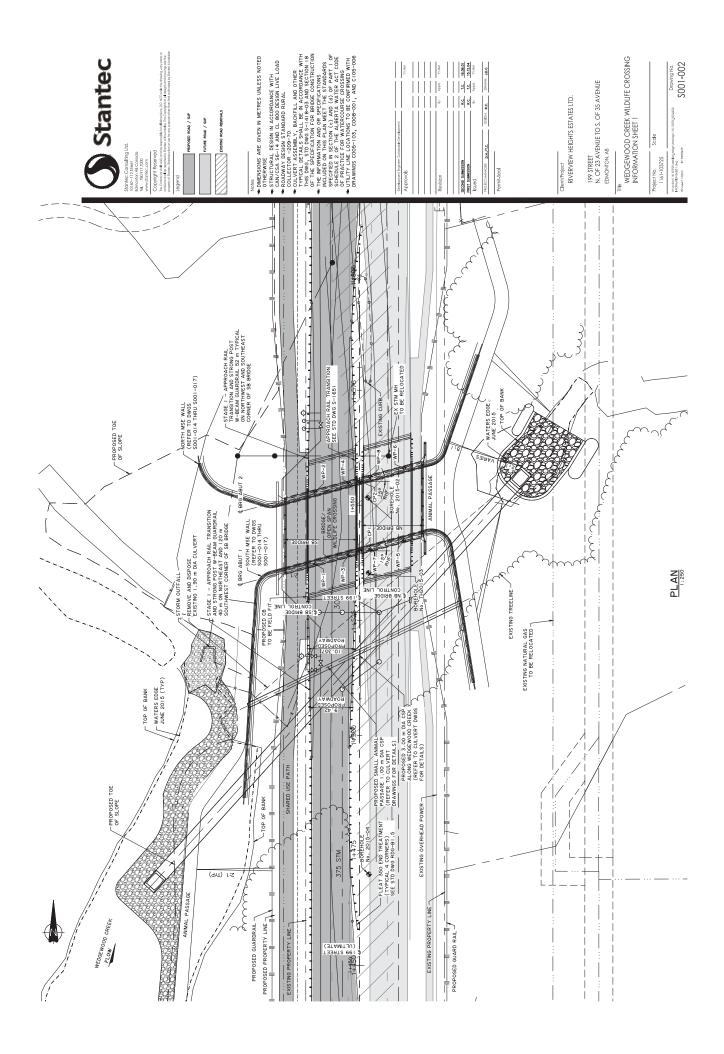


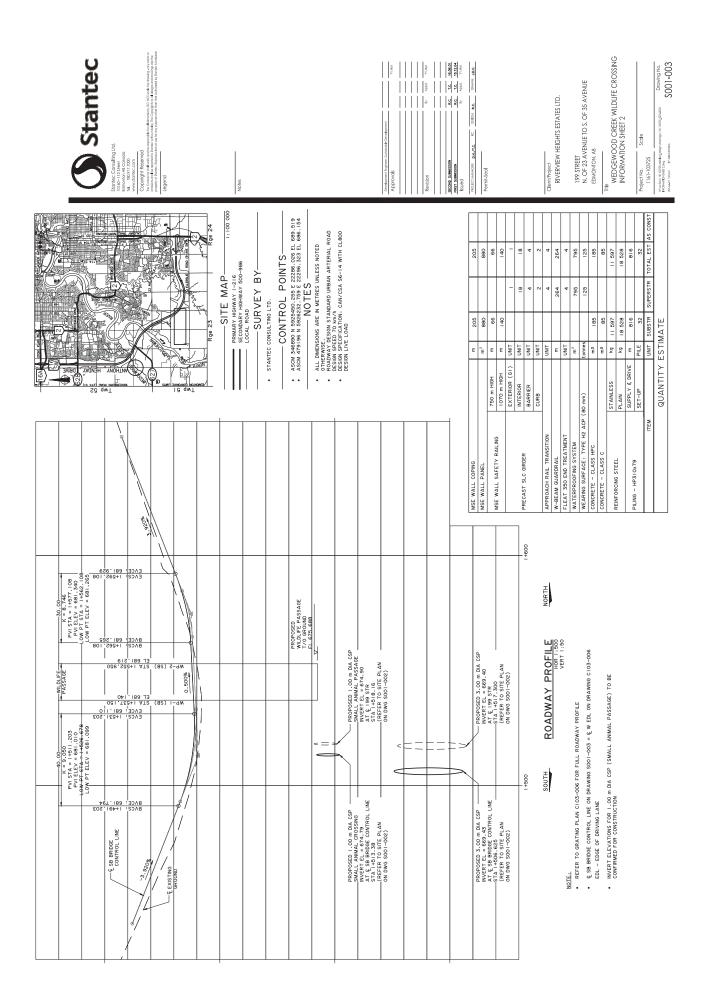


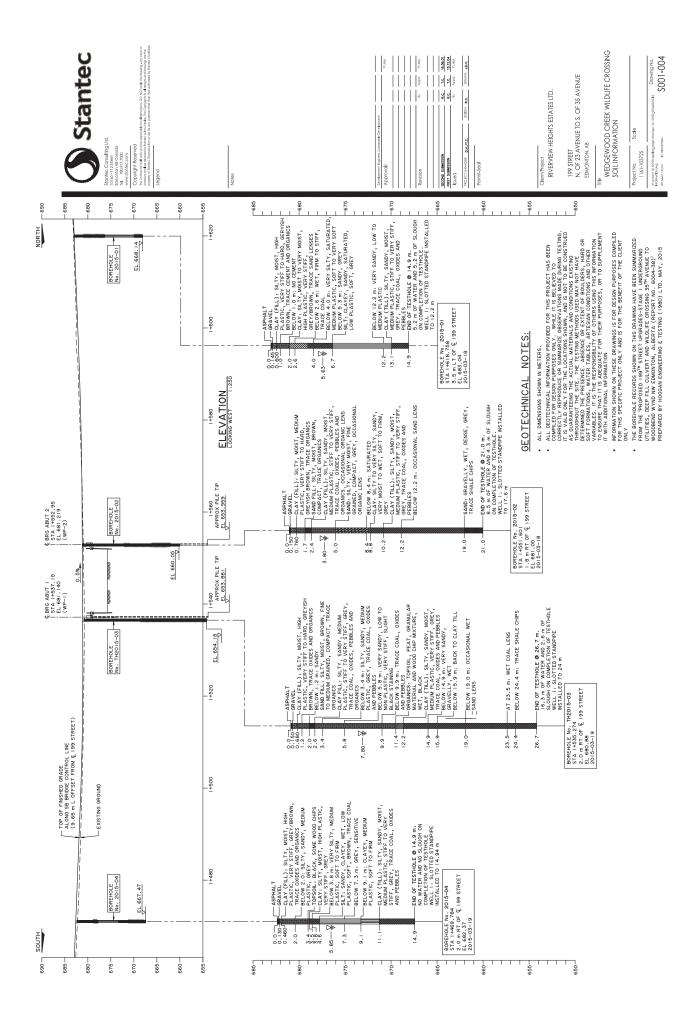


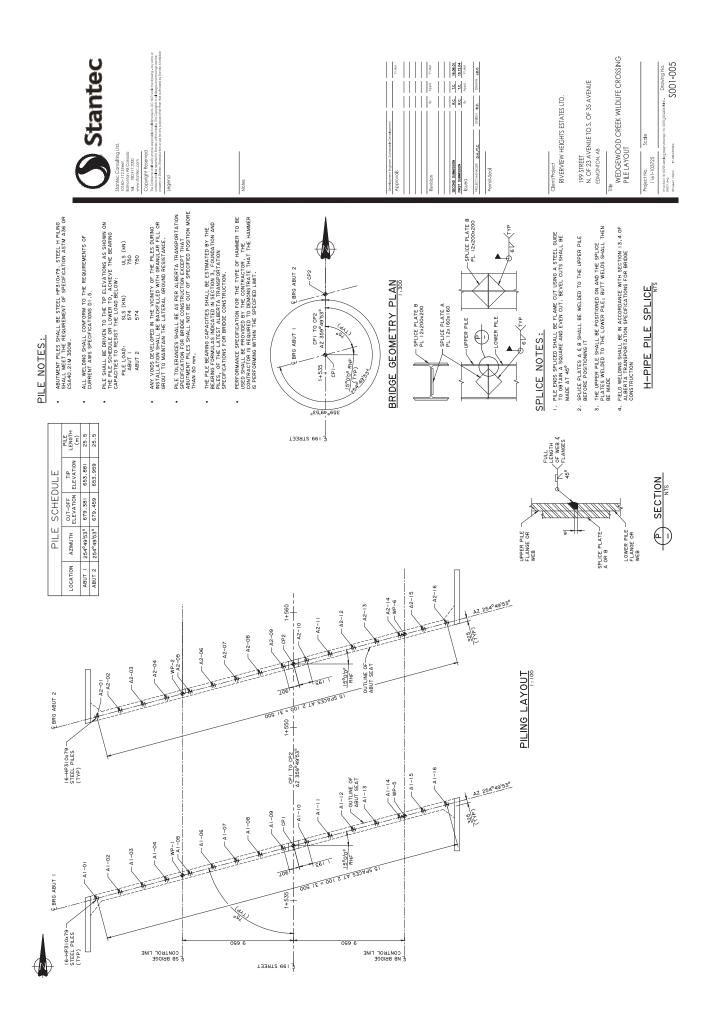
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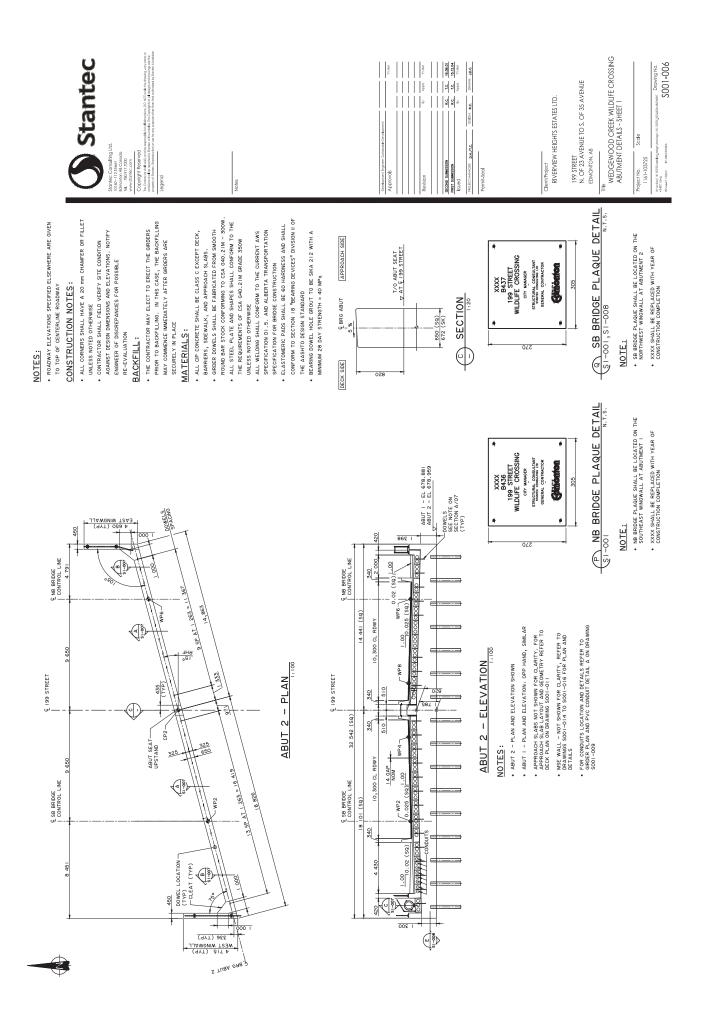


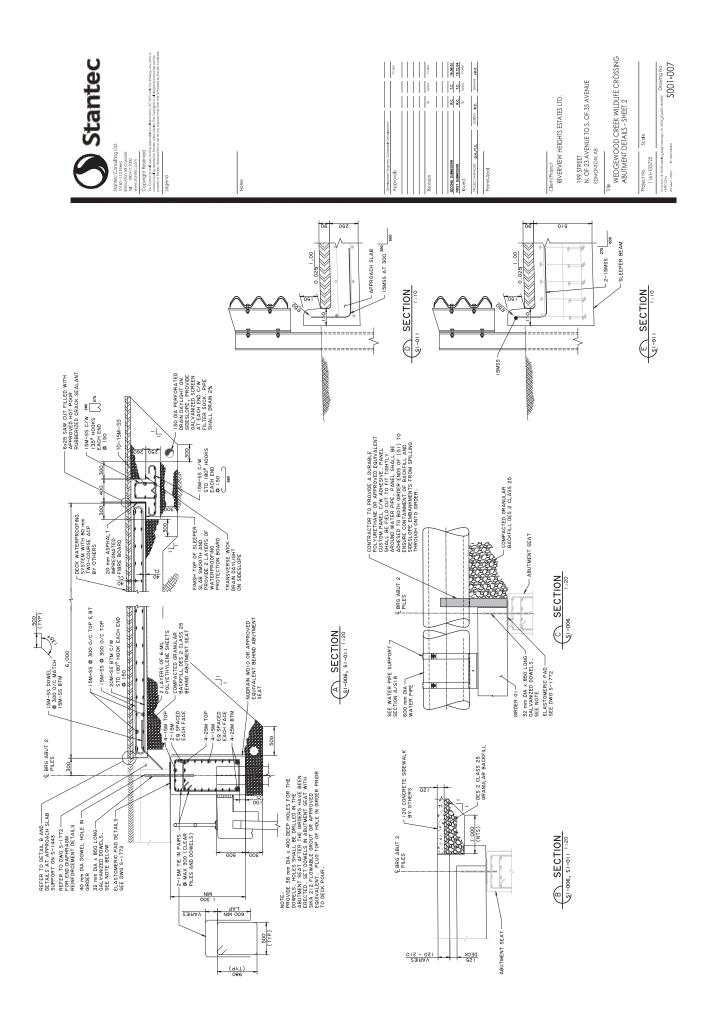


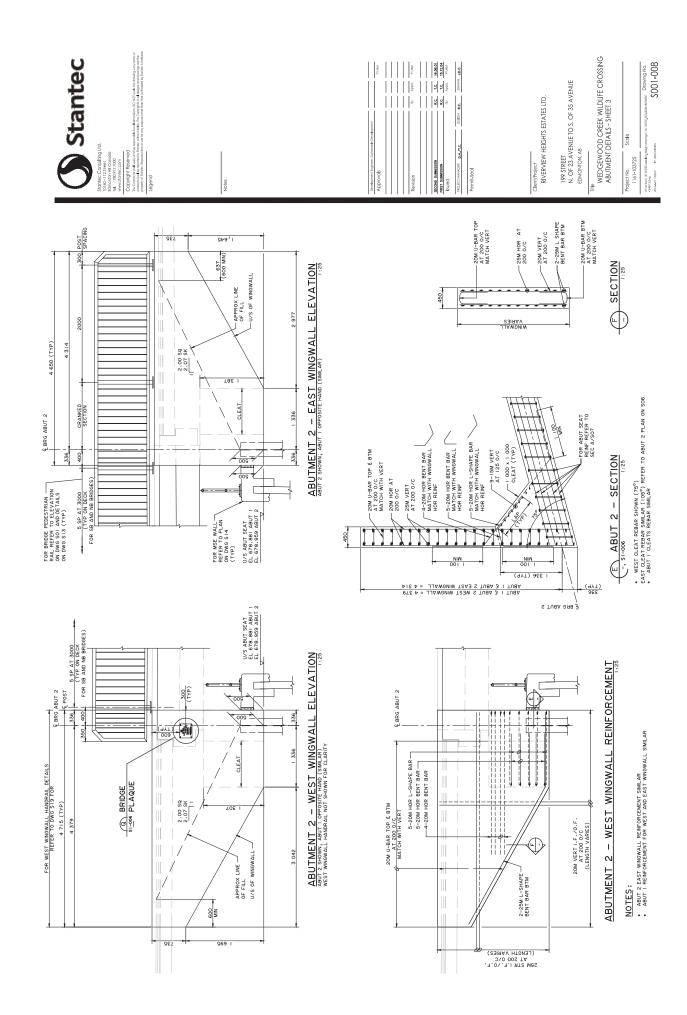


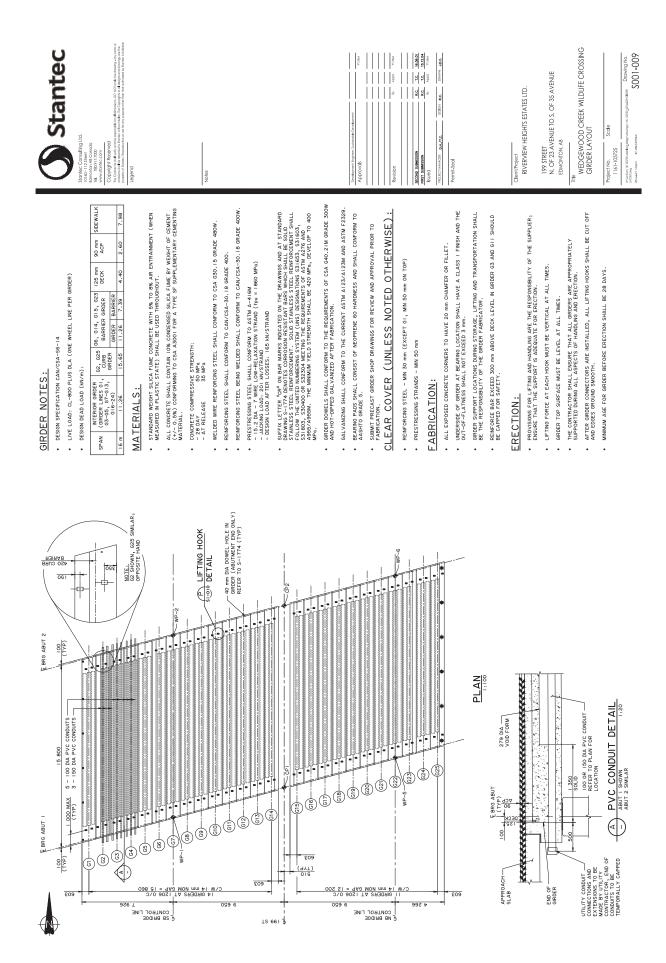


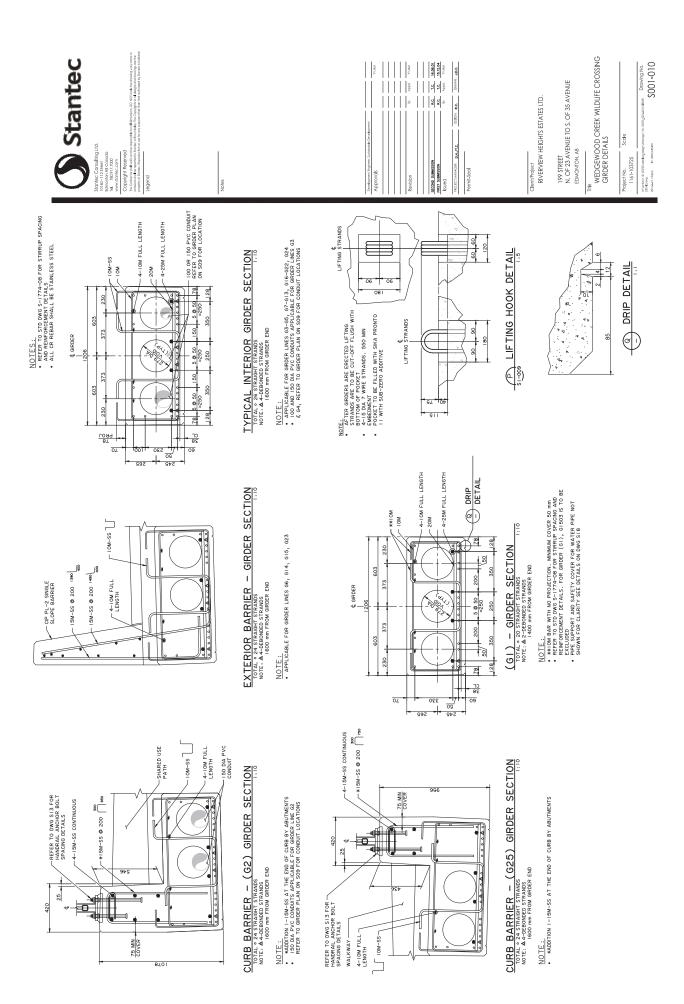


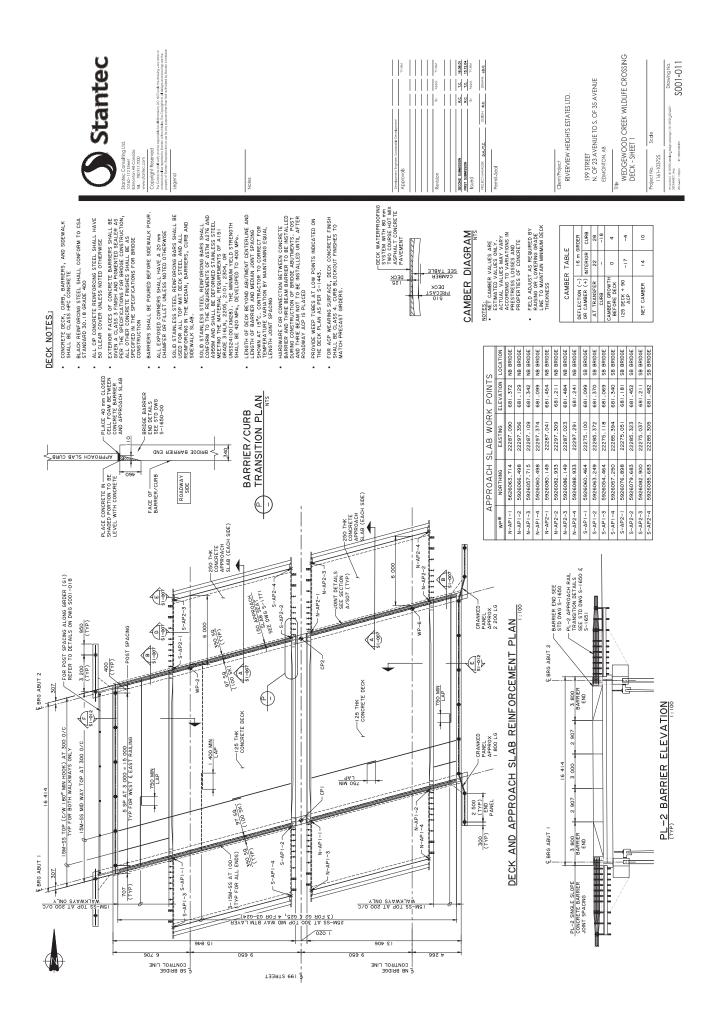


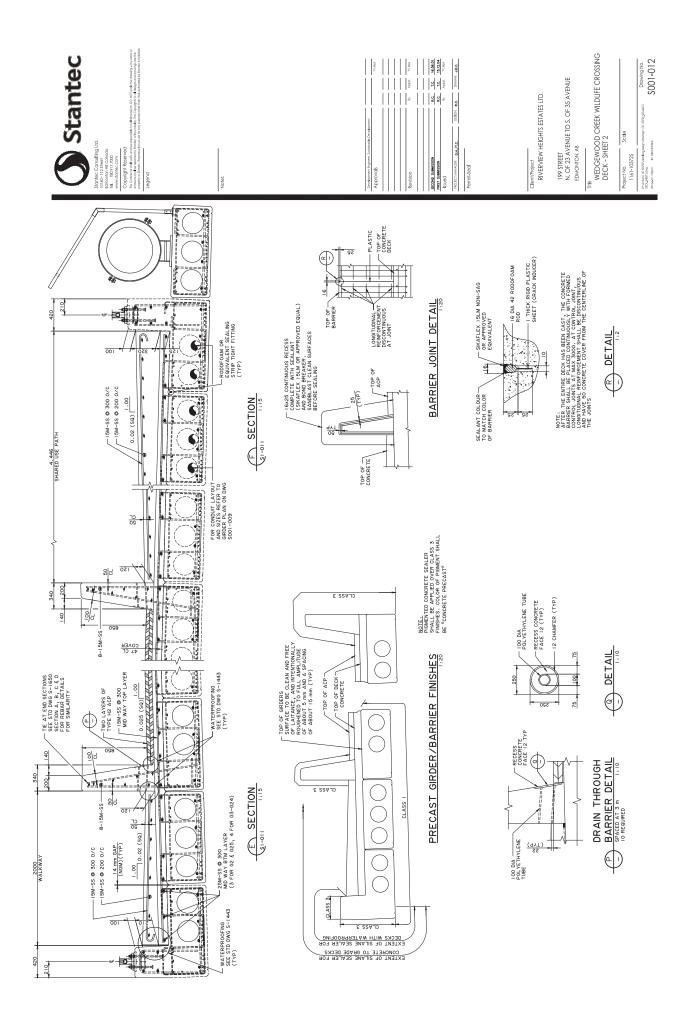


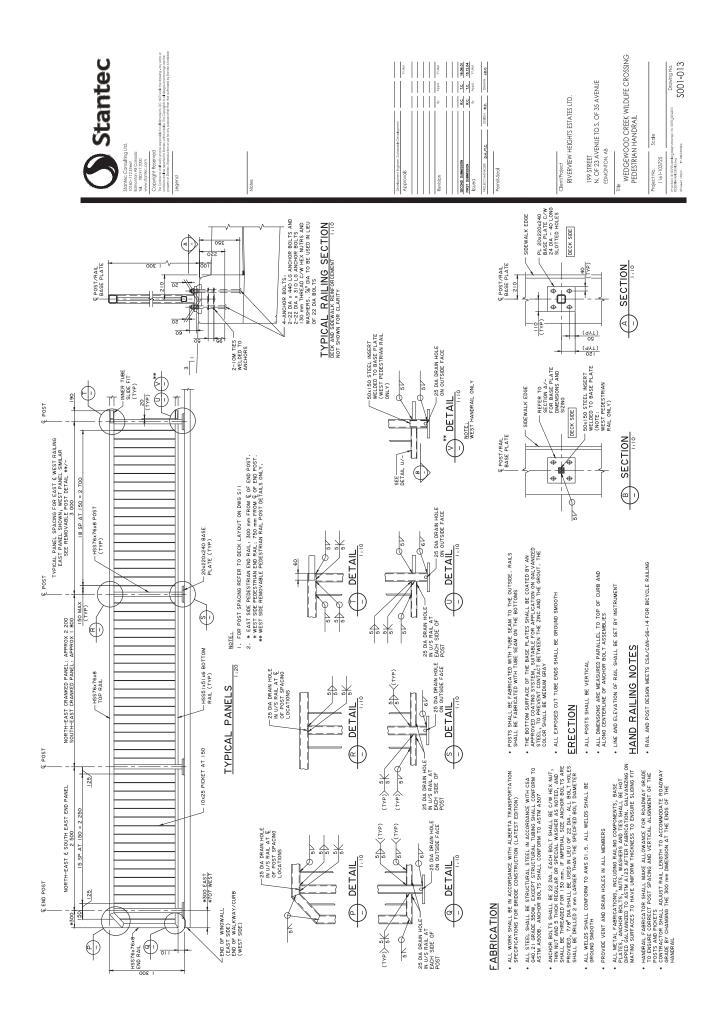


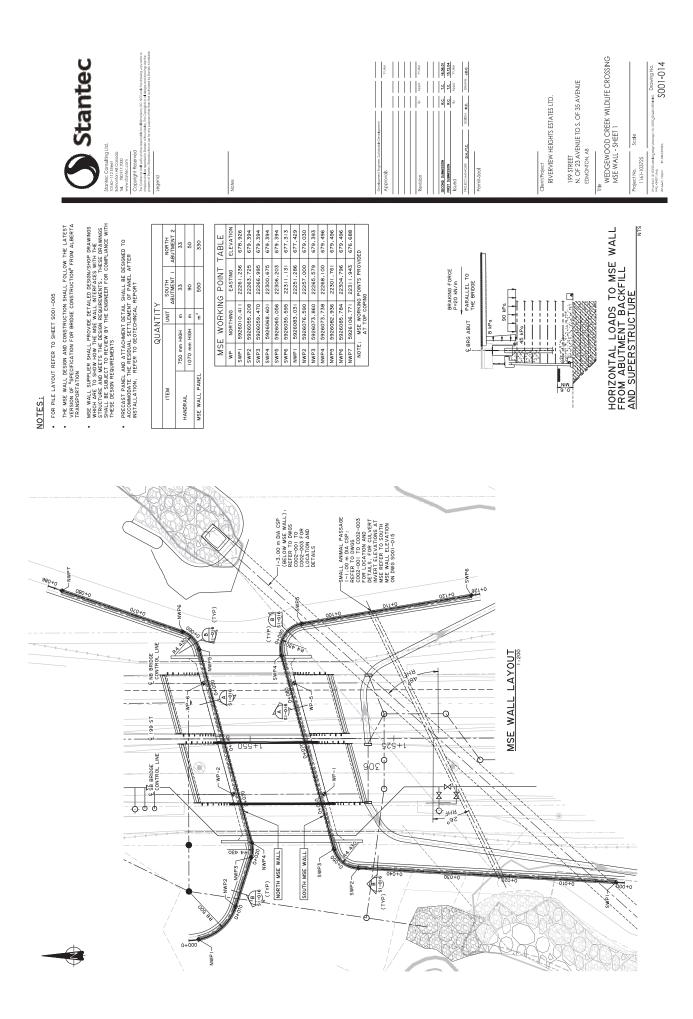


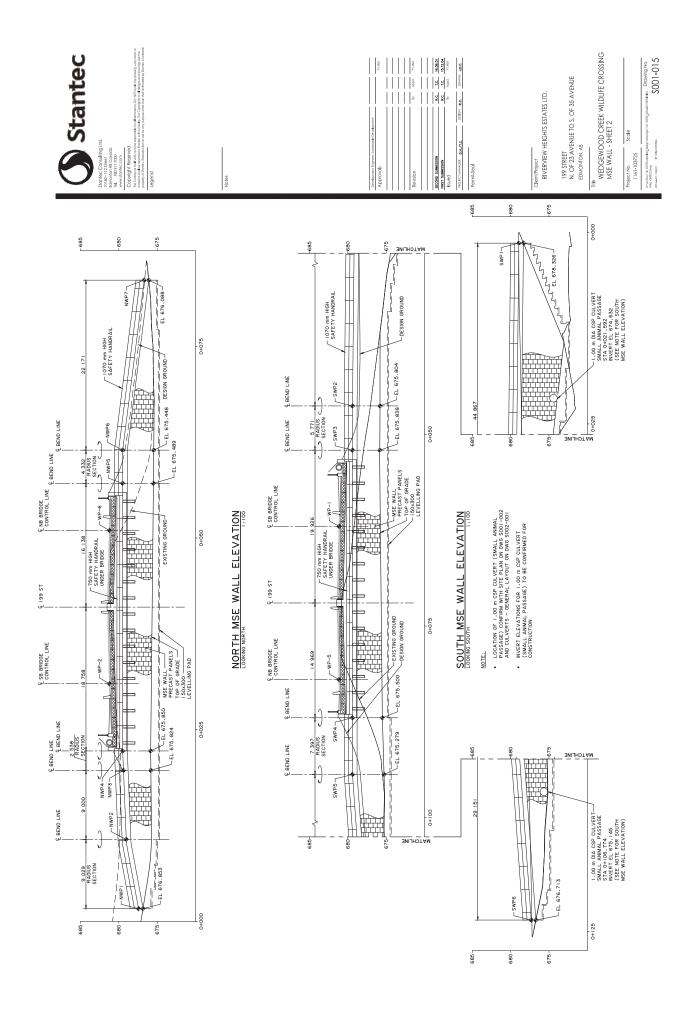


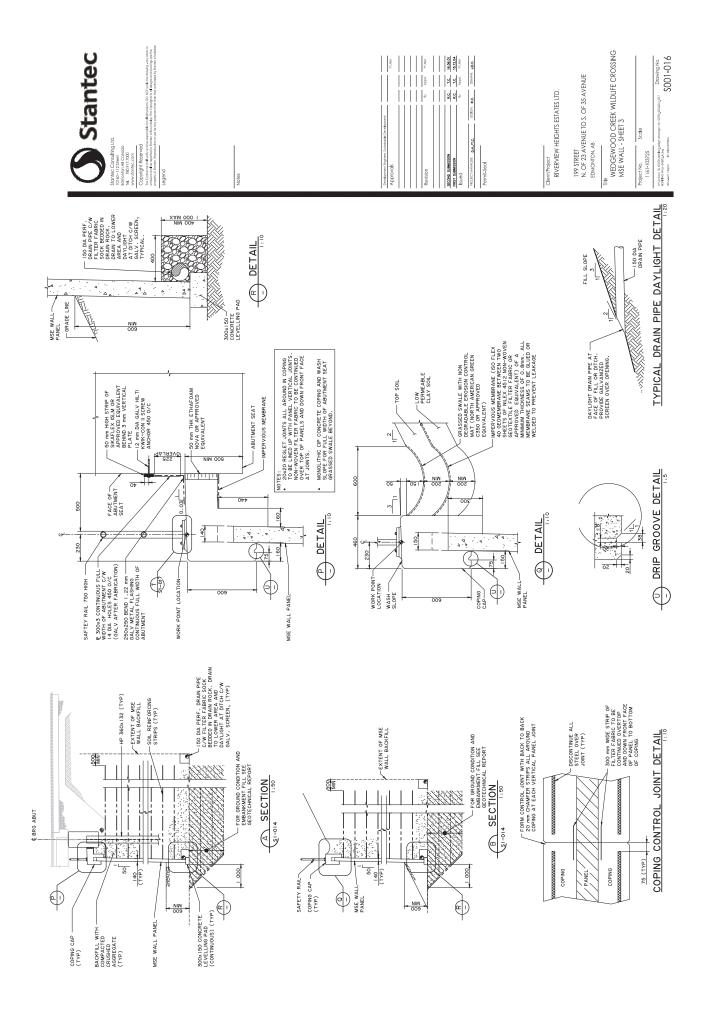




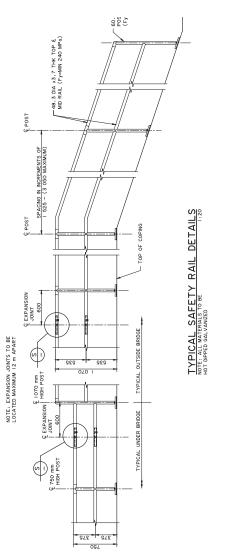


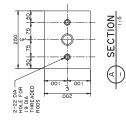


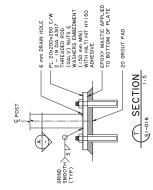


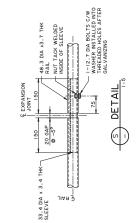


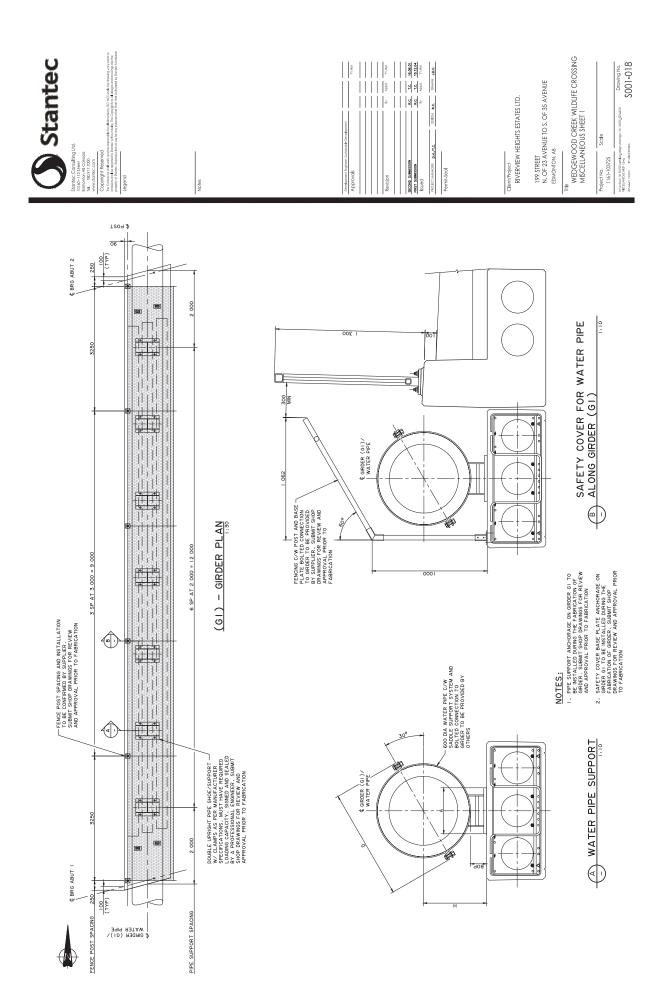


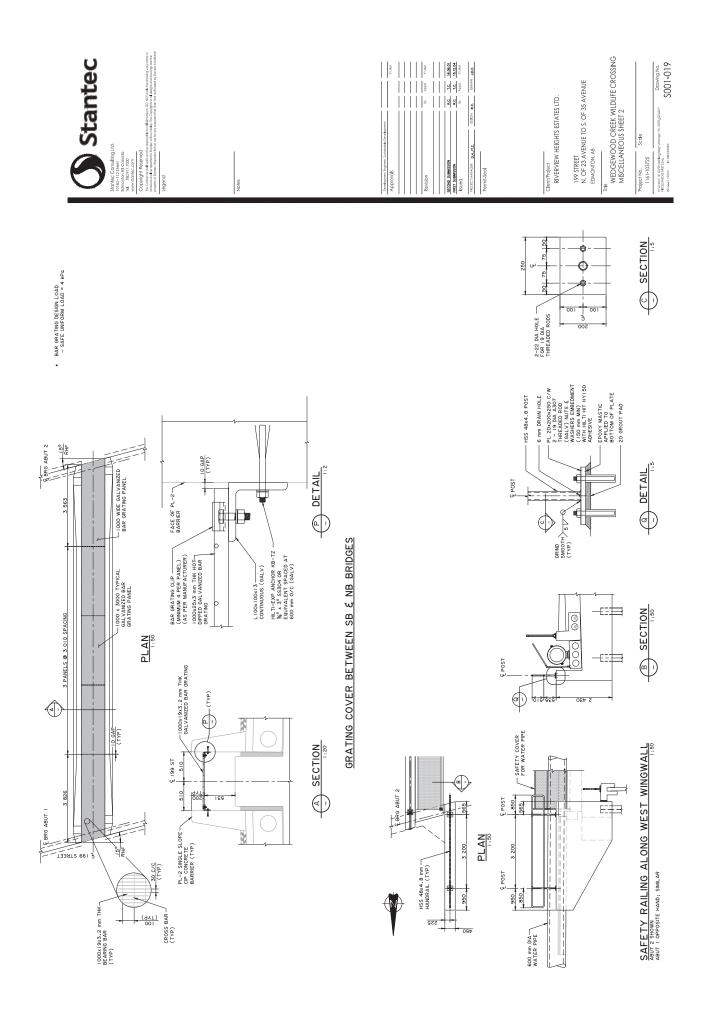


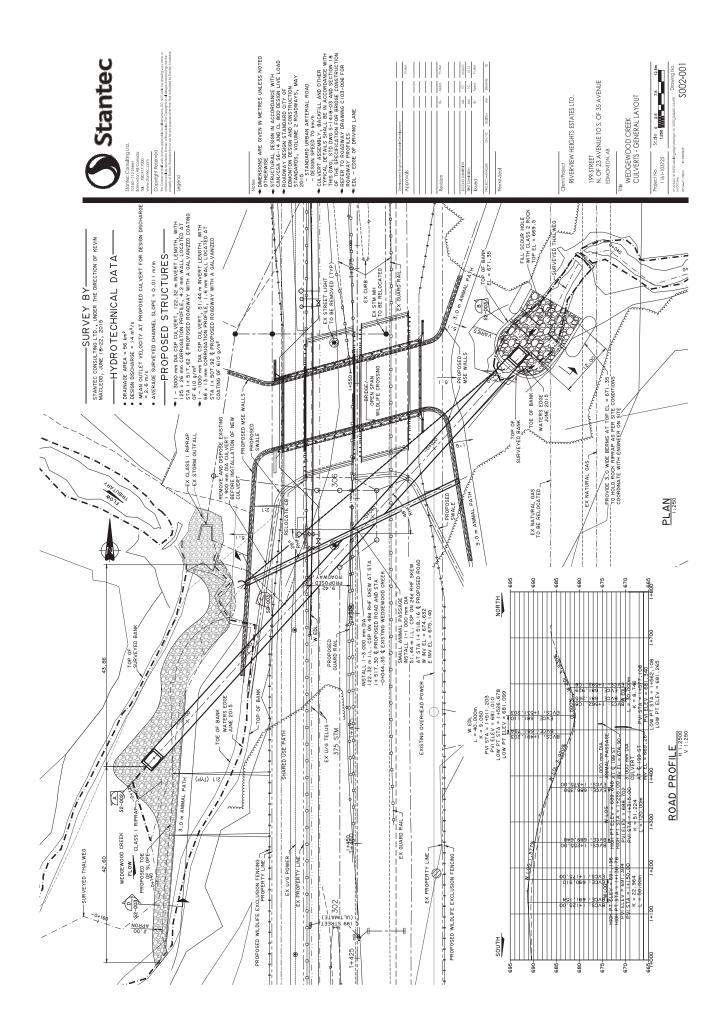


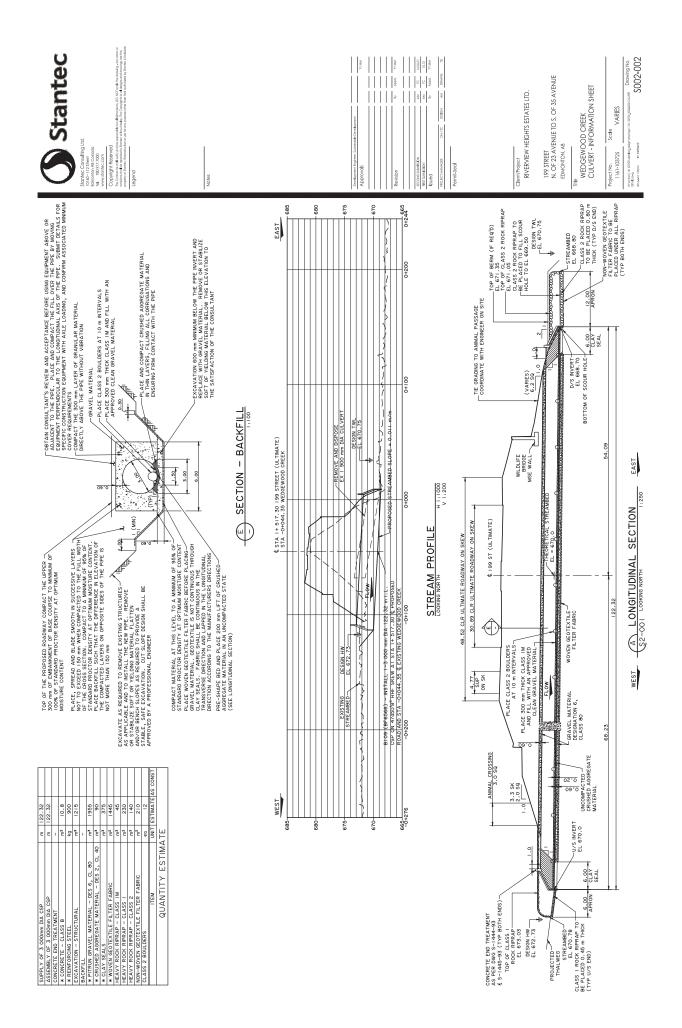


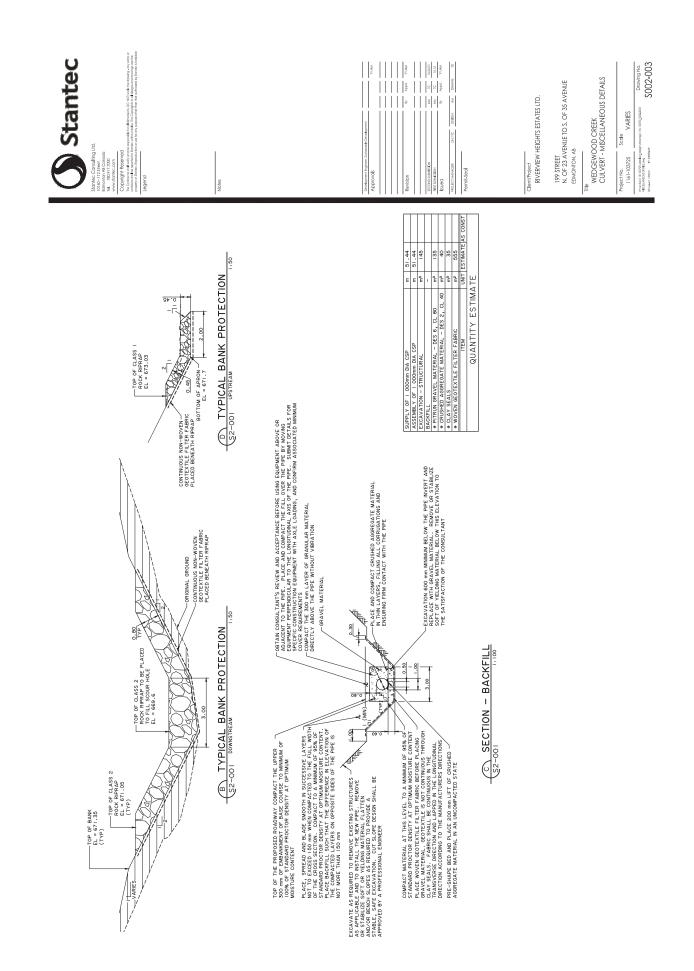


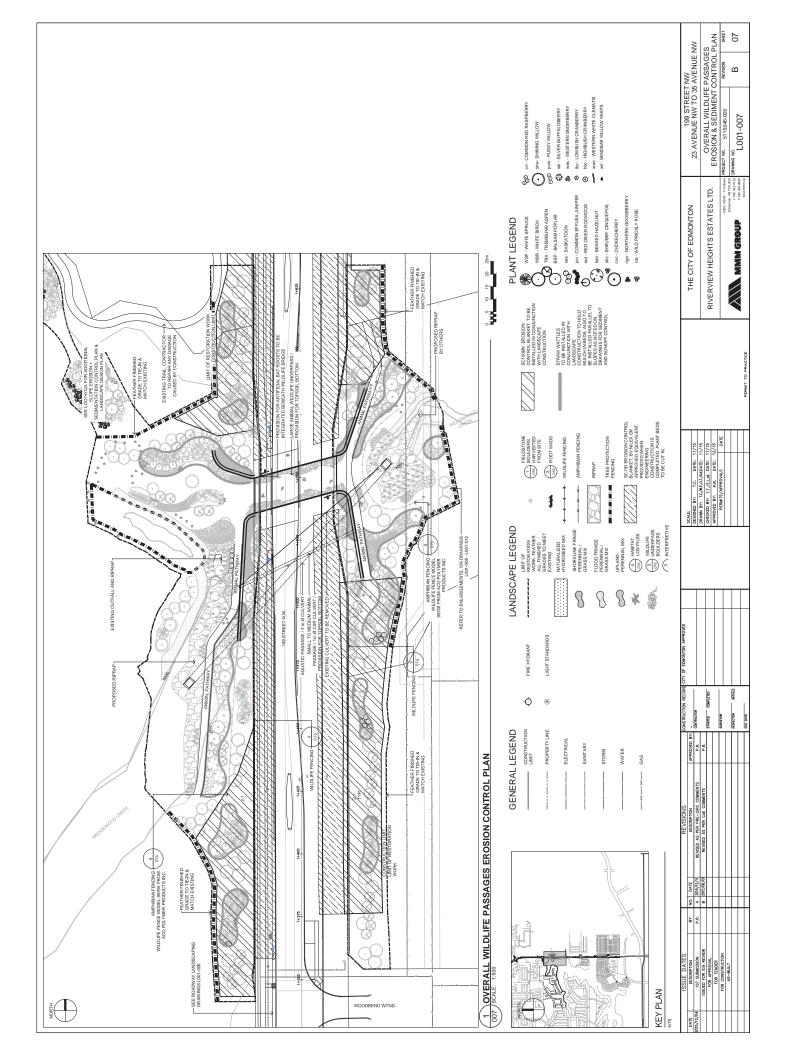


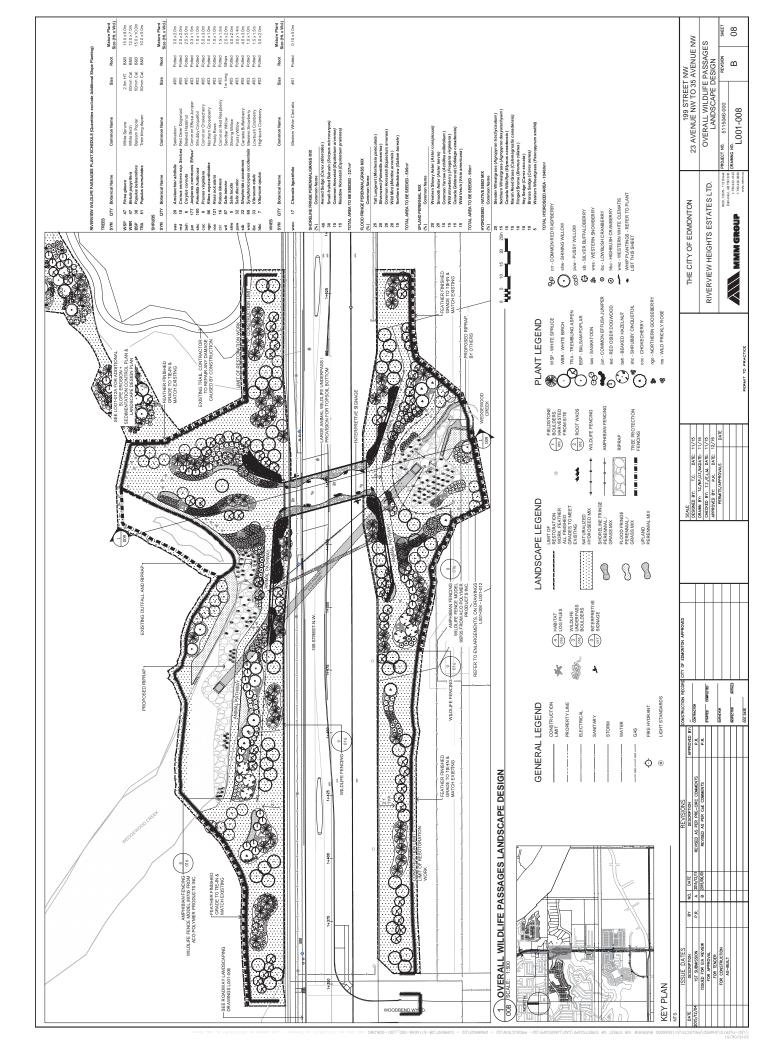


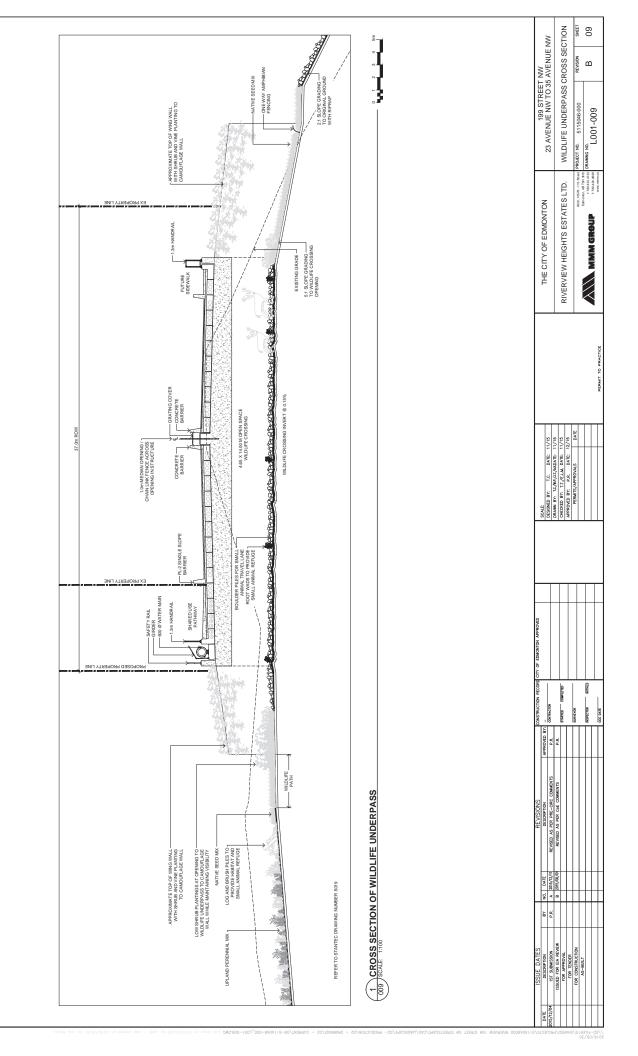


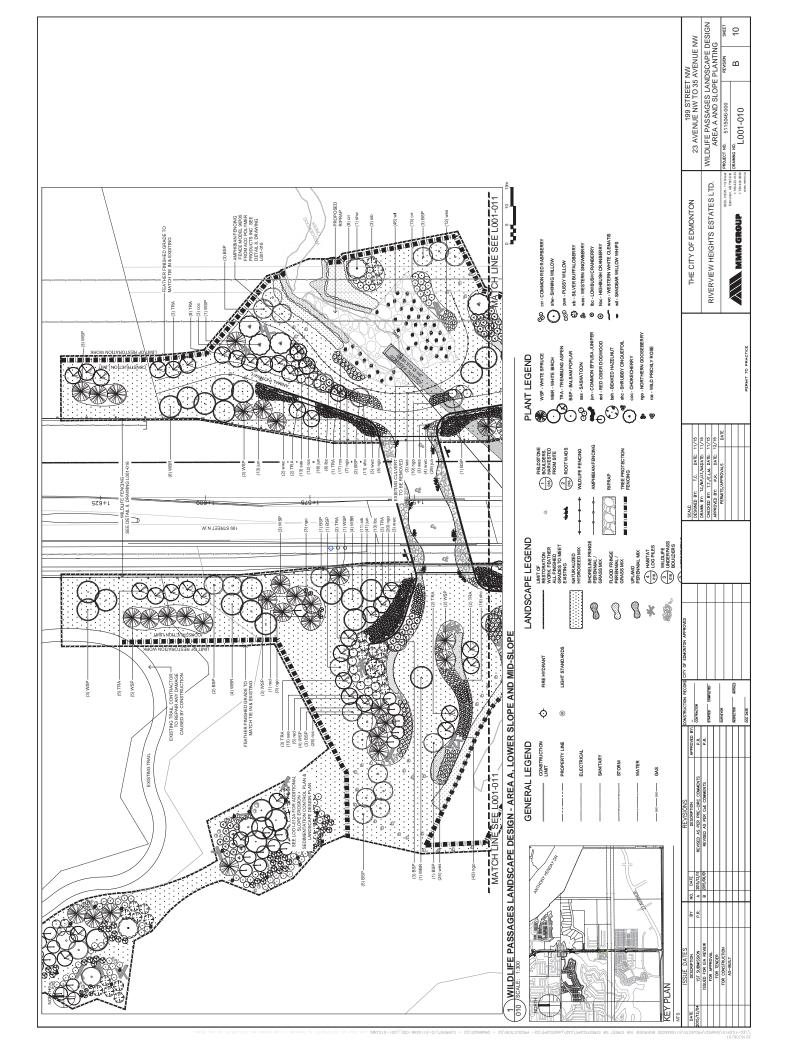


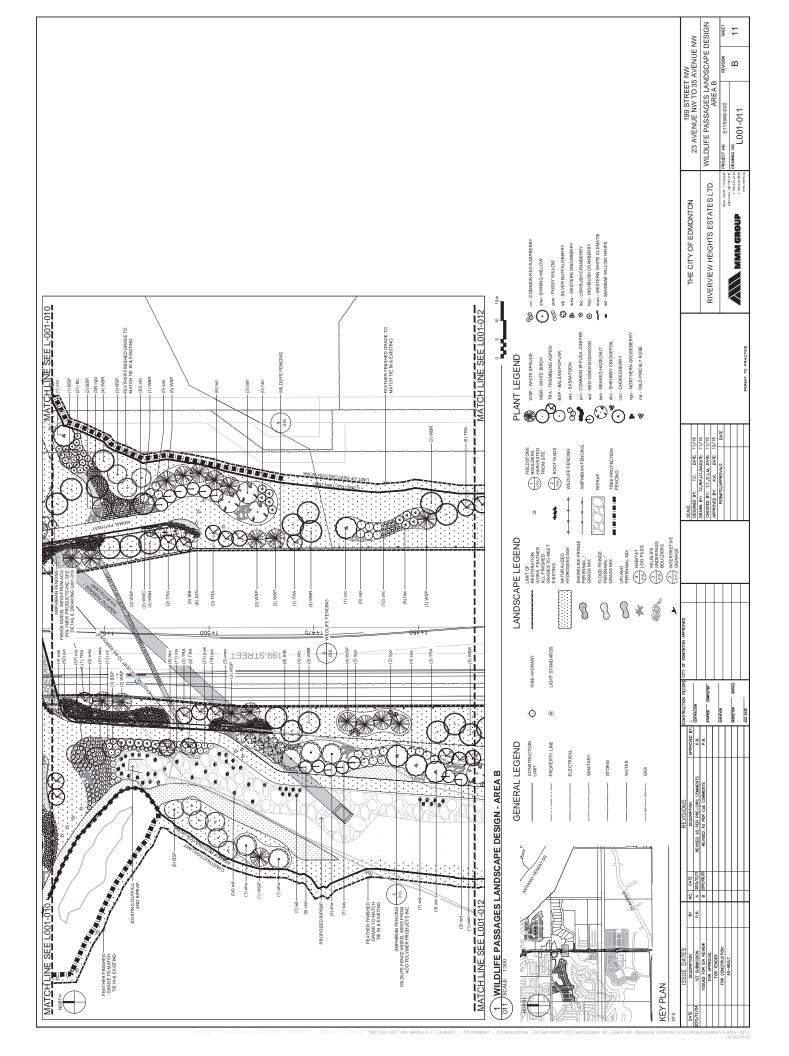


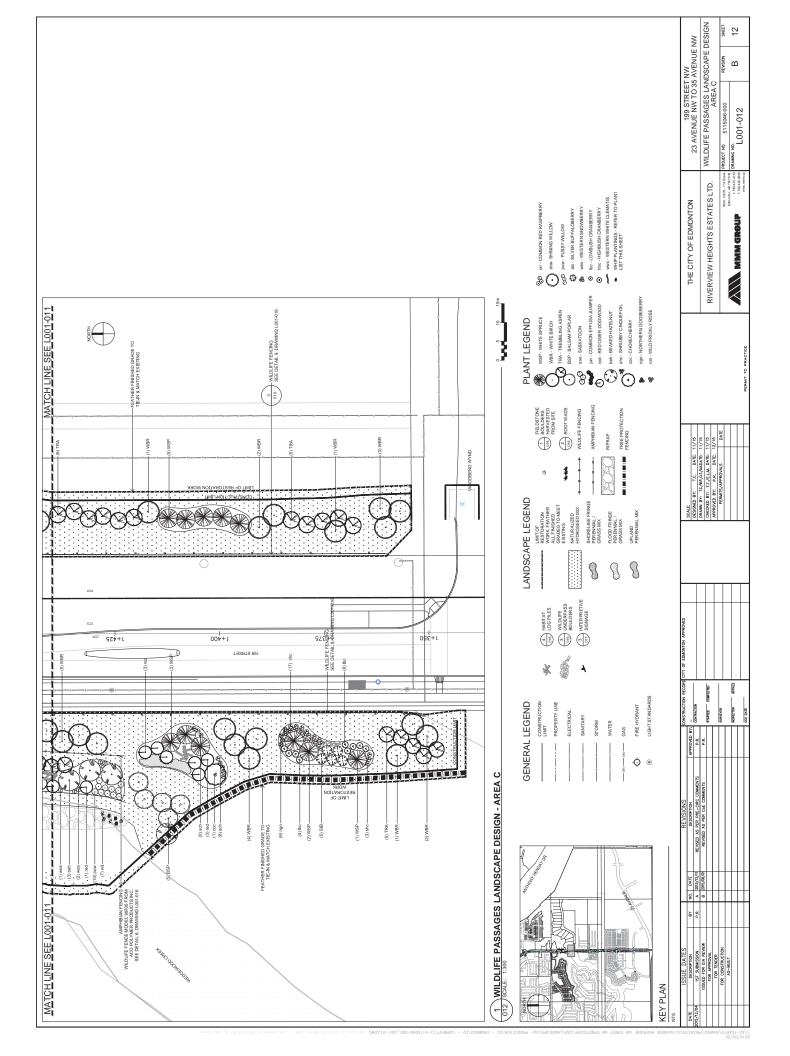




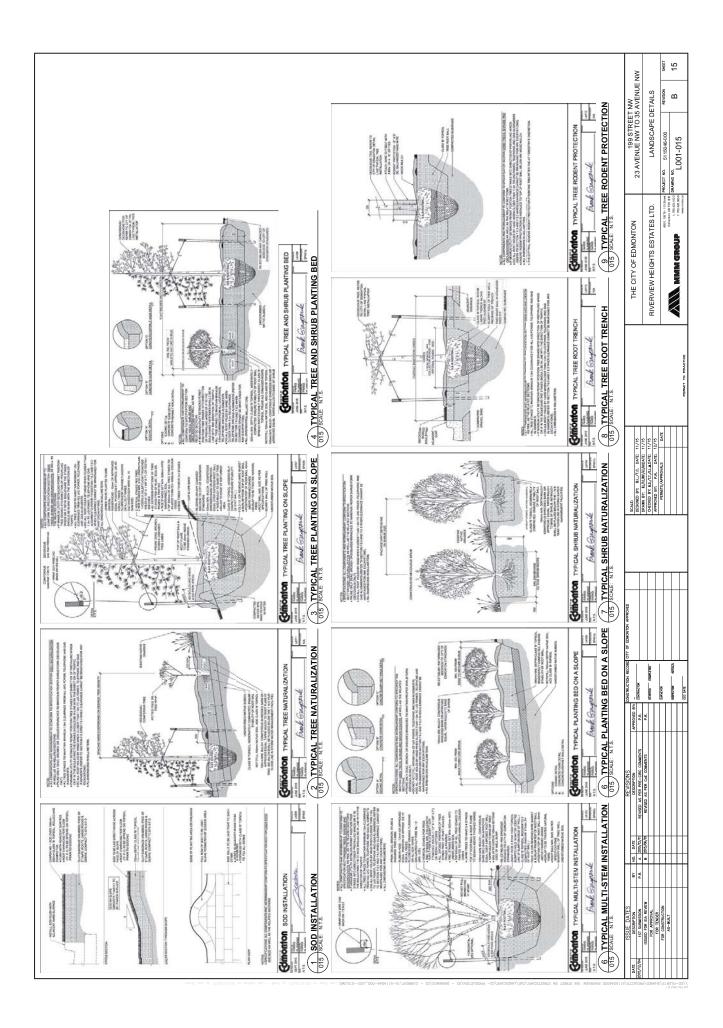


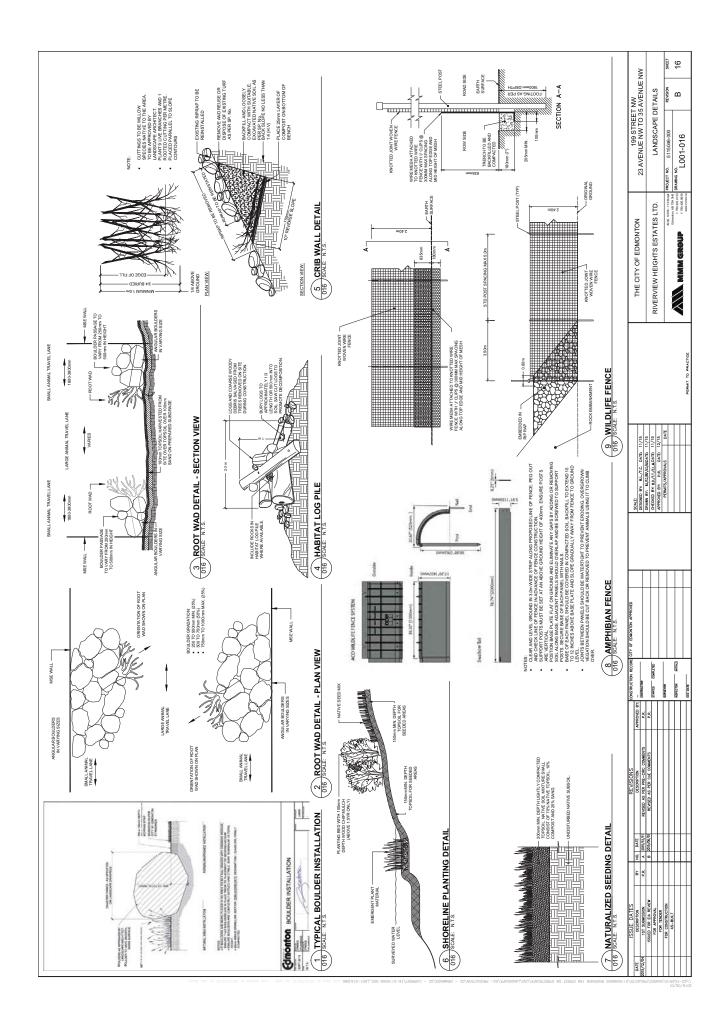


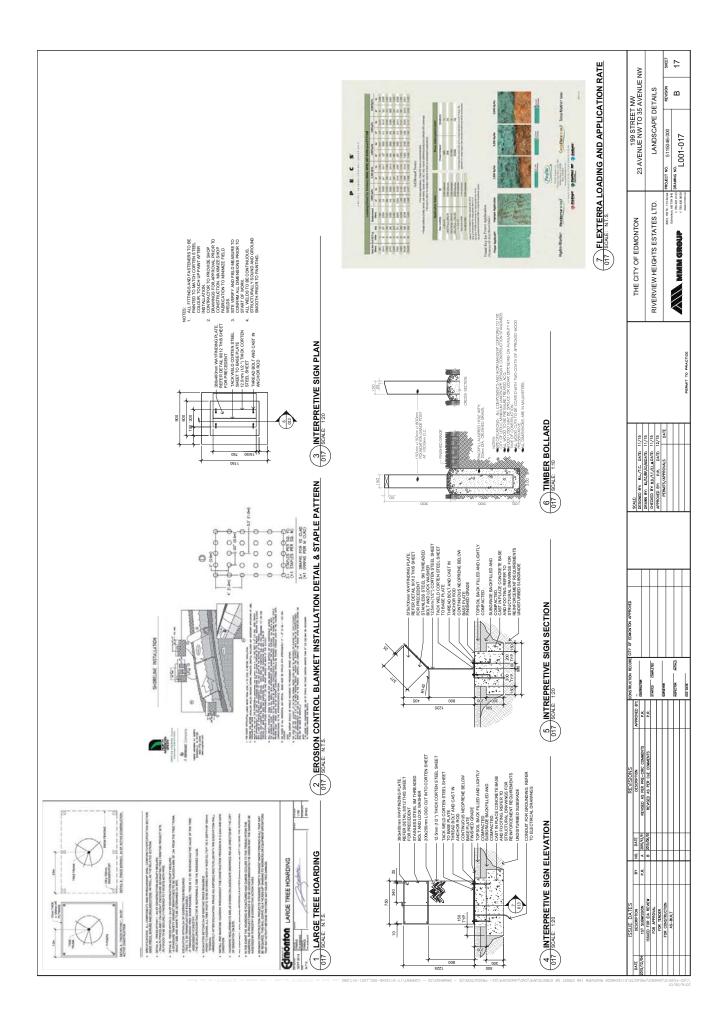












APPENDIX D SUPPORTING DOCUMENTATION



To:	Marc Obert	Date:	January 15, 2016
From:	Erin Mastre/ Tara Callaghan	Job No.:	5115046-000
Subject:	199 Street Wildlife Crossing Restoration Brief	CC:	Tony Chiarello (Stantec) Tara Callaghan (MMM)

Key to the design of the Wedgewood Creek Wildlife Crossing was an understanding of basic principles of landscape ecology, connecting patches of habitat via a habitat corridor within the matrix of urban development. The City of Edmonton has identified 11 Ecological Design Groups (EDGs) that may be targeted in the design of wildlife passage (Chisholm et al., 2010). It was anticipated that species from all EDGs could be present within the Wedgewood Creek area. As a result, a general approach rather than a species-specific approach has been taken in the landscape design.

Where existing parcels of vegetation exist, trees and shrub plantings have been proposed adjacent to them to connect and strengthen the Wedgewood Creek corridor. Shrub and tree selection draws largely from a comprehensive species list provided in the Environmental Impact Assessment (EIA) Report prepared for the project area by Stantec (May 2015). Some additional species native to the Edmonton area have also been included. Common Effusa Juniper (Juniper communis 'Effusa') were placed above retaining walls leading to the wildlife passage to create a dense mass that will discourage animal movement above walls, yearround. Western White Clematis (Clematis ligustifolia) was also planted in this area, with the intention that it will trail over the wall edges to help camouflage them.

Shrubby Cinqeufoil (Potentilla fruticosa) was added to increase the variety of shrubs under 1m in height. Finally, Pussy Willow (Salix discolor) and Sandbar Willow (Salix interior) were included to increase variety along the creek edge.Perennial seed mixes specific to different hydric zones (Shoreline, Fringe and Upland mixes) were developed using various forbs listed in the comprehensive species list of the EIA, as well as the following species native to the Edmonotn area: Awned Sedge (Carex atherodes), Small-fruited Bulrush (Scirpus microcarpus), Silverweed (Potentilla anserina), Wild Mint (Mentha arvensis), Common Yarrow (Achillea millefolium), Canada Goldenrod (Solidago canadensis), Canada Wild Rye (Elymus canadensis), Marsh Reed Grass (Calamagrostis canadensis), Fringed Brome (Bromus ciliatus), Bronze Sedge (Carex aenea), Western Wheatgrass (Pascopyrum smithii).

To encourage animal movement toward the small to medium animal passage, mixed shrub corridors that provide coverage and protection for animals have been designed to meander from undisturbed areas to the passage entry. Brush and logs piles were placed in a random fashion throughout the project area to create instant and additional habitat and offer refuge from predators. Within the small to medium animal passage, provision for a topsoil bottom was given as it is provides more comfort for animal movement than that of a cold concrete base. Concrete wing walls from the crossing will be neutrally stained in 'Davis Colour Green Slate 3LBS 3685'.

For larger animal movement, Stantec Engineering has allowed for pathways that lead to the wildlife underpass. To attract large animals to the pathways, fruiting shrubs such as Saskatoon (Amelanchier alnifolia) and Northern Gooseberry (Ribes oxyacanthoides), and other native



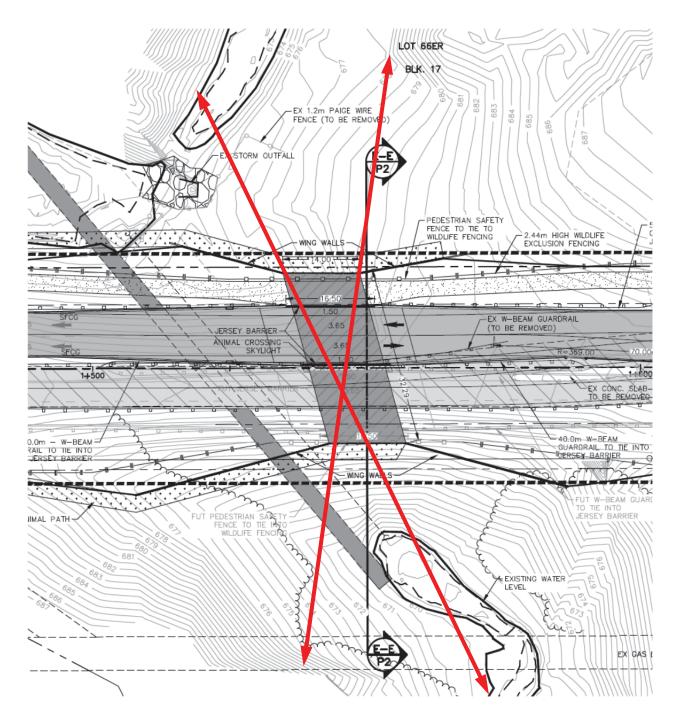
shrubs commonly foraged on by deer such as Willows (Salix spp.) are to be planted along it. Willow whips planted within the riprap along the west pathway also serve to stabilize the creek edge.

To maintain sightlines for larger animals to the wildlife underpass, only shrubs less than 1m in height were planted directly in front of the underpass. Within the underpass itself, provision for a topsoil bottom was given as this is the preferred substrate for large animal movement. Root wads and boulders have been integrated along the edges of the underpass to provide protection and refuge to smaller animals while serving to camouflage the interior walls and bring a more natural aesthetic to the corridor. Artificial bat roosts have also been proposed, to be integrated on the underside of the bridge to encourage bats to cross under the road rather than above. Alternatively, large tree species have been proposed above the bridge to encourage birds to cross over 199 Street at a height that will not intercept vehicles.

Lastly, in addition to the wildlife fencing that is proposed along 199 Street, we have included an amphibian fence at a lower elevation. Considering that amphibian migration occurs between dry and wet habitats rather than along a moist corridor such as the creek edge, efforts to prevent amphibian movement toward the road edge were made. While silt fencing is a common method used for such an application, we specified ACO one-way fencing as it requires less maintenance and upkeep and has a more discrete appearance. This simple fence system allows small to large animals to move freely across the fence while restricting amphibian movement upslope above the fence toward the roadway, instead limiting it to one direction toward the creek.

Sources:

Chisholm, M., Bates, A., Vriend, D. and Cooper, D. 2010. City of Edmonton Wildlife Passage Engineering Design Guidelines. Stantec Consulting Ltd.



Sight-lines associated with the 15 degree skew

Wedgewood Creek Crossing at 199 Street NE 6-52-25-W4 and NW 5-52-25-W4, Edmonton, AB

Hydrotechnical Summary Report

Prepared for: Qualico Communities

Prepared by: Stantec Consulting Ltd.



August 2015

Table of Contents

1.0		.1
2.0	SITE DESCRIPTION	.1
	HYDROTECHNICAL SITE VISIT INFORMATION AND REVIEW OF AVAILABLE INFORMATION 3.1.1 Site visit information 3.1.2 Review of available information pertinent to this study	.2 .2
3.3 3.4 3.5	DRAINAGE AREA CONTRIBUTING FLOW TO SITE ASSESSMENT BASIN RUNOFF POTENTIAL METHOD CHANNEL CAPACITY METHOD CHANNEL HYDRAULIC ANALYSIS RECOMMENDED DESIGN AND CHECK DISCHARGE PARAMETERS	.6 .8 .8 .9
4.1 4.2	STRUCTURE HYDRAULICS EXISTING ONE 1.8 M DIAMETER CLOSED BOTTOM STRUCTURAL PLATE CORRUGATED STEEL PIPE (SPCSP)	10 11
	STEEL PIPE (SPCSP) SINGLE 3.0 M SPAN BY 2.4 M RISE CONCRETE BOX CULVERT	12 14
5.0	ROCK PROTECTION WORKS	
6.0	ENVIRONMENTAL CONSIDERATIONS	16
7.0	GEOTECHNICAL	17
	STRUCTURE OPTIONS	
	OPTION B – SINGLE 3050 MM DIAMETER CLOSED BOTTOM STRUCTURAL PLATE CORRUGATED STEEL PIPE (SPCSP)	18
9.0	OPINION OF PROBABLE COST	19
10.0	DETAILED DESIGN CONSIDERATIONS	20
11.0	DRECOMMENDATION	20
11 (CLOSING	22

Stantec

Wedgewood Creek Crossing at 199 Street, Hydrotechnical Summary Report August 2015

APPENDICES

APPENDIX A	TOPOGRAPHIC MAPS AND DRAINAGE AREA ASSESSMENT
APPENDIX B	JUNE 18, 2015 SITE VISIT PHOTOS
APPENDIX C	CHANNEL HYDRAULIC RESULTS
APPENDIX D	STRUCTURE HYDRAULICS RESULTS
APPENDIX E	SITE SURVEY INFORMATION
APPENDIX F	SKETCHES
APPENDIX G	GEOTECHNICAL REPORT
APPENDIX H	COST ESTIMATES

1.0 Introduction

Stantec Consulting Ltd. (Stantec) was engaged by Qualico Communities to complete the hydrotechnical investigation for a proposed culvert replacement located at 199 street over Wedgewood Creek Edmonton, Alberta. The overall project includes the widening of a roadway on 199 street in support of a development for Riverview Neighborhoods 1, 2 and 3.

This report provides a hydrotechnical summary for the proposed culvert replacement. The hydrotechnical assessment was carried out to determine the impact of the design flood i.e. 1:100 year flood on the proposed culvert replacement options. For the purpose of this report, the Wedgewood Creek will be referred to as the "WWC".

2.0 Site Description

The proposed Wedgewood Creek (WWC) crossing is located at 199 street, within NE 6-52-25-W4 and NW 5-52-25-W4, Edmonton, Alberta (53°28'1.46"N, 113°39'51.69"W). WWC is a North Saskatchewan River (NSR) tributary that has its headwaters in the tablelands and then transition to a deeply incised ravine as it flows towards river. This crossing is situated approximately 3.3 km upstream of WWC confluence with North Saskatchewan River (NSR). The existing structure at WWC crossing consists of a single 1.8 m diameter x 68.6 long Structural Plate Corrugated Steel Pipe (SPCSP) culvert installed at approximately 40° RHF skew with roadway centerline. The Anthony Henday Drive (AHD) i.e. highway 216 bridge is located approximately 1.4 km along WWC, downstream of 199 street crossing. Figure A1 given in Appendix A shows approximate location of WWC crossing at 199 street.

3.0 Hydrotechnical

The proposed Wedgewood Creek (WWC) crossing is located at 199 street. WWC is a North Saskatchewan River (NSR) tributary that has its headwaters in the tablelands and then transition to a deeply incised ravine as it flows towards river. The most of the drainage area, contributing flows to the proposed site is relatively flat and is characterized by farming fields, vegetated land, small lakes and interconnected ponds (during high runoff periods). The watercourse at and in the vicinity of proposed crossing has high beaver activity and there are several beaver dams along WWC. During design flood these beaver dams would act as weirs and design flood would pass over them. From 215 street to 184 street all WWC crossings

appear to be undersized for design flood except AHD bridge. The high beaver activity and undersized culvert crossings has resulted in ponded water along WWC.

There are no Water Survey Canada (WSC) stream flow measurement gauges on the WWC. Figure A1 given in Appendix A shows approximate location of WSC gauges in vicinity of study area. Based on Golder Associates Ltd. December 2012 report the drainage area contributing to the WSC gauge Whitemud Creek Near Ellerslie (i.e. number 05DF006) is similar in basin characteristics to the drainage area contributing flow to the proposed WWC crossing. The 05DF006 gauge has a drainage area of 330.4 km² and is located approximately 8.0 km south west of the proposed crossing. The Golder Associates Ltd. December 2012 report has estimated the drainage area at the proposed crossing to be 170 km². The 05DF006 gauge has been in service since 1969 to the present time. This gauge provides 47 years of hydrometric data record. The maximum instantaneous discharge recorded at this gauge was 114 m³/s on April 23, 1974 with unit discharge of 0.35 m³/s/km².

In order to determine the design (i.e. 1:100 year) flood for WWC crossing at 199 street, a literature and database review for various crossings in the vicinity of study site was conducted. A site visit was carried out on June 18, 2015 as part of this study. Hydraulic analysis of the channel was also conducted.

Components of the hydrotechnical assessment described above assisted in determining the design (1:100 year) flood and associated water level elevation. This hydrotechnical assessment is in accordance with current hydrotechnical design practices.

3.1 SITE VISIT INFORMATION AND REVIEW OF AVAILABLE INFORMATION

There are no stream flow measurement gauges on the Wedgewood creek. There are several stream crossings over the Wedgewood in the vicinity of the 199 street crossing. A site visit on June 18, 2015 was conducted by Claudine Girouard and Arshed Mahmood of Stantec. Appendix B provides site visit photos taken on June 18, 2015.

3.1.1 Site visit information

- The existing WWC crossing at 199 street is a 1.8 m diameter x 68.6 m long (based on Stantec June 18, 2015 survey information) SPCSP culvert. During site visit Stantec was unable to locate 1.05 m diameter overflow culvert installed in roadway embankment as mentioned in Golder Associate Ltd 2012 report.
- WWC has very high beaver activity and high beaver activity was found along WWC reach between 215 street and Anthony Henday Drive (AHD) crossings during site visit (See site visit photos given in Appendix B)
- Debris is accumulated around cage at culvert inlet and has resulted in a considerably reduced culvert flow capacity (see Photos # 15 and 16 given in appendix B). Culvert inlet and cage at inlet are heavily damaged. This suggests that this culvert requires

maintenance at regular intervals. Debris catcher cage contributes to the debris accumulation and eventually becomes another dam at the culvert inlet if debris is not removed. A debris catcher is one solution but only works with regular culvert maintenance and debris removal to keep culvert functioning.

- Water is ponding upstream of culvert since culvert flow capacity is reduced due to beaver dam and debris accumulation around inlet cage. During Stantec site visit, water was flowing in culvert with depth of flow of 0.1 m measured at culvert inlet. Bed material observed at culvert invert was silt.
- There is a large beaver dam approximately; 200 m upstream of existing culvert inlet (See site visit photo # 22, given in Appendix B). This top of dam is approximately 1.2 m above June 18, 2015 downstream water level and approximately 2 m above the lowest channel bed elevation. A dam break during a catastrophic flood event would release significant amount of debris and water.
- A tributary and the City of Edmonton's outfall structure discharge into the WWC just north of existing culvert inlet. A beaver dam was observed at mouth of this tributary. Tributary is flowing along left (north) bank north of outfall structure (See site visit photos given in Appendix B) and there is sign of an old slump along WWC left (north) bank at mouth of tributary.
- Most of the channel reach in vicinity of 199 crossing is impacted by a high level of beaver activity. Channel bed width and top width are wider than natural channel due to bank slumping because of ponding resulting from beaver activity. There are signs of active bank erosion along WWC downstream of existing 199 street crossing (See site visit Photo # 25 given in Appendix B). Surveyed section approximately, 50 m downstream of culvert outlet was used for hydraulic analysis due to its proximity to natural channel section (See site visit Photo # 33 given in Appendix B). Scour hole and ponding due to beaver dam was observed at culvert downstream end (See site visit Photos # 28 and 29 given in Appendix B). Scour hole at culvert downstream end suggests that existing 1.8 m diameter culvert is under sized for design flood.
- WWC bed width at a section under Anthony Henday Drive (AHD) was measured at 2 m. This section appears to be representative of natural creek section that is not impacted by beaver activity (See site visit Photo # 38, given in Appendix B). This section was utilized to carryout Channel Flow Capacity Analysis.

3.1.2 Review of available information pertinent to this study

3.1.2.1 Alberta Transportation (AT) Hydrotechnical Information System (HIS)

Location of relevant AT BFs (Bridge Files) crossing along WWC are shown on Figure A2 given in Appendix A. Table-1 given below provides relevant AT BFs information that was utilized for hydrotechnical assessment of 199 street crossing.

AT BF No.	eBMS Structue ID	Hwy	Location	Year Built	Structure Type	Bridge Spans/ No of Pipes	Length of Structure (m)	Pipe Diameter/ Bridge Width (m)	Height of roadway from Streamb ed (m)	Drainage Area to Crossing (km2)
70768	NA	60:2:20.923		UNKNOWN			0.0			12
08470	NA	Range Road 261	WINTERBURN	1990	MP	2	36.0	1.8	4.8	38
07061	NA	627:4:20.518	WINTERBURN	1981	SPE	1	70.7	1.7	9	39
09167	NA	627:4:18.125	WINTERBURN	1982	SPE	1	52.4	1.7	4	20
09168	NA	627:4:17.419	WINTERBURN	1982	SPE	1	53.0	1.7	5	18
06566	B109	199 Street	EDMONTON/627	1952	SP	1	62.8	1.8	8.8	56
02329	B144	215 Street	EDMONTON	1961	SP	1	37.8	1.8	5.8	50
85012N	B318	216:6:12.699	ANTHONY HENDAY DRIVE	2005	NU	3	135.0	41.5		58
85012S	B319	216:6:12.718	ANTHONY HENDAY DRIVE	2005	NU	3	135.0	41.5		58
07417	B021	184 Street	EDMONTON	1931	MP	2	24.4	1.8	2.3	62

Table-1: AT Relevant BFs Information from HIS

Based on HIS information provided in Table-1, drainage area contributing flow to WWC crossing at 199 street is 56 km².

3.1.2.2 Erosion Study for Wedgwood Creek at Edmonton dated December 2012, Golder Associates Ltd.

The Golder Associates Ltd. December 2012 report has presented detailed review of WWC in vicinity of 199 street crossing. Summary of information relevant to 199 street crossing is presented below:

- The WWC gross drainage area (GDA) contributing flow at mouth was determined to be approximately 170 km² with effective drainage area (EDA) of 147 km² (See Figure A3, given in Appendix A). Most (90 %) of the drainage area is located beyond City of Edmonton limit at 215 street in Parkland County and Stony Plain Indian Reserves and consists of residential developments and agricultural lands.
- The report also documented WWC watershed flood frequency analysis for maximum instantaneous discharge at the mouth. This flood frequency analysis summary is provided in Table-2 given below.

	Maximum Insta	*Future Maximum Instantaneous Unit		
Return Period (Years)	Historical	Existing	Future (Existing and Development)	discharge (q)= Future MID (m³/s)/GDA(km²)
2	6.2	5.8	6.9	0.04
5	13.0	12.3	14.5	0.09
10	19.4	18.3	21.6	0.13
20	27.4	25.9	30.5	0.18
25	30.5	28.7	33.9	0.20
50	41.5	39.1	46.1	0.27
100	55.6	52.4	61.8	0.36

Table-2: Flood Frequency Analysis for Wedgewood Creek Watershed

* Table 2 is from Golder Associates Ltd. December 2012 report and * Denotes calculations by Stantec.

- The report has mentioned that existing WWC crossings at 215 street, 199 street and 184 street are undersized and recommend that any of these crossings replacement plan must consider the benefits of flow attenuation and sediment storage provided by the existing undersized culverts as well as effects on the ecosystem in the WWC valley.
- It was recommended in this report to support beaver activity and preserving undersized culverts at 215 street, 199 street and 184 street crossings with installation of overflow culverts to handle catastrophic floods. It was also recommended to install or repair beaver deterrence measures such as culvert cages or tree fencing in locations where ponded water is a threat to infrastructure.

3.1.2.3 Riverview Area Master Plan dated March 2013, Stantec

The pertinent information of this report is presented below:

Based on the proposed concept presented in this report, approximately 220 ha (2.2 km²) of the Riverview area will drain into WWC; the remaining watershed will drain into the North Saskatchewan River through existing creeks/ravines located within the basin. The allowable discharge rates used were 2.5 L/s/ha (0.25 m³/s/km²) and 5.0 L/s/ha (0.5 m³/s/km²) for WWC and North Saskatchewan River (NSR).

3.1.2.4 Conceptual Bridge Planning Report Wedgewood Creek Crossing on 199 Street NW in the City of Edmonton Edmonton dated May 2014, Terrace Engineering Lid.

Terrace Engineering Ltd. has presented three structure options to accommodate creek flow and wildlife passage at 199 street crossing over WWC. Summary of these options is presented below:

- Bridge structure with or without large abutment walls: Terrace Engineering estimated a bridge, 28.6 m overall width x 120 m long out to out of fills and estimated conceptual bridge cost in the order of \$25 million.
- Oversized culvert structure suitable for wildlife passage in addition to stream flows: This option was not explored further due to cost associated with culvert size and length.
- Culvert sized only for stream flows and a separate wildlife passage structure: Terrace suggested 2.4 m diameter SPCSP culvert to accommodate creek flow and separate bridge with 28.6 m overall width x 26 m long out to out of fills to accommodate wildlife passage. The cost estimate for this option was in the order of \$7 million.

3.1.2.5 Riverview 199 Street Drainage System at Wedgewood Creek dated March 2015, Stantec:

The pertinent information of this report is presented below:

Implementation of storage and releasing at a controlled outflow was reviewed in this report. An underground storage pipe was recommended in this report due to the limited space and geometry available, and proximity to the WWC. A controlled outlet flow rate of 35 l/s/ha (0.35 m³/s/km²) was selected in conformance with the design parameters used for existing Edgemont 199 street storage.

3.2 DRAINAGE AREA CONTRIBUTING FLOW TO SITE ASSESSMENT

The proposed Wedgewood Creek (WWC) crossing is located at 199 street. WWC is a North Saskatchewan River (NSR) tributary that has its headwaters in the tablelands and then transition to a deeply incised ravine as it flows towards river. Most of the drainage area, contributing flows to the proposed site is relatively flat and is characterized by farming fields, vegetated land, small lakes and interconnected ponds (during high runoff periods).

The Golder Associates Ltd. December 2012 report has determined WWC gross drainage area (GDA) contributing flow at mouth to be approximately 170 km² with effective drainage area (EDA) of 147 km² (See Figure A3, given in Appendix A). This report also mentioned that most (90 %) of the drainage area is located beyond City of Edmonton limit at 215 street in Parkland

County and Stony Plain Indian Reserves and consists of residential developments and agricultural lands.

Based on Stantec's past working experience in WWC watershed area (City of Edmonton and Parkland County), engineering judgment, and;

Stantec's review of WWC watershed area (See Figures A1, A2, A3 and A4 given in Appendix A) using:

- Google Earth Pro Tool;
- Alberta Environment and Parks Flood Hazard Mapping Tool;
- Toporama Mapping Tool and;
- Information presented above including AT's HIS etc.

The effective drainage contributing flow to WWC crossing at 199 street identified by Golder report appears to be higher based on following considerations:

- Drainage area estimated in Golder report can be divided into two components due to land features: west of highway 60 and; east of highway 60.
- Drainage area component West of highway 60 is relatively flat and is characterized by
 agriculture land, residential areas, several wooded areas, some marsh areas, several
 small (intermittent and some permanent) lakes and interconnected ponds (during high
 runoff periods). WWC watercourse is not well defined west of highway 60. This is a
 major component of total WWC drainage area as estimated in Golder report. Due to
 presence of these land features, this component of area would have adequate internal
 storage and would provide minimum surface runoff during design flood event.
- Most of flow to site is contributed by drainage area component east of highway 60 due to its land feature and creek is well defined deeply incised ravine as it flows towards river.
- Based on HIS information provided in Table-1, drainage area contributing flow to WWC crossing at 199 street is 56 km². Based on land features of component of drainage area west of highway 60, the effective drainage area of 56 km² appears to be correct. HIS information provided in Table-1 also shows that there is no bridge file structure (i.e. equal or larger than 1.5 m diameter culvert) under highway 60.

Based on Stantec's past working experience in WWC watershed area (City of Edmonton and Parkland County), engineering judgment, review of above information presented in this section of report and considering the natural channel stream characteristics (See Site visit Photo # 38 given in Appendix B) the recommended effective drainage area contributing flow to WWC crossing at 199 street is 56 km².

3.3 BASIN RUNOFF POTENTIAL METHOD

The Basin Runoff Potential Method is a hydrotechnical tool developed by Alberta Transportation to help determine the 1: 100 year design discharge. The formula provided by Alberta Transportation's Technical Standards Branch to determine the maximum runoff potential:

 $Q = q \times DA$

Where

- Q = Basin Runoff Potential (m^3/s)
- q = Unit Runoff Potential (m³/s/km²), this parameter is based on AT's Basin Runoff
 Potential Map, past experience in the area (City of Edmonton and Parkland County) and engineering judgment.
- $q_1 = 0.55 \text{ m}^3/\text{s/km}^2$, based on AT's Basin Runoff Potential Map for this area
- q₂ = 0.25 m³/s/km², based on past experience in the area (City of Edmonton and Parkland County), information provided in Section 3.1 of this report and engineering judgment.
- DA = drainage area (km²) = 56 km², this is drainage area contributing flows to site is based on information provided in Section 3.2 of this report.

Based on past experience in the area (City of Edmonton and Parkland County), engineering judgment, the Basin Runoff Potential method and its sensitivity estimated the design flood to be in a range of $14 - 30.8 \text{ m}^3$ /s.

3.4 CHANNEL CAPACITY METHOD

Alberta Transportation's (AT) Channel Capacity method was used to calculate the channel capacity of WWC natural section. WWC bed width at a section under Anthony Henday Drive (AHD) was measured at 2 m. Creek at this section appears to be representative of natural creek section and is not impacted by beaver activity (See site visit Photo # 38, given in Appendix B). This section was utilized to carryout Channel Flow Capacity Analysis. Based on site visit and surveyed channel morphology, the Channel Capacity method and its sensitivity analysis estimated the design flood to be in a range of 9 - 13 m³/s with a depth of flow in a range of 1.2 - 1.5 m and a velocity of flow in a range of 2.9 - 3.2 m/s. Details of the analysis are included in the Appendix C.

3.5 CHANNEL HYDRAULIC ANALYSIS

The WWC channel section approximately 50 m downstream of the 199 street crossing was modeled by utilizing Alberta Transportation's HydroChan software and is based on surveyed section (see Appendix E for the survey information). Manning's "n" for the main channel and floodway were estimated for crossing based on the site visit and engineering judgment. Rating curve based on surveyed cross-section was analyzed hydraulically to determine a design discharge and associated flood stage. Based on this analysis, the average capacity of the channel resulted in a flow of range $19.6 - 31.35 \text{ m}^3$ /s with a depth of flow range of 1.5-1.8 m and a main channel average velocity in the range of 2.5 - 2.6 m/s. This surveyed section is somewhat impacted by high beaver activity. Channel bed width and top width are wider than natural channel due to bank slumping because of ponding resulting from beaver activity (See site visit photo given in Appendix B). Design flood quantities would be higher based on this section. Details of the analysis are included in the Appendix C.

3.6 RECOMMENDED DESIGN AND CHECK DISCHARGE PARAMETERS

Based on a review of the above methods, engineering calculations, experience and engineering judgment, the following design and check discharge parameters for the sizing of the hydraulic structure for Wedgewood Creek crossing at 199 street are recommended.

- The Q_{Design} flood was estimated to be 14 m³/s with a depth of flow of 1.3 m and a main channel average velocity of 2.4 m/s.
- Based on AT's guidelines Q_{fish passage} was estimated to be 1.4 m³/s with a depth of flow of 0.5 m and a main channel average velocity of 1.2 m/s.
- Based on AT's Basin Runoff Potential Method, the estimated flow of 30.8 m³/s with a depth of flow of 1.8 m and a main channel average velocity of 2.6 m/s was utilized as Q_{Check1} flood.
- Based on Golder Associates Ltd work (December 2012 report), the maximum instantaneous discharge of 61.8 m³/s with a depth of flow of 2.3 m in main channel and a main channel average velocity of 2.8 m/s was utilized as Q_{Check2} flood.

4.0 Structure Hydraulics

The following three structures options are proposed to replace the existing one 1.8 m diameter closed bottom Structural Plate Corrugated Steel Pipe (SPCSP):

a) One 3.0 m diameter closed bottom Corrugated Steel Pipe (CSP) Culvert

- b) One 3.05 m diameter closed bottom Structural Plate Corrugated Steel Pipe (SPCSP) and
- c) One 3.0 m Span x 2.4 m Rise Concrete Box Culvert.

An open bottom with 6 m span x 3m span x 117.5 long Deep Corrugated Steel Arch culvert option was also reviewed briefly. Based on Stantec experience on similar structure, this option will have a large cost component due to its length and size and geotechnical considerations. This option is not further considered in this report.

All other culvert options that were considered in this report would be designed with burial depth to accommodate fish passage. This would provide a bedwidth within the culvert similar to bedwidth in natural channel.

The hydraulic analysis for the existing one 1.8 m diameter closed bottom SPCSP and three proposed structure options assessed are provided in the following sections.

4.1 EXISTING ONE 1.8 M DIAMETER CLOSED BOTTOM STRUCTURAL PLATE CORRUGATED STEEL PIPE (SPCSP)

The design and check discharges have been analyzed hydraulically through the existing single 1.8 m diameter closed bottom Structural Plate Corrugated Steel Pipe (SPCSP) culvert for WWC crossing at 199 street under existing conditions. Alberta Transportation's Hydro Culv software was used for the hydraulic analysis.

Existing single 1.8 m diameter SPCSP culverts was modeled with existing conditions (culvert invert length of 68.6 m, culvert centerline invert elevation of 671.41 m, no pipe burial depth and a 3.3 % slope) for the design and check discharges. These existing culvert measurements are based on Stantec June 2015 survey.

Under these conditions, existing pipe would flow full under a head of 8.3 m at pipe inlet for 1:100 year design flow. See Sketch SK-1 in Appendix F for hydraulic details.

The velocity for fish passage flow through the existing single 1.8 m diameter SPCSP culvert are higher than the velocity calculated for the natural channel and there is also hydraulic jump at pipe downstream end.

Table-3 summarizes the hydraulics of the proposed structures.

	1-1.8 m Diameter SPCSP Culvert								
	Na	atural Char	nnel		Propos	ed Culvert			
Flow	Flow (m³/s)	Depth (m)	Velocity (m/s)	Pipe Upstream Depth of Flow ⁽¹⁾ (m)	Mean Velocity at Inlet (m/s)	Mean Velocity at Outlet (m/s)	Freeboard and Comments (m)		
Q _{design}	14	1.3	2.4	8.2	5.5	5.5	Flowing full		
Q_{fish} passage	1.4	0.5	1.2	0.9	2.0	2.3	0.9 and Jump at pipe end		
Q _{check1}	30.8	1.8	2.6	42.6	12.1	12.1	Flowing full and most likely road embankment will fail due to overtopping		
Q _{check2}	61.8	2.3	2.8	171.7	24.3	24.3	Flowing full most likely road embankment will fail due to overtopping		

Table-3: Hydraulics of Existing 1-1.8 m Diameter SPCSP Culvert

Note: ⁽¹⁾ Depth of flow is above the streambed elevation at the upstream culverts end.

Details of the hydraulic results are included in Appendix D.

This option is not recommended.

4.2 SINGLE 3.0 M DIAMETER CLOSED BOTTOM CORRUGATED STEEL PIPE (CSP)

The design and check discharges have been analyzed hydraulically through the proposed single 3.0 m diameter closed bottom Corrugated Steel Pipe (CSP) culvert for WWC crossing at 199 street. Alberta Transportation's Hydro Culv software was used for the hydraulic analysis.

Proposed single 3.0 m diameter CSP culvert and proposed wild life passage bridge (14 m wide x 32 m long x 4.5 high) were modelled. Proposed CSP culvert was modelled with an invert length of 117.5 m with a theoretical streambed centerline elevation of 670.0 m and a pipe burial depth of 0.75 m on a 1.4 % slope. Proposed bridge was modelled with a theoretical streambed centerline elevation of 675.85 m. Both structures were modelled for the design and check discharges and downstream boundary conditions.

Under these conditions, proposed pipe would flow with a freeboard of 0.3 m for design flow (1:100 year). During extreme floods (Qcheck1 and Qcheck2), wildlife passage bridge would provide adequate hydraulic opening to pass these floods without overtopping roadway embankment. See Sketch SK-2 in Appendix F for hydraulic details.

The velocity for fish passage flow through the proposed single 3.0 m diameter SPCSP culvert is higher than the velocity calculated for the natural channel for same flow. Installation of Class 1M rock (max size 300 mm) with pitrun gravel substrate is warranted at culvert invert for fish passage. Class 2 boulders would also be installed at 10 m spacing to interlock substrate and to minimize its movement.

Class 2 (max size 800 mm) heavy rock riprap on the upstream and downstream ends of the culvert is warranted for erosion and scour protection. Table-4 summarizes the hydraulic parameters of the proposed structures.

	1-3.0 m Diameter CSP Culvert							
	Na	atural Char	nnel	Proposed	Culvert with	Substrate In	stalled	
Flow	Flow (m³/s)	Depth (m)	Velocity (m/s)	Pipe Upstream Depth of Flow ⁽¹⁾ (m)	Mean Velocity at Inlet (m/s)	Mean Velocity at Outlet (m/s)	Freeboard and Comments (m)	
Q _{design}	14	1.3	2.4	2.7	2.6	2.4	0.3	
Q _{fish passage}	1.4	0.5	1.2	0.8	1.4	0.5	2.2	
Q _{check1}	30.8	1.8	2.6	6.4	3.6	3.6	Pipe Flowing Full and Flow in Wildlife Bridge	
Q _{check2}	61.8	2.3	2.8	7.5	3.8	3.8	Pipe Flowing Full and Flow in Wildlife Bridge	

Table-4: Hydraulics of	f Existing 1-3.0 m	Diameter CSP Culvert
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Note: ⁽¹⁾ Depth of flow is above the streambed elevation at the upstream culverts end.

Details of the hydraulic results are included in Appendix D.

4.3 SINGLE 3.05 M DIAMETER CLOSED BOTTOM STRUCTURAL PLATE CORRUGATED STEEL PIPE (SPCSP)

The design and check discharges have been analyzed hydraulically through the proposed single 3.05 m diameter closed bottom Structural Plate Corrugated Steel Pipe (SPCSP) culvert

for WWC crossing at 199 street. Alberta Transportation's Hydro Culv software was used for the hydraulic analysis.

Proposed single 3.05 m diameter SPCSP culvert and proposed wild life passage bridge (14 m wide x 32 m long x 4.5 high) were modeled. Proposed SPCSP culvert was modelled with an invert length of 117.5 m with a theoretical streambed centerline elevation of 670.0 m and a pipe burial depth of 0.75 m on a 1.4 % slope. Proposed bridge was modelled with a theoretical streambed centerline elevation of 675.85 m. Both structures were modelled for the design and check discharges and downstream boundary conditions.

Under these conditions, proposed pipe would flow with a freeboard of 0.3 m for design flood (1:100 year). During extreme floods (Qcheck1 and Qcheck2), wildlife passage bridge would provide adequate hydraulic opening to pass these floods without overtopping roadway embankment. See Sketch SK-3 in Appendix F for hydraulic details.

The velocity for fish passage through the proposed single 3.0 m diameter SPCSP culverts is higher than the velocity calculated for the natural channel for same flow. Installation of Class 1M rock (max size 300 mm) with pitrun gravel substrate is warranted at culvert invert for fish passage. Class 2 boulders would also be installed at 10 m spacing to interlock substrate and to minimize its movement.

Class 2 (max size 800 mm) heavy rock riprap on the upstream and downstream ends of the culverts is warranted for erosion and scour protection.

Table-5 summarizes the hydraulic parameters of the proposed structures.

	1-3.05 m Diameter SPCSP Culvert								
	Natural Channel		Proposed	Proposed Culvert with Substrate Installed					
Flow	Flow (m³/s)	Depth (m)	Velocity (m/s)	Pipe Upstream Depth of Flow ⁽¹⁾ (m)	Mean Velocity at Inlet (m/s)	Mean Velocity at Outlet (m/s)	Freeboard and Comments (m)		
Q _{design}	14	1.3	2.4	2.7	2.6	2.3	0.35		
Q _{fish passage}	1.4	0.5	1.2	0.8	1.4	0.5	2.3		
Q _{check1}	30.8	1.8	2.6	6.3	3.6	3.7	Pipe Flowing Full and Flow in Wildlife Bridge		
Q _{check2}	61.8	2.3	2.8	7.4	3.8	3.8	Pipe Flowing Full and Flow in Wildlife Bridge		

Table-5: Hydraulics of Existing 1-3.05 m Diameter SPCSP Culvert

Note: ⁽¹⁾ Depth of flow is above the streambed elevation at the upstream culverts end.

Details of the hydraulic results are included in Appendix D.

4.4 SINGLE 3.0 M SPAN BY 2.4 M RISE CONCRETE BOX CULVERT

The design and check discharges have been analyzed hydraulically through the proposed single 3.0 m span x 2.4 m rise concrete box culvert for WWC crossing at 199 street. Alberta Transportation's Hydro Culv software was used for the hydraulic analysis.

Proposed one 3.0 m span x 2.4 m rise concrete box culvert and proposed wild life passage bridge (14 m wide x 32 m long x 4.5 high) were modeled. Proposed concrete box culvert was modelled with an invert length of 117.5 m with a theoretical streambed centerline elevation of 670.0 m and a pipe burial depth of 0.6 m on a 1.4 % slope. Proposed bridge was modelled with a theoretical streambed centerline elevation of 675.85 m. Both structures were modelled for the design and check discharges and downstream boundary conditions.

Under these conditions, proposed concrete box culvert would flow full for design flood (1:100 year). During extreme floods (Qcheck1 and Qcheck2), wildlife passage bridge would provide adequate hydraulic opening to pass these floods without overtopping roadway embankment. See Sketch SK-4 in Appendix F for hydraulic details.

The velocities for fish passage through the proposed single 3.0 m span x 2.4 m rise concrete box culvert are higher than the velocity calculated for the natural channel. Installation of Class 1M rock (max size 300 mm) with pitrun gravel substrate is warranted at culvert invert for fish passage. Class 2 boulders would also be installed at 10 m spacing to interlock substrate and to minimize its movement.

Class 2 (max size 800 mm) heavy rock riprap on the upstream and downstream ends of the culvert is warranted for erosion and scour protection.

Table-6 summarizes the hydraulic parameters of the proposed structures.

	Culvert1-3.0 m Span x 2.4 m Rise Concrete Box Culvert							
	Na	atural Char	nnel	Proposed	Culvert with	Substrate In	stalled	
Flow	Flow (m³/s)	Depth (m)	Velocity (m/s)	Pipe Upstream Depth of Flow ⁽¹⁾ (m)	Mean Velocity at Inlet (m/s)	Mean Velocity at Outlet (m/s)	Freeboard and Comments (m)	
Q _{design}	14	1.3	2.4	2.6	2.4	2.1	Pipe Flowing Full with no Freeboard	
Q _{fish passage}	1.4	0.5	1.2	0.7	1.2	0.4	1.9	
Q _{check1}	30.8	1.8	2.6	6.4	3.4	3.4	Pipe Flowing Full and Flow in Wildlife Bridge	
Q _{check2}	61.8	2.3	2.8	7.5	3.6	3.6	Pipe Flowing Full and Flow in Wildlife Bridge	

Table-6: Hydraulics of 1-3.0 m Span x 2.4 m Rise Concrete Box Culvert

Note: ⁽¹⁾ Depth of flow is above the streambed elevation at the upstream culverts end.

Details of the hydraulic results are included in Appendix D.

5.0 Rock Protection Works

The material provided for Class 1M and Class 2 heavy rock riprap shall have a gradation that conforms to the following given in Table 7.

Table-7: Specification of Class 2 Rock Riprap (Source: Alberta Transportation)

Description	Units	Class 1M	Class 2
Nominal Mass	Kg	7	200
Nominal Diameter	or mm	175	500
Not greater than	Kg	40	700
	or mm	300	800
20 % to 50%	Kg	10	300
	or mm	200	600
50% to 80%	Kg	7	200
	or mm	175	500
100% greater than:	Kg	3	40
	or mm	125	300

6.0 Environmental Considerations

It has been identified by others that WWC crossing at 199 street would require to accommodate both aquatic and small terrestrial animal passage through proposed culvert. Stantec has reviewed to design culvert crossing to accommodate both aquatic and small terrestrial animal passage.

Based on Wedgewood Creek Road Crossing 199 Street: Fish Habitat Assessment report dated December 2014, prepared by Stantec, the fish habitat in Wedgewood crossing is rated as moderate for forage fish species. WWC crossing at 199 street would be designed for fish passage.

Based on high beaver dam activity and wood debris in Wedgewood creek, it appears that construction of a shelf along culvert length with ramp at culvert inlet to assist movement of small terrestrial animals through culvert would cause maintenance issues and would also cause an accumulation of debris at culvert inlet. Based on discussion with Bill Harper, Senior Wildlife Biologist of Stantec, a single 1.0 m diameter CSP culvert invert would be installed above design flood elevation (See Sketches 2, 3 and 4 given in Appendix F). This single 1.0 m diameter culvert would be solely dedicated to small terrestrial animal passage.

The site considered is not navigable in vicinity of 199 proposed crossing according to the watercourse features, presence of high beaver dam activity and several undersized crossings.

Due to high beaver dam activity in area WWC crossing at 199 street would be designed to accommodate debris passage through crossing opening crossing hydraulic opening would be designed with freeboard for design flood. This freeboard would help debris passage through this crossing. The option to install cage at culvert inlet would require regular maintenance and debris removal for design flow passage through culvert. From site visit (See site visit photos in Appendix B), it is evident that culvert is not performing at its full capacity due to debris accumulation around debris catcher cage at culvert inlet. The existing cage is damaged due to debris. This suggests that this culvert requires maintenance and debris removal at regular intervals. Debris catcher cage contributes to the debris accumulation and eventually becomes another dam at the culvert inlet if debris is not removed. A debris catcher is one solution but only works with regular culvert maintenance and debris removal to keep culvert functioning. Stantec would recommend not installing debris catcher cage at culvert with some freeboard. Stantec also recommend regular maintenance and large debris removal from culvert inlet to keep it working at its full hydraulic capacity.

7.0 Geotechnical

Hoggan Engineering & Testing (1980) Ltd. was retained for undertaking the geotechnical investigations for this project. Hoggan Engineering & Testing (1980) Ltd. drilled five test holes 2015-01 to 2015-05 in vicinity of WWC crossing at 199 street crossing. The subsurface condition generally consists of clay fill overlaying sand and/or lacustrine high plastic clay underlain by silt. The final soil encountered in testholes was clay till. Geotechnical report received from Hoggan Engineering & Testing (1980) Ltd. is included in Appendix G.

As part of the Geotechnical Investigation, Hoggan Engineering & Testing (1980) Ltd. completed soil analysis for this site and an assessment of corrosion potential. The conductivity of water was reported 586 μ S/cm (equaling resistivity 1706.5 ohm-cm). The pH of the water was 8.09. According to the "CSP Durability Guide" by the National Corrugated Steel Pipe Association, a single galvanized coating 610g/m² culvert with a culvert wall thickness of 1.6 mm is considered acceptable for these conditions for more than 75 year average invert service life of CSP (80 years). For this culvert we are recommending culvert wall thickness of 3.5 mm for CSP and 4.0 mm for SPCSP. Soil and water analysis excerpts are given in geotechnical report included in the Appendix G.

8.0 Structure Options

Options investigated for the proposed crossing are; 1-3000 mm diameter round corrugated steel culvert (CSP), 1-3050 mm diameter round structural plate corrugated steel culvert (SPCSP) and 1-3000 mm span x 2400 mm rise box concrete box culvert.

A summary of the structures under consideration are summarized below:

8.1 OPTION A – SINGLE 3000 MM DIAMETER CLOSED BOTTOM CORRUGATED STEEL PIPE (CSP)

A single 3000 mm CSP culvert with an invert length in the order of 117.5 m under a fill in order of 9.1 m at 1.4 % slope would be installed on 40° RHF skew to the roadway centerline. Due to high fill load, a wall thickness of 3.5 mm would be required to meet the structural capacity requirements. Hydraulics point of view, that culvert accommodates design flood with some freeboard to accommodate debris flow. With the provision of Class 1M rock (maximum size 300 mm) with pitrun gravel and Class 2 (maximum size 800 mm at spacing of 10 m) boulders on the culvert invert, culvert would provide fish passage. A separate single 1.0 m diameter CSP culvert with an invert length in the order of 92.5 m under a fill in order of 6.6 m at 0.5 % slope would be installed on 40° RHF skew to the roadway centerline. This single 1.0 m diameter culvert would be solely dedicated to small terrestrial animal passage. Guardrail for the culvert option is warranted based on the provision of 2:1 sideslopes.

8.2 OPTION B – SINGLE 3050 MM DIAMETER CLOSED BOTTOM STRUCTURAL PLATE CORRUGATED STEEL PIPE (SPCSP)

A single 3050 mm SPCSP culvert with an invert length in the order of 117.5 m under a fill in order of 9.1 m at 1.4 % slope would be installed on 40° RHF skew to the roadway centerline. Due to high fill load, a wall thickness of 4.0 mm would be required to meet the structural capacity requirements. Hydraulics point of view, that culvert accommodates design flow with some freeboard to accommodate debris. With the provision of Class 1M rock (with maximum size 300 mm) with pitrun gravel and Class 2 (maximum size 800 mm at spacing of 10 m) on the culvert invert, culvert would provide fish passage. A separate single 1.0 m diameter CSP culvert with an invert length in the order of 92.5 m under a fill in order of 6.6 m at 0.5 % slope would be installed on 40° RHF skew to the roadway centerline. This single 1.0 m diameter culvert would be solely dedicated to small terrestrial animal passage. Guardrail for the culvert option is warranted based on the provision of 2:1 sideslopes.

8.3 OPTION C – SINGLE 3000 MM SPAN BY 2400 MM RISE CONCRETE BOX CULVERT

A single 3000 mm span x 2400 mm rise concrete box culvert with an invert length in the order of 117.5 m under a fill in order of 9.3 m at 1.4 % slope would be installed on 40° RHF skew to the roadway centerline. Hydraulics point of view, that culvert accommodates design flood with no freeboard. With the provision of Class 1M (maximum size 300 mm) pitrun gravel and Class 2 (maximum size 800 mm at spacing of 10 m) on the culvert invert, culvert would provide fish passage. A separate single 1.0 m diameter CSP culvert with an invert length in the order of 92.5 m under a fill in order of 6.6 m at 0.5 % slope would be installed on 40° RHF skew to the roadway centerline. This single 1.0 m diameter culvert would be solely dedicated to small terrestrial animal passage. Guardrail for the culvert option is warranted based on the provision of 2:1 sideslopes.

9.0 Opinion of Probable Cost

The estimated contract cost (within +/- 25 %) for this project including 15 % contingency is summarized below in Table-8. Other project costs such as, wildlife passage bridge, utility relocation, traffic accommodation during construction, common fill, slope erosion control measures and additional right of way etc. are not included. Small animal passage culvert cost is included in estimated cost. Details of the cost estimate are included in the Appendix H.

Description	Probable Cost Estimate
A Single 3000 mm diameter closed bottom CSP culvert with a 117.5 m invert length	\$ 906,000
A Single 3050 mm diameter closed bottom SPCSP culvert with a 117.5 m invert length	\$ 1,178,000
A Single 3000 mm span x 2400 mm rise concrete box culvert with a 117.5 m invert length	\$ 1,605,000

Table-8: Or	oinion of Probable	e Cost includina	15% Contingency
		, eeee moraamig	io/o oonungonoy

10.0 Detailed Design Considerations

Based on information provided in above sections of this report, the following items will need to be incorporated into the detailed design:

- Outfall operation and WWC tributary flows at upstream end.
- North bank stability (old slump) at upstream end.
- Geotechnical recommendations
- Roadway geomatics
- Design flow, fish passage, large animal passage and small animal passage
- Beaver dam activity and its impacts on culvert flows and environment.
- Downstream WWC scour and erosion
- Constructability issues will need to be considered and addressed for chosen structure option during the detailed design stage.

11.0 Recommendation

Considering cost, technical feasibility, installation, hydraulic performance and long term functionality, it is recommended to proceed with the detail design of Option 1 (Single 3000 mm diameter closed bottom corrugated steel pipe (CSP)) for the Wedgewood Creek Crossing at 199 street culvert replacement. Option 1 provides adequate hydraulic capacity for design flood with some freeboard to assist in accommodating debris passage. It would also provide fish passage. Option 1 would also facilitate an easy and fast installation of the new structure.

Stantec would also recommend regular maintenance and debris removal from culvert inlet to keep it working at its full hydraulic capacity.

It is evident that existing 1.8 m diameter SPCSP culvert is not performing at its full capacity due to debris accumulation around debris catcher cage at culvert inlet. The existing cage is damaged due to debris. Debris catcher cage contributes to the debris accumulation and eventually becomes another dam at the culvert inlet if debris is not removed. A debris catcher is one solution but only works with regular culvert maintenance and debris removal to keep culvert functioning. Considering all the pros and cons of a debris catcher, Stantec is not recommending a debris catcher cage at proposed culvert inlet.

Based on discussion with Bill Harper, Senior Wildlife Biologist of Stantec, it is also recommended that a single 1.0 m diameter CSP culvert be designed. This culvert would be solely dedicated to small terrestrial animal passage and the culvert invert would be installed above design flood elevation (See Sketches 2, 3, 4 given in Appendix F).

11.0 Closing

We would be pleased to discuss the recommendations provided in this report with Qualico Communities at your earliest convenience.

Prepared By:

Reviewed By:

Arshed Mahmood, M.Sc., P.Eng.

Bridge Planning Engineer

Ralph Walters, M.Eng., P.Eng.

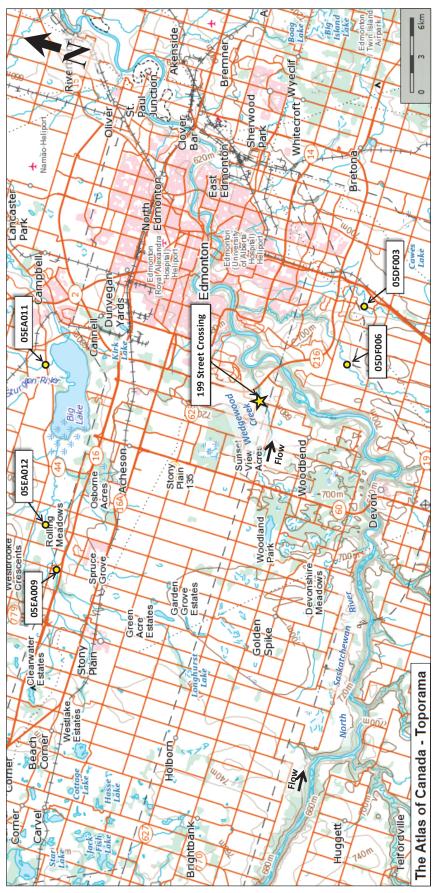
S. Bridge Planning Engineer

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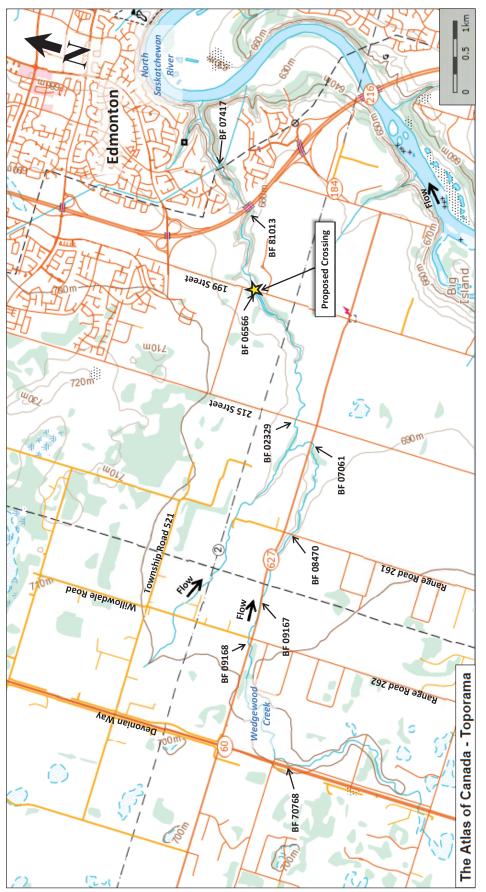
APPENDICES

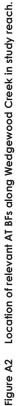
APPENDIX A

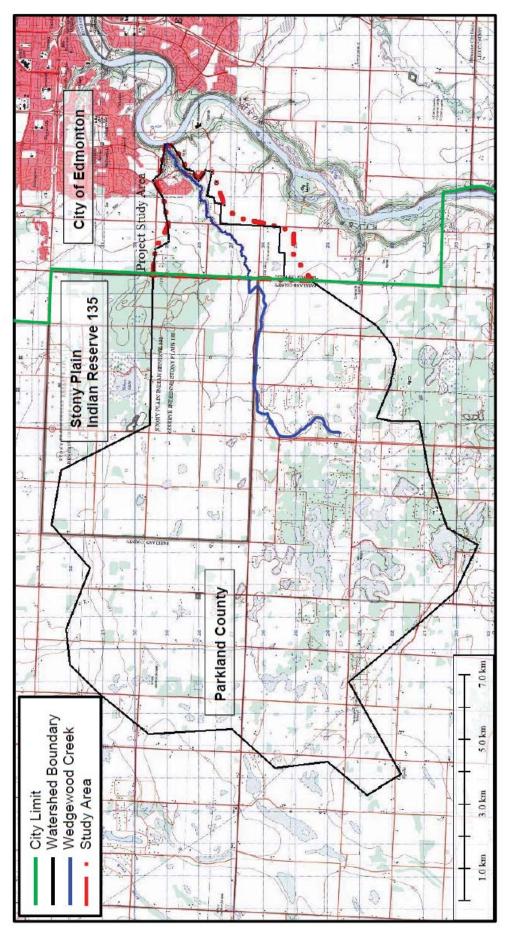
TOPOGRAPHIC MAPS AND DRAINAGE AREA ASSESSMENT



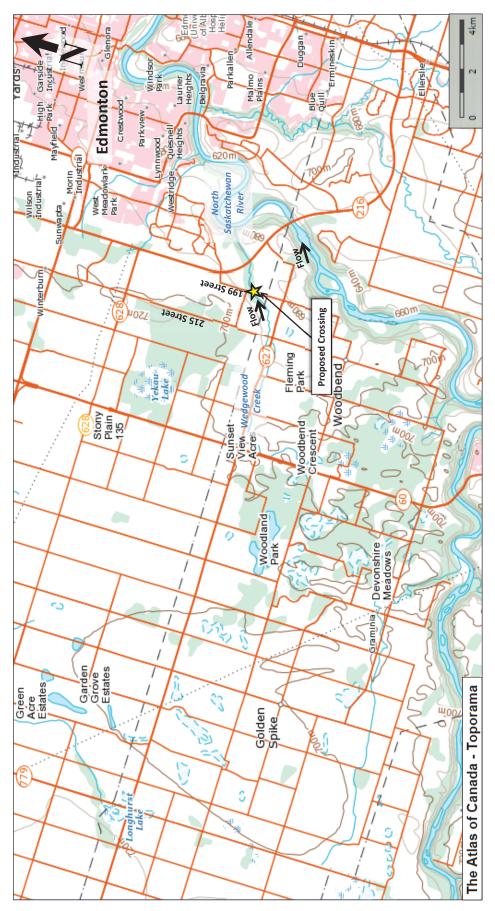














APPENDIX B

JUNE 18, 2015 SITE VISIT PHOTOS





Photo 1: Looking upstream at upstream end of Culvert



Photo 2: Looking upstream at upstream end of Culvert Note: Debris accumulation



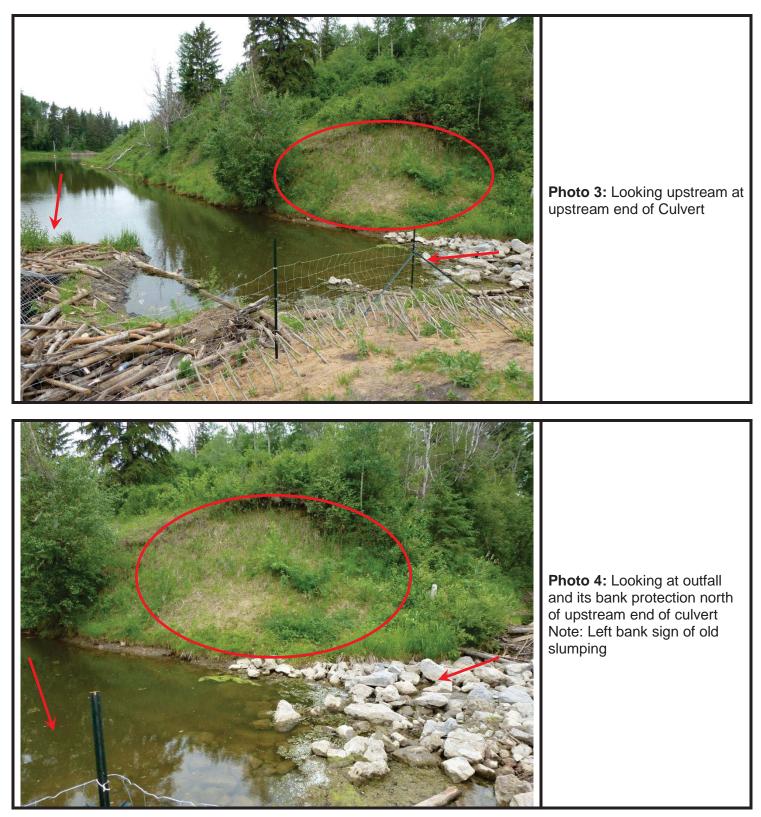






Photo 5: Looking at outfall and its bank protection north of upstream end of culvert Note: Left (north) bank sign of old slumping



Photo 6: Looking at outfall and its bank protection north of upstream end of culvert Note: Beaver dam at mouth of tributary joining Wedgewood creek





Photo 7: :Looking at upstream end of the culvert Note: Beaver dam, debris catcher and accumulation of debris at upstream end of culvert. Please also note slope of right (south) bank slope.



Photo 8: Looking at outfall and its bank protection north of upstream end of culvert





Photo 9 : Looking at outfall and its bank protection north of upstream end of culvert Note: Beaver dam at mouth of tributary joining Wedgewood creek



Photo 10: Looking at erosion control measures along upstream (west) side slope





Photo 11: Looking downstream at outfall

Note: Extent of Class 1 rock protection provided at outfall outlet.



Photo 12: Looking downstream at upstream end of existing culvert Note: Beaver dam, debris catcher and accumulation of debris at upstream end of culvert.



Bridge File: 06566 (B109) Highway: 199 Street Location: Edmonton Date: June 18, 2015



Photo 13: Looking upstream at tributary joining Wedgewood Creek upstream of crossing along left (north) bank north of outfall



Photo 14: Looking at beaver dam on tributary upstream of crossing along left (north) bank



Wedgewood Creek Crossing at 199 Street

Bridge File: 06566 (B109) Highway: 199 Street Location: Edmonton Date: June 18, 2015

